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Transportation Technology Center, Inc., a subsidiary of the Association of American Railroads

VTI Simulation Workshop Suspensions Part 2 and other Modeling Challenges

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◆ **Suspension components**

- Coil springs (PEK)
- Further improvements for friction wedges (PEK)
- Air suspensions (PEK)
- Center plates
- Couplers and Draft gears
- Polymer Springs
- Falling and variable friction for friction elements

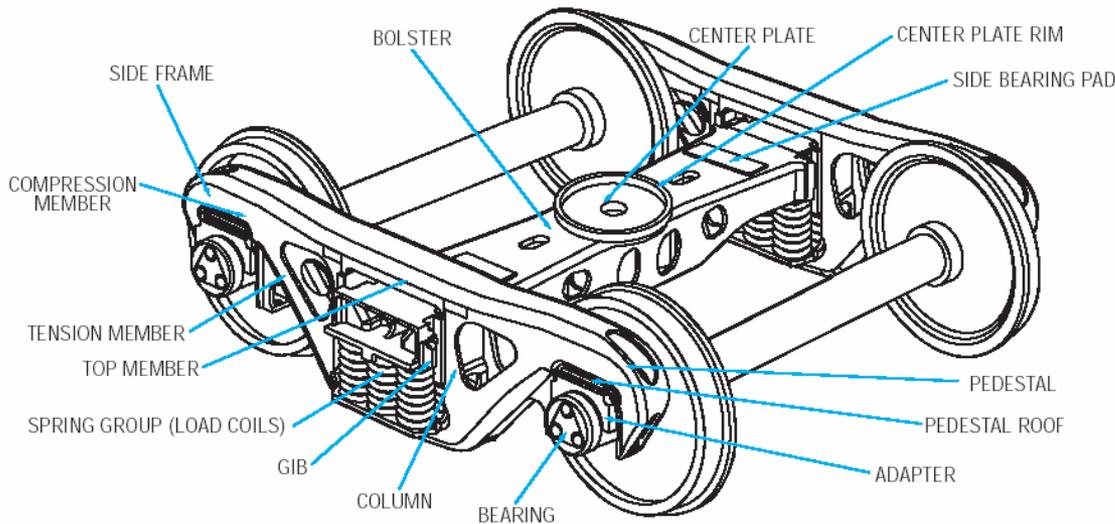
◆ **Other simulation challenges**

- Variation of rail profile along the track
- 3-D WR contact
- Special Track Work and Track Structure modeling
- Parametric variations and stochastic modeling
- On-line interaction w/FEA
- Integration methods



Centerplates & Centerbearings

- ◆ Center plates and bowls with inner or outer rim contact
- ◆ Hemispherical bowls
- ◆ Friction surfaces with varying load distribution



Centerplates & Centerbearings

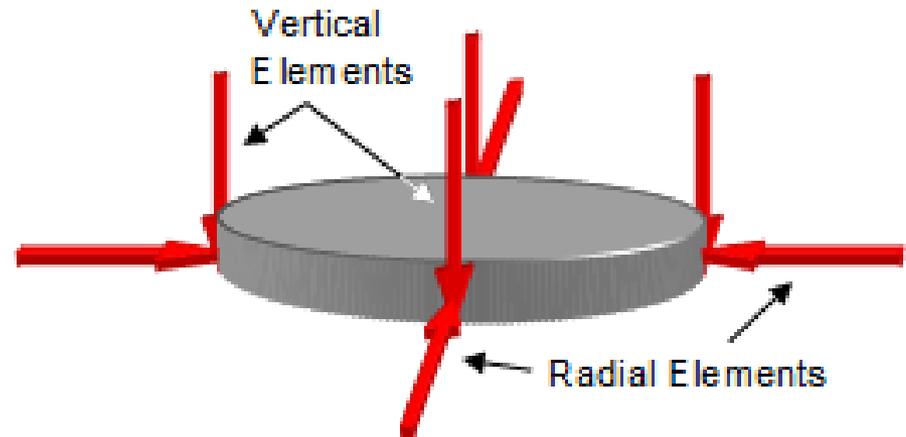
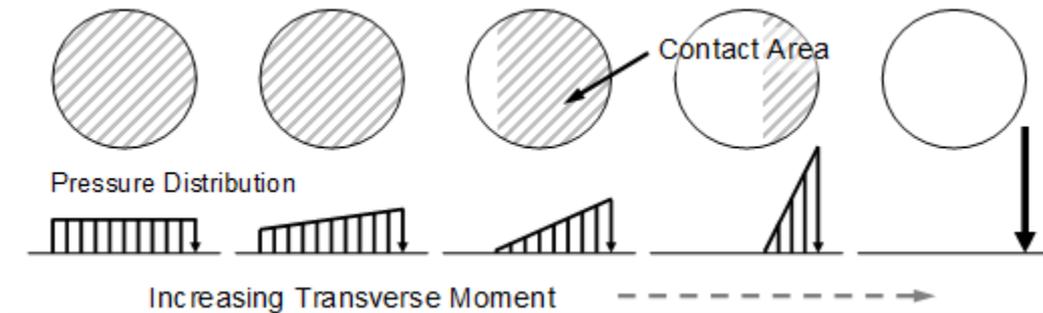
Simulation Challenges

◆ Representation of load distribution across surface under influence of pitching and rocking motions

- Often simulated by multiple point load line or surface friction elements

◆ Load dependent stick slip friction

- What μ ?
- Effects of lubrication and polymer liners



Centerplates & Centerbearings More More Simulation Challenges

◆ Effect of chamfers on centerplate

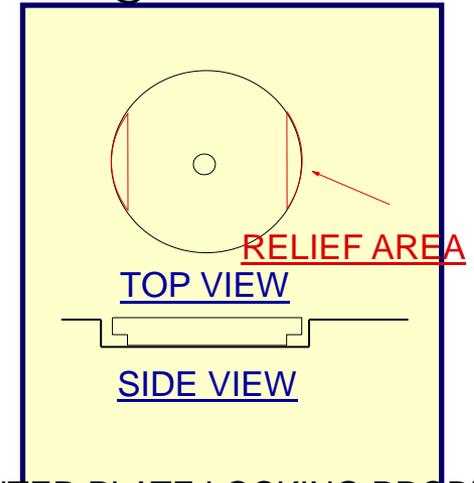
- Chamfers can complicate analysis
- Corners can dig in, act as center of rotation

◆ Effects of wear and galling on surfaces: What μ ? Falling friction?

◆ Centerbowl rim contact friction – effect of radial gap and moving points of contact around the circumference of rim

- Can significantly increase effective turning resistance
- Need numerous point load elements to capture the effects

◆ MAY NEED TO DEVELOP A VERY DETAILED SPECIFIC MODEL!

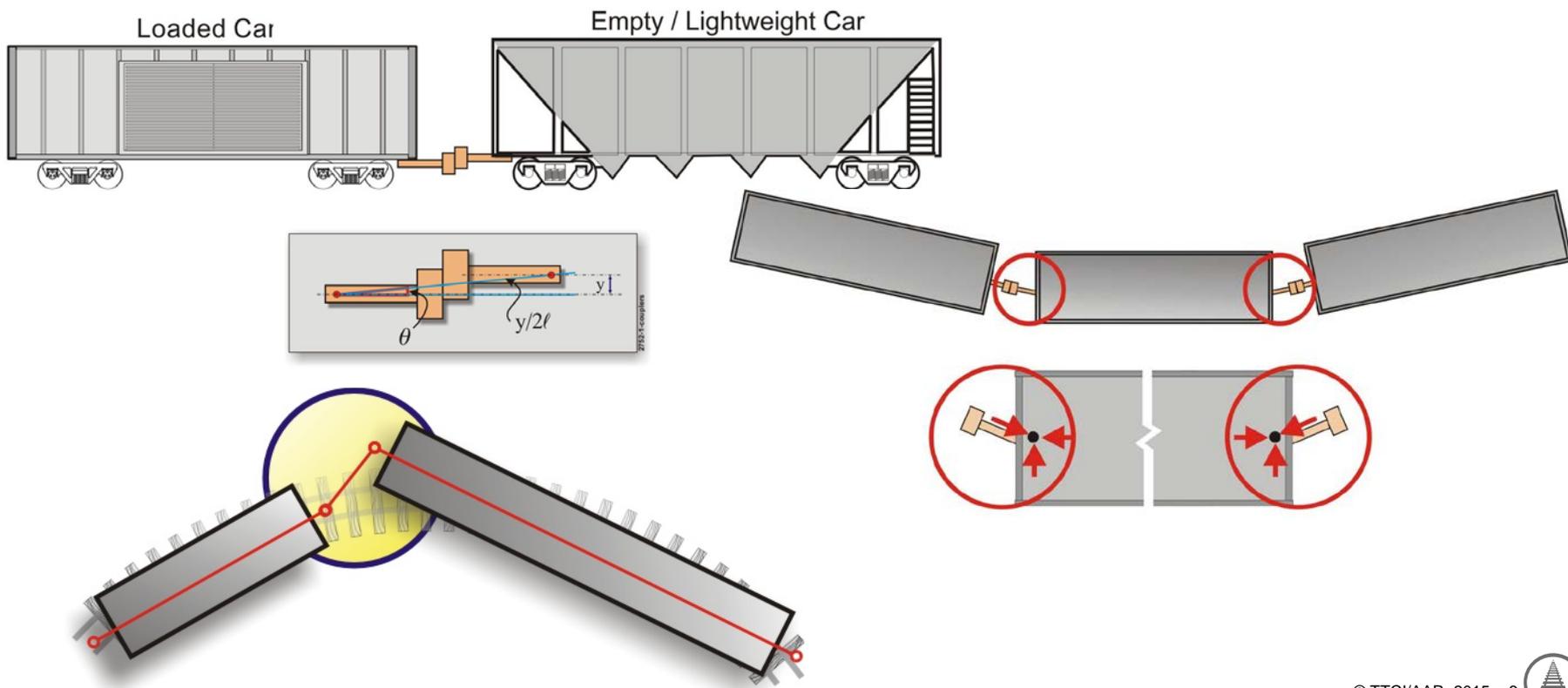


CENTER PLATE LOCKING PROBLEM



TTCI Couplers, Draft Gears & Train Forces

- ◆ **Buff-draft forces, coupler offsets & angles an generate significant off-axis forces between cars => derailment**
 - Buff-Draft forces can increase lateral WR forces and L/Vs
 - 250 k-lb buff force can lift a 20,000lb empty carbody car off of its trucks with a coupler misalignment of only 0.4 inch



- ◆ **Train action models such as TOES™ can provide macroscopic analysis**
- ◆ **Detailed MBD models required for accurate analyses**
 - Effect on WR forces and L/V ratios
 - Draft gear action
 - ▲ Stiffness and damping, including hysteresis of polymer springs
 - ▲ Friction effects
 - ▲ Limit stops
 - ▲ Rough castings may change line of action
 - ▲ Manufacturing tolerances
 - Coupler-Coupler interface
 - ▲ Vertical sliding
 - ▲ Toggling action can be indeterminate, might pop to left or right => stochastic modeling required?

Polymer Suspension Elements

◆ Used in:

- Primary suspensions, side bearings, damper bushings, coupler draft gears, centerpins, main secondary suspension element
- Materials can have very non-linear response
 - ▲ Hysteretic damping
 - ▲ Velocity dependent damping
 - ▲ Stroke dependent damping
 - ▲ Material Creep – from age, and also short term settling
 - Can make identification of static load conditions difficult
 - ▲ Shaping to generate non-linear characteristics
 - ▲ Shear stiffness sometimes dependent on axial loads
 - Can result in unstable conditions with negative effective stiffness
 - ▲ Internal damping (energy dissipation) can change the effective stiffness and damping response



Example: Polymer Primary Suspension

- ◆ **Lateral flexibility, shape of ears and ridges, and tolerances in pedestal jaws allow small sliding on top surface: surface friction**
- ◆ **Material should be designed/tuned for balance of curving and hunting response**
 - Early soft versions allowed hunting under loaded (286k-lb) cars
- ◆ **Required combination of several types of standard connection to capture the response**

Wilson, N.G., Wu, H., Tournay, Urban, C., "Effects of Wheel/Rail Contact Patterns and Vehicle Parameters on Lateral Stability," Supplement to the International Journal of Vehicle Systems Dynamics, Volume 48, pp. 487-504, Taylor Francis, 2010, ISBN 978-0-415-66949-8. Presented at the 21st IAVSD Symposium, Stockholm, Sweden, August 2009





Polymer Suspension Elements

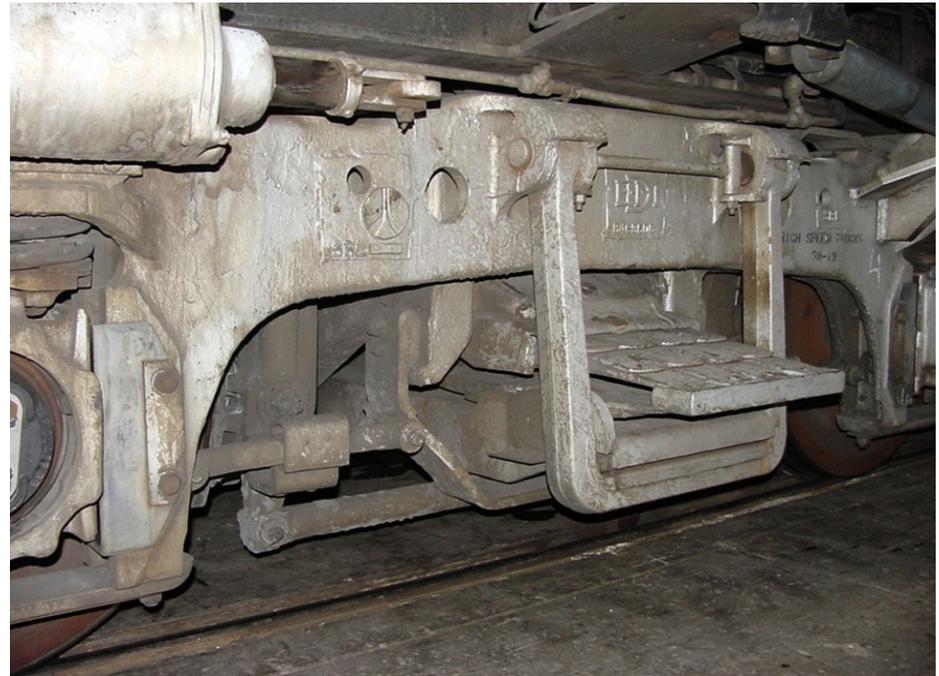
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- ◆ **Non-linear response may be difficult to represent using standard connection/suspension elements**
- ◆ **Detailed characteristic data often considered proprietary by manufacturers**
- ◆ **Extensive laboratory tests of components may be required to measure characteristics for model inputs**
 - Shear under various axial loads
 - Wide range of inputs for loads, frequencies, strokes
 - Some applications such as draft gears and secondary suspension may require very high forces to test correctly
 - ▲ Static load + 50% for main spring of 286 klb freight car is 80klb
 - ▲ Typical draft gear must withstand 200 – 300 klb buff force



Friction Modeling

- ◆ **It is not only in the wheel-rail interface!**
- ◆ **Sidebearings, centerplate, friction wedges, pedestal jaws, pin joints, swing hangers, leaf springs**
 - This common locomotive truck has all of them
 - Small variations can have significant effect on results
- ◆ **Point load vs distributed load**
- ◆ **Surface vs line friction**
- ◆ **Stick slip modeling**
- ◆ **Falling friction (static vs dynamic)**



◆ Required for:

- High AOA (greater than 15 to 20 mrad)
- Switches and crossings
- Guard and restraining rails
- Damaged track such as collapsed railheads
- Damaged wheels such as broken flanges
- Switch point guards

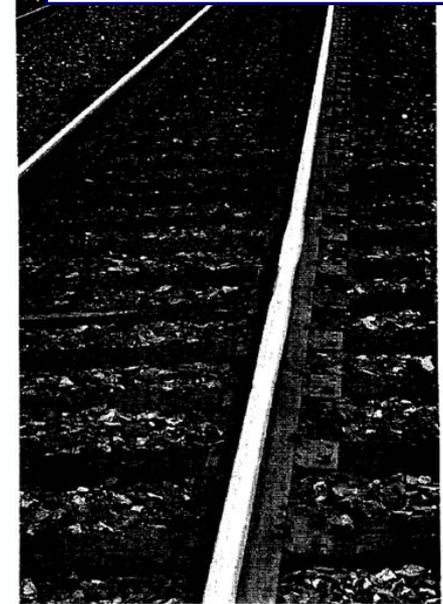
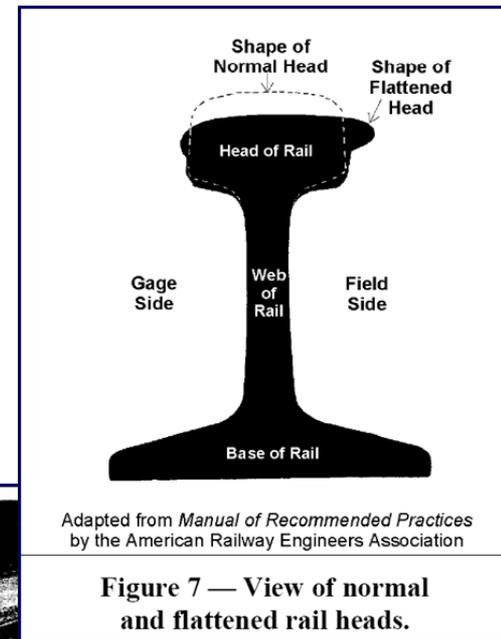
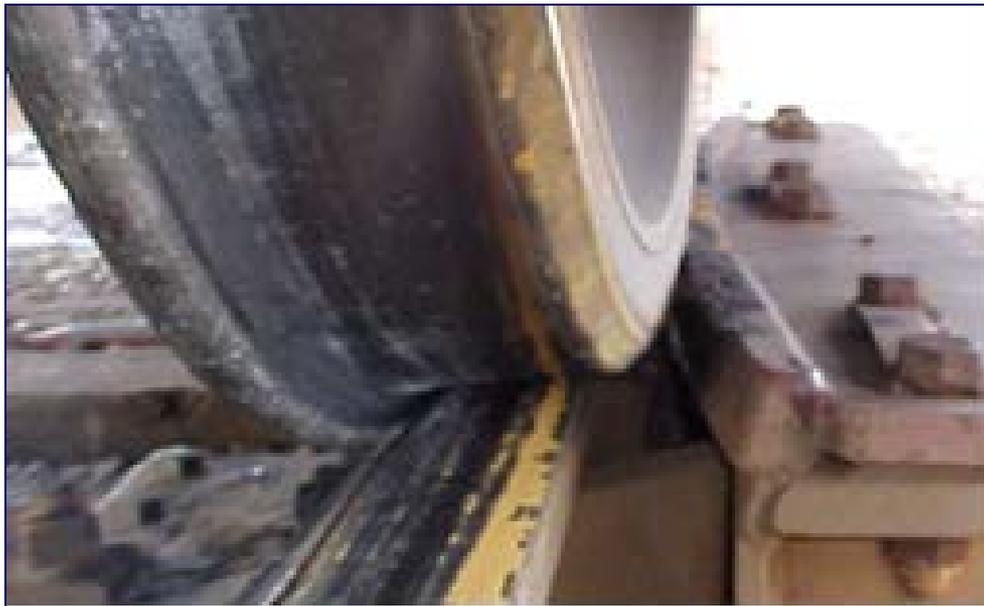


Figure 10 — Flattened rail head at initial POD (looking east).

3 Dimensional W-R Contact

Simulation Challenges

- ◆ **Multiple contact points per wheel**
- ◆ **Conformal Contact**
- ◆ **Variation of rail profile along the track**
- ◆ **Likely to require on-line calculation of WR contact, will affect computation speed**
- ◆ **Rail contacts may move relative to each other due to flexibility of track structure and components**
- ◆ **W-R contact location varies along the track**
 - Not in line with axle centerline – longitudinal offset generates additional moments
 - May also need to keep track of difference in track geometry for each contact point
- ◆ **Approximations of 3-d contact have been successful for some applications such as simple guard and restraining rails**
 - Calculate contact angle based on longitudinal offset and AOA



Along Track Variation of Rail Profiles

◆ Required for:

- Accurate simulation of worn rails in tangents, spirals and curves
 - ▲ Can have significant effect on axle steering and stability
- Switches and Crossings
- Wear and RCF studies
- Derailment investigation and problem solving

◆ Challenges:

- Implementation of smooth variations as well as step changes
- May require on-line calculation of WR contact
 - ▲ Likely to affect computation speed
 - ▲ Some codes interpolate pre-calculated WR contact tables
- How many rail profiles are required and how to calculate intermediate shapes?
- Direct input from track measurement systems
 - ▲ How to deal with "bad" data?
- How to link to flexible/moving rails?



◆ How much detail is required?

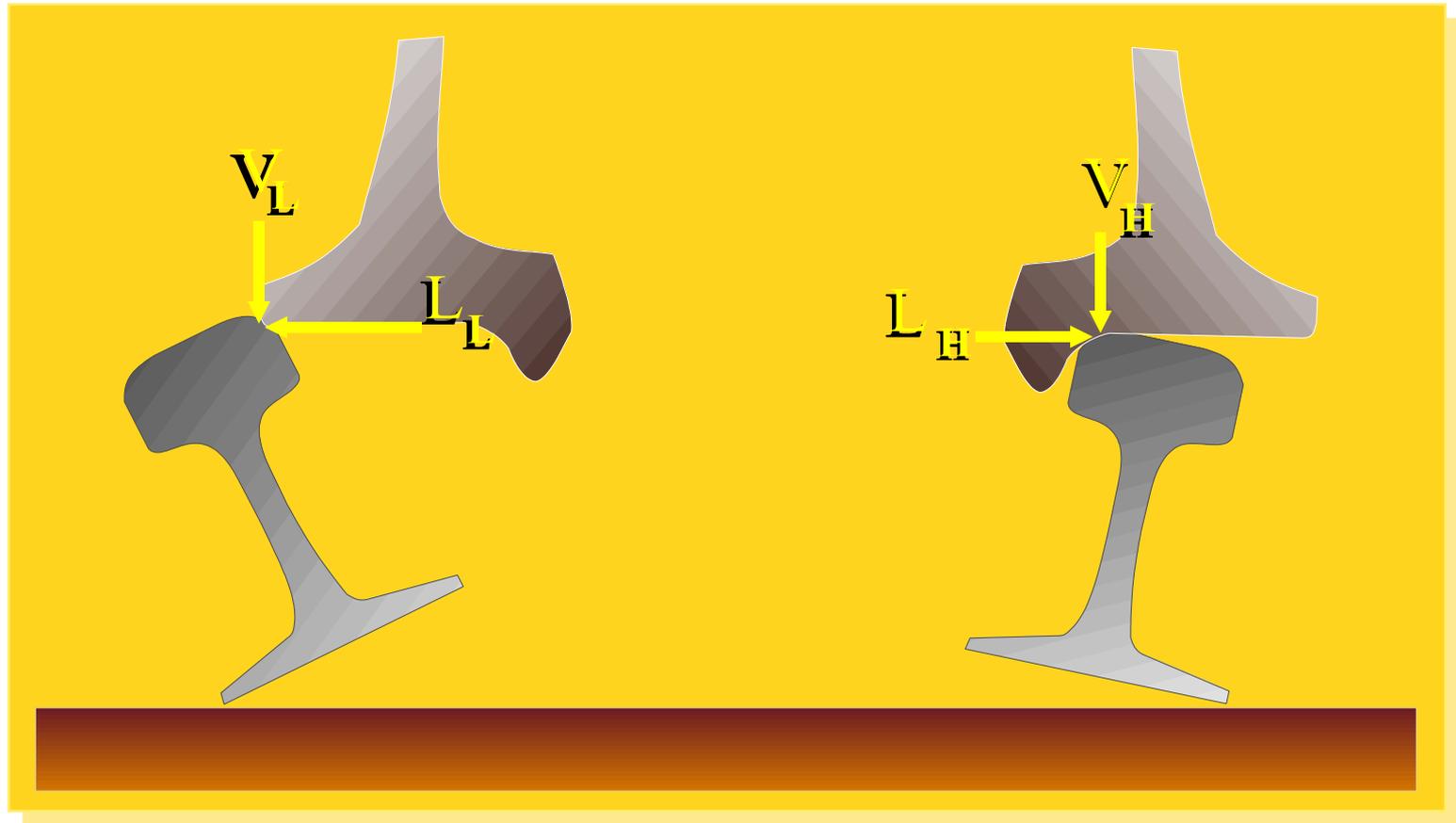
- Most vehicle simulations use simple representations of stiffness and damping between WR contact point and ground
 - ▲ Vertical and lateral motion of rails
- Reasonable approximation for many vehicle simulations
 - ▲ Massless rails with no interconnection to adjacent wheels

◆ More detail required for simulations where track dynamic response is important

- Rail roll and effects on gage widening and WR contact
- Corrugations and RCF
- Analyses of forces in track structure
- Variations in track structure
 - ▲ Missing/weak/broken components,
 - ▲ Transitions between track types
- Switches and crossings
- Adjacent axle effects on wheel load and rail stress

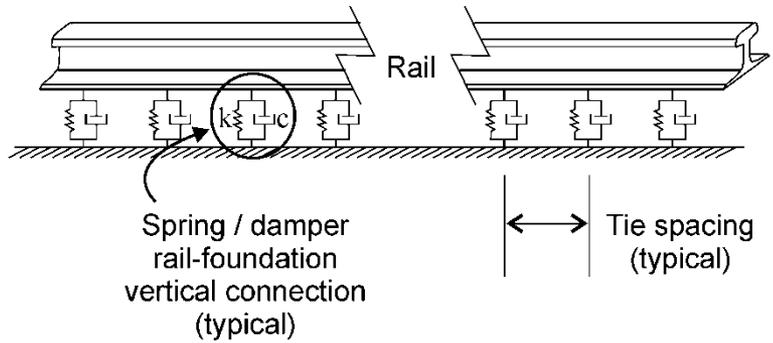


- ◆ **Requires: Rail Roll DOF in WR contact calculation, flexible rail model, detailed track fastener model**



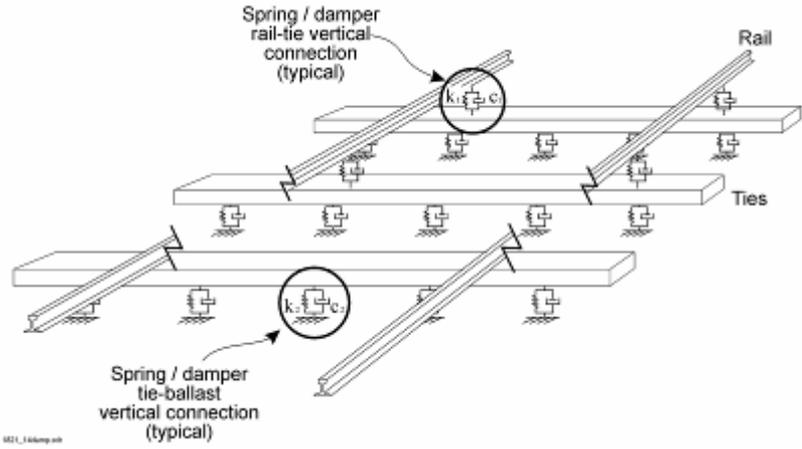
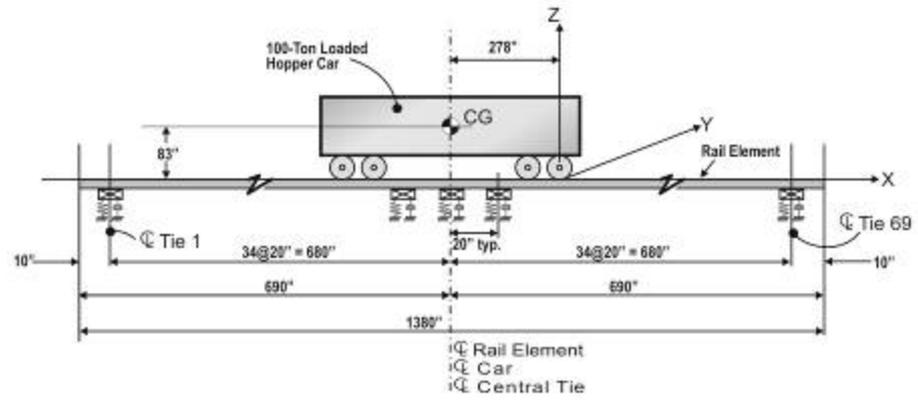


Track Structure Modeling in NUCARS[®]



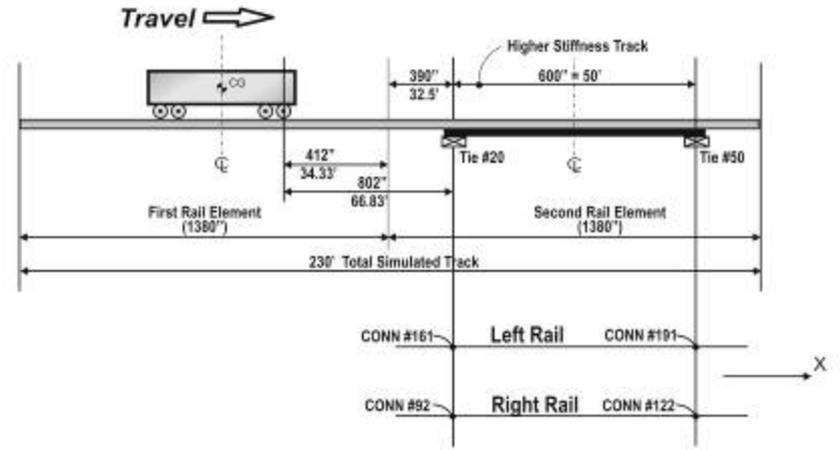
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Single layer track model



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Two layer track model



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Vehicle on infinite track with varying stiffness and damping

◆ Flexible rails

- How to simulate very long track segments?
- How to simulate varying rail cross sections, joints, gaps and breaks?
- How to simulate guard/restraining rails, switch points, and movable point frogs that move relative to running rails?
- What DOFs and how many bending modes?
 - ▲ Lateral, Vertical, Roll, Vert/Lat bending and Torsion
 - ▲ How to include Longitudinal?

◆ Rail fastener modeling

- Non-uniform fasteners: Broken, missing, weak, change in fastener type along the track
- Linear stiffness and damping is not sufficient!
- Cut spikes may require gaps and a friction model

◆ Ties

- Flexible ties: What DOFs and how many modes?
- Special ties: Ladders and dog-bones
- Uneven tie spacing
- Ties with principal axis not perpendicular to rail, such as ties in frog area

◆ Ballast and subgrade

- How to represent distributed support?
 - ▲ NUCARS® uses multiple point loads
- Effects of compaction
- Variation in stiffness/damping along track
- Non-uniform spacing

◆ Other Track Elements

- Bridges
 - ▲ Simple spans vs complex structures
- Bridge abutment effects
- Slabs, including floating slabs
- May require FEA mode shape input or in-line link to FEA software

◆ Moving Ground Plane

- Earthquakes
- Floating bridges
 - ▲ Recent work by TTCI for Sound Transit has demonstrated viable approach for linking Vehicle Dynamics analyses that include track models to FEA models of movable objects such as a floating bridge

- ▲ Ketchum, C., Cooper, T., Foan, A., Joy, R., Sederat, H., Sleavin, J., "Dynamic Simulations in Support of Installation of Light Rail Tracks on the Homer H. Hadley Memorial Floating Bridge," April 2015, The Stephenson Conference Research for Railways, ImechE London



◆ Prediction of Worn Wheel and Rail Profiles Shapes

- Iterative simulations over route with representative selection of curves and tangents
- Methodology has been demonstrated with some success by Shu and others, needs considerable refinement
 - Shu. X., Dembosky, M.A., Urban, C.L., Wilson, N.G., "RAIL WEAR SIMULATION AND VALIDATION," Proceedings of 2010 Joint Rail Conference, JRC 2010, Paper JRC2010-36189, Urbana, IL, April 27-29, 2010
- Apply wear to wheels and rails based on distribution of energy dissipated across the contacting surfaces
 - ▲ Simple linear wear index models may not be sufficient
- Improved calculation of conformal contact, interfacial layers ETC, may be required
- Dynamic rail motions (such as roll) likely to affect results

Other Modeling Challenges

continued

◆ Simulation/calculation methods

- Alternative integration methods
 - Need to accommodate sudden step changes in state such as gaps, stick-slip friction, loss of WR contact, impact forces (WR and other)
 - Euler methods have been reliable but may be slow
- Stochastic modeling, parametric studies using monte-carlo methods
 - ▲ Determine vehicle and system performance envelopes based on component design and wear tolerances
 - ▲ Will require automated analyses of large data bases of results
- Direct links for interactive computing with other software such as FEA

