

Evaluation of Performance Based Concrete for Bridge Decks

WA-RD 845.1

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EVALUATION OF PERFORMANCE BASED CONCRETE FOR BRIDGE DECKS



**Washington State
Department of Transportation**



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- Appendix C – Multi-Span Prestressed Girder Bridges
- Appendix D – Multi-Span Steel Plate Girder Bridges

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EXECUTIVE SUMMARY

This report documents the effectiveness of the changes made to the Washington State Department of Transportation (WSDOT) concrete specifications for bridge decks. The bridge deck concrete specifications were revised to eliminate or reduce early-age restraint cracking in bridge decks. Restraint cracking is caused by length changes due to shrinkage or temperature effects that are restrained by girders and internal reinforcement and show up primarily as transverse through cracks. Many of the revisions came from recommendations from the WA-RD Report 747.1 “Mitigation Strategies for Early-Age Shrinkage Cracking in Bridge Decks.” Bridge decks constructed with this revised concrete specification are commonly referred to as “Performance Based Bridge Decks.”

The undersides of 28 bridge decks were visually inspected for cracks; 15 were constructed using the performance based specification, and 13 were constructed using the traditional WSDOT specification. The information gathered is converted into “crack intensity” diagrams. These diagrams illustrate the severity and location of cracking for each bridge deck.

In general, the performance based concrete specification resulted in fewer visible cracks in bridge decks than the traditional concrete specification. A few of the traditional bridge decks performed similar to the performance based bridge decks, but this appears to be the exception, not the rule. Only one of the performance based concrete decks had a high intensity of cracking. It is unclear what contributed to the poor performance of this particular bridge deck.

What is apparent from this study is that cracking of bridge decks is variable within the same bridge. In some cases, it appears to be variable within the same concrete placement. This indicates that there are many variables that affect the cracking performance of a bridge deck that change during the construction of the bridge.

A secondary objective of this study was to identify trends or issues with the current performance based specification that could be improved. Mix design, test data and temperature information was gathered for the performance based bridge decks evaluated in this study. No correlation could be made between this data and crack intensity; however, improvements in data collection on future projects may provide better data to identify trends or issues.

Ultimately, based on this study, no significant changes to the bridge deck concrete specifications are necessary. Some minor changes related to quality of data submitted by Contractors may be beneficial to identify possible improvements in performance limits identified in the specification.

OVERVIEW

The objective of this report is to evaluate and document the effectiveness of the changes made to the Washington State Department of Transportation (WSDOT) concrete specification for bridge decks. The WSDOT revamped the bridge deck concrete specifications in an effort to eliminate or reduce early-age restraint cracking in bridge decks. Restraint cracking is caused by length changes due to shrinkage or temperature effects that are restrained by girders and internal reinforcement and show up primarily as transverse through cracks. Many of the revisions came from recommendations from the WA-RD Report 747.1 “Mitigation Strategies for Early-Age Shrinkage Cracking in Bridge Decks.” Bridge decks constructed with this revised concrete specification are commonly referred to as “Performance Based Bridge Decks.”

The term “Performance Based” is used because the revised specification removes prescribed requirements (minimum cement content, use of fly ash, etc.) and adds performance criteria such as shrinkage and permeability limits. Contractors are required to submit test results to prove their concrete mix design meets the specified performance requirements.

The performance based specification was first implemented in mid-2011. Since then, 30+ bridges have been constructed using project specific specifications as well as a handful of bridge deck replacements. The performance based specification is now included in the WSDOT 2014 Standard Specifications (as amended April 6, 2015).

To evaluate the effectiveness of the revised concrete specification, a sample of bridges recently constructed with the performance based specification and the traditional specification have been visually inspected for cracks. This inspection data has been used to judge the severity or intensity of cracking for each bridge deck. The cracking severity is used to compare the bridges and can be used to draw conclusions on the effectiveness of the revised specification to prevent or reduce early-age restraint cracking in the bridge decks.

A secondary objective is to identify any improvements that could be made to the current performance based specification. To facilitate this, the concrete mix design, test results and temperature data submitted by Contractors is collected. This data is then used to identify possible trends that correlate to the cracking performance of the bridge decks.

DECK CONCRETE SPECIFICATION

In April of 2010 WA-RD Report 747.1 “Mitigation for Early-Age Shrinkage Cracking in Bridge Decks” was published and was used to revise the WSDOT specification for bridge deck concrete which is classified as Class 4000D. The 2014 WSDOT Standard Specifications includes revisions to the following sections:

- 6-02.3(2)A – Contractor Mix Design
- 6-02.3(10)D – Concrete Placement, Finishing, and Texturing [for Bridge Decks]
- 6-02.3(11) – Curing Concrete

CONTRACTOR MIX DESIGN

The revisions to the “Contractor Mix Design” remove some of the prescriptive requirements and replace them with performance based requirements. The most significant prescriptive requirement that was removed was the requirement for a minimum cementitious content for the Class 4000D concrete. The previous specification contained a requirement that the 4000D concrete was to contain a minimum of 660 lbs of cement and 75 lbs of fly ash (for a total of 735 lb cementitious material). The revised specification no longer has a minimum cementitious content and does not require the use of fly ash.

The performance based requirement for minimum concrete compressive strength at 28 days remains in the specification as 4,000 psi. Added were performance limits on permeability, length change (“shrinkage”) and scaling (as well as an optional requirement for freeze-thaw durability to reduce prescribed air content). In addition to the performance limits, modulus of elasticity and density are required to be provided (but no limits attached).

Another significant change resulting from recommendations of WA-RD Report 747.1 was to increase the aggregate size. The nominal maximum aggregate size increased from 1” to 1½”. Note that the nominal maximum aggregate size changed from ¾” in the 2008 WSDOT Standard Specifications to 1” in the 2010 WSDOT Standard Specifications.

See Table 1 for a summary of the revisions to the Class 4000D specification.

Table 1 - Summary of 4000D Concrete Specifications

	Original Class 4000D	Revised Class 4000D
Minimum 28-day Compressive Strength	4,000 psi	4,000 psi
Cement	Type I or II Portland	Type I or II Portland
Cementitious Content	735 lbs minimum (660 lbs cement & 75 lbs fly ash)	No set limits
Fly Ash	Required	Optional
Nominal Max. Aggregate Size	1-inch	1½-inch
Water Reducing Admixture	Required	Optional
Air Content	4.5% to 7.5%	4.5% to 7.5%
Freeze-Thaw Durability Test (instead of above air content requirement)	Not an Option	3.0% min. air content 90% minimum durability factor after 300 cycles per AASHTO T 161
Permeability	No Requirement	Less than 2000 coulombs at 56 days per AASHTO T 277
Length Change (“shrinkage”)	No Requirement	Less than 0.032% (320 microstrain) at 28 days per AASHTO T 160
Scaling	No Requirement	Visual rating ≤ 2 after 50 cycles per ASTM C 672
Modulus of Elasticity	No Requirement	Measured and Submitted per ASTM C 469
Density	No Requirement	Measured and Submitted per ASTM C 138

The overall intent of the changes to the Class 4000D mix design is to focus on the behavior (or performance) of the concrete rather than providing a set “recipe.” This puts more burdens on the Contractor and concrete supplier but allows for more flexibility and provides more information on the actual properties of the concrete being placed.

CONCRETE PLACEMENT, TEXTURING AND CURING

In addition to revisions to the mix design, changes were made to the placement, finishing and texturing portions of the specification. The ultimate goal of these revisions is to begin adequate wet curing as soon as possible. The original specifications for placing and texturing typically resulted in a delay of application of wet burlap to the surface of the bridge deck. This delay occurred because the texturing was done by tining transverse grooves with a metal comb and could not occur until the concrete was sufficiently stiff. After the bridge deck was tined, curing compound was applied. When the deck had taken initial set, the presoaked burlap and soaker hoses were applied and kept in place for 14 consecutive days.

Revisions to the curing portion of the specification require fogging of the deck immediately after the finishing machine passes “maintaining a wet sheen without developing pooling or sheeting water” (see Figure 1). Tining of the bridge deck is eliminated and presoaked burlap is applied almost immediately “without damaging the finish, other than minor marring of the concrete surface” (see Figure 2). The use of curing compound is explicitly forbidden. Fogging shall continue until the concrete has achieved initial set when soaker hoses are added (See Figure 3). The wet burlap and soaker hoses remain in place for 14 consecutive days.



Figure 1 - Fogging of Bridge Deck



Figure 2 - Application of Presoaked Burlap



Figure 3 - Burlap and Soaker Hoses

Since the bridge deck is not textured before the wet burlap is applied (see Figure 4), it has to occur after the concrete has hardened. This is achieved through the use of “diamond tipped saw blades mounted on a power driven, self-propelled machine that is designed to texture concrete surfaces” (see Figure 5). The revised specification results in a bridge deck that has longitudinal grooves instead of transverse grooves provided by a metal comb (see Figure 6).



Figure 4 - Bridge Deck Surface after Curing



Figure 5 - Bridge Deck Texturing Machine



Figure 6 - Finished Bridge Deck Texture

BRIDGE DECK TEMPERATURE

Another change to the Class 4000D specification requires the concrete temperature at the time of placement to be between 55°F and 75°F. The original specification limited concrete placement temperature between 55°F and 90°F. The goal of this revision is to reduce the peak temperature of the concrete during placement and curing. Concrete typically heats up as it sets and hardens (see Figure 7). If concrete temperature is much higher than ambient temperature when it achieves initial set, stresses will be locked in which could cause cracking.

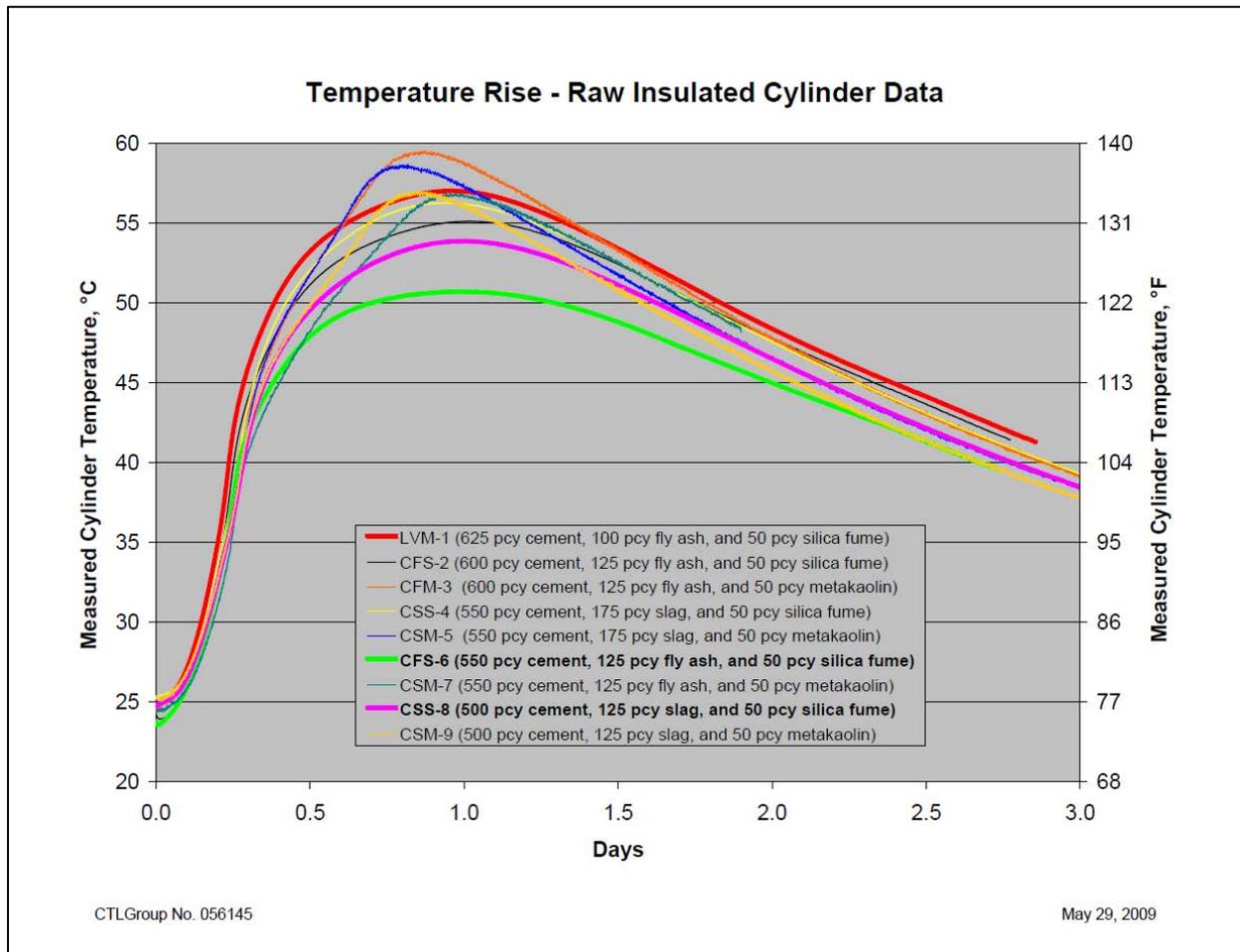


Figure 7 - Example of Concrete Temperature Rise (from "SR 520 – ACME Project Final Findings Report")

Additionally, requirements were added to monitor the temperature of the bridge deck concrete for 7-days after concrete placement. This is done by embedding temperature monitoring devices in the bridge deck and recording temperatures hourly. Ambient temperature is also recorded from monitoring devices placed near the locations of the monitors embedded in the concrete. The Contractor is then required to submit this data to WSDOT; however, no other contractual limits are placed on this information.

BRIDGE DECK EVALUATION METHOD

The main issue that drove the revisions to the Class 4000D bridge deck concrete specifications is the presence of highly visible cracks on the roadway surface and the underside of bridge decks between girder flanges and in the overhangs. Therefore, “cracking severity” is used as the measure of success for bridge deck concrete.

Cracks on the underside of bridge decks are generally easier to see than those on the top (primarily due to effloresce or “leaching” seen). Cracks on the top of bridge decks can be easily seen after a rain when the deck is drying out. However, this would require careful timing of inspections as well as traffic control. To quickly and easily evaluate deck cracking, visible cracks in the underside of decks between the girders are used to evaluate deck cracking. Cracking in the underside of the overhangs or top of deck are not quantified for this evaluation

To quantify the severity of deck cracking, easily visible cracks are counted on the underside of the deck and converted to “crack intensity” percentage. 100% crack intensity is set as transverse cracks spaced at an average of 2-feet on center. Each bridge is divided up into “bays” which are bounded by girders and diaphragms (or cross-frames for the steel bridges), see Figure 8. The number of cracks for 100% crack intensity is equal to the length of the bay divided by 2-feet. A crack intensity for each bay is calculated by dividing the number of cracks counted (N_{CR}) by the number of cracks for 100% crack intensity (N_{100}). An example of the resulting Crack Intensity Diagram is shown in Figure 9.

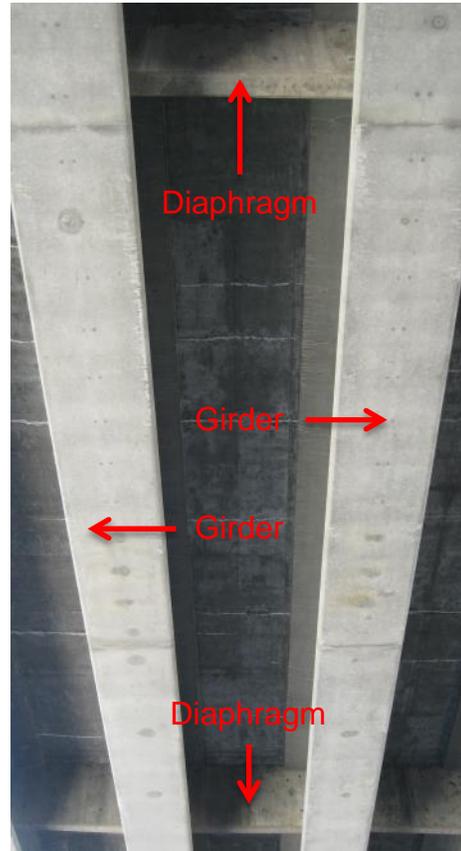


Figure 8 - Example of a “Bay”

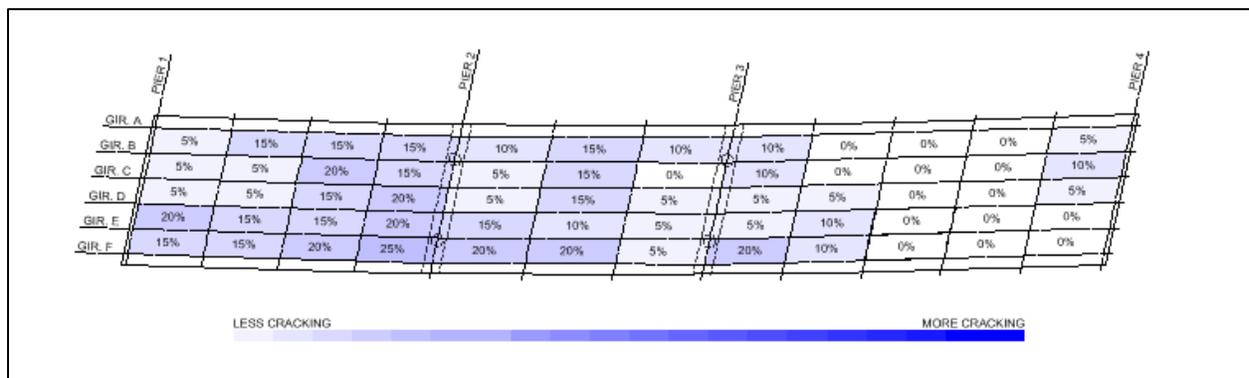


Figure 9 - Crack Intensity Diagram Example

In reality, the cracking in a “bay” is not always uniformly spaced. Sometimes a few cracks are closely spaced, but concentrated in a small portion of the “bay” (see Figure 10). Other times they are more uniformly spaced throughout (see Figure 11). This information is lost in the above diagrams as this evaluation method assumes the cracks are uniformly distributed along the length of the “bay.”



Figure 10 - Non-uniform Spaced Cracks



Figure 11 - Uniformly Spaced Cracks

BRIDGES FOR EVALUATION

The criteria for the bridges chosen for this study were:

- Constructed in 2008 or later
- Visibility of the underside of deck
- Relatively easy access
- Relatively simple geometry

A total of 28 bridges were inspected and evaluated; 15 were constructed using the performance based specification and 13 were constructed using the traditional WSDOT specification. Throughout this report the bridges are color coded; red is used for “Traditional” bridge decks, and green is used for “Performance Based” bridge decks.

Prestressed I-girders and steel plate I-girders were selected for the ability to inspect the underside of the decks between girders. Deck bulb-T girders appear to be more common in recent years, and several have been constructed with a performance based topping slab, but these were not included because the underside of the decks are not visible.

The bridges were sorted into four “trips” to different geographical regions which are described in the following sections.

SOUTH TRIP

The bridges included in this trip are in the Centralia area primarily along I-5, as shown in Figure 12. The inspection of these bridges was performed on 4/8/2015.



Br. No.	Bridge Name	Str. ID	Contract	Region	Contractor	Year	Perform.
5/302E	PRAIRIE CREEK NB	0017465A	7465	OR	Scarsella Bros.	2009	No
5/302W	PRAIRIE CREEK SB	0017465B	7465	OR	Scarsella Bros.	2010	No
5/229	MELLEN STREET COUPLER	0018473B	8473	SW	Scarsella Bros.	2014	Yes
5/234W	I-5 OVER BLAKESLEE JCT RR	0018272C	8272	SW	Cascade Bridge	2013	Yes
5/232SCD	SKOOKUMCHUCK RIVER SCD	0018272B	8272	SW	Cascade Bridge	2013	Yes
5/232NCD	SKOOKUMCHUCK RIVER NCD	0018272A	8272	SW	Cascade Bridge	2013	Yes
6/115	S FORK CHEHALIS R	0017587A	7587	SW	Scarsella Bros.	2009	No

Figure 12 - Map of South Trip Bridges

WEST TRIP

The bridges included in this trip are in the Willapa Bay area near the coast, as shown in Figure 13. The inspection of these bridges was performed on 5/7/2015.



Br. No.	Bridge Name	Str. ID	Contract	Region	Contractor	Year	Perform.
105/3	SMITH CREEK	0018345A	8345	SW	Scarsella Bros., Inc.	2013	Yes
105/4	NORTH RIVER	0018345B	8345	SW	Scarsella Bros., Inc.	2014	Yes
101/44	BONE RIVER	0018292A	8292	SW	Cascade Bridge, LLC	2013	Yes
101/31	MIDDLE NEMAH RIVER	0018344A	8344	SW	SB Structures, LLC	2014	Yes
6/8	WILLAPA RIVER	0018464A	8464	SW	Rotschy, Inc.	2014	Yes

Figure 13 - Map of West Trip Bridges

EAST TRIP

The bridges included in this trip are near the Keechelus Lake and Spokane areas along I-90, as shown in Figure 14. The inspection of these bridges was performed on 5/20/2015 and 5/21/2015.



Br. No.	Bridge Name	Str. ID	Contract	Region	Contractor	Year	Perform.
90/106N	GOLD CREEK WB	0017852D	7852	SC	Max J. Kuney Company	2012	No
90/105.5N	GOLD CREEK ANIMAL CROSSING WB	0017852B	7852	SC	Max J. Kuney Company	2012	No
90/105.5S	GOLD CREEK ANIMAL CROSSING EB	0017852A	7852	SC	Max J. Kuney Company	2010	No
195/117	CHENEY SPOKANE RD OVER US 195	0018378A	8378	ER	Selland Construction	2014	Yes
395/441N-E	N-E RAMP OVER N-N RAMP	0017610E	7610	ER	Graham Construction & Manage.	2011	Yes
2/651W-S	W-S RAMP OVER US 2/US 395	0017610D	7610	ER	Graham Construction & Manage.	2011	No
395/442W	US 395 OVER US 2	0017610B	7610	ER	Graham Construction & Manage.	2011	No

Figure 14 - Map of East Trip Bridges

NORTH TRIP

The bridges included in this trip are near Tacoma, Bremerton and Marysville areas, as shown in Figure 15. The inspection of these bridges was performed on 5/21/2015, 5/22/2015 and 5/29/2015.



Br. No.	Bridge Name	Str. ID	Contract	Region	Contractor	Year	Perform.
5/434SCD	SBCD OVER SR 16 HOV & RAMPS	0018189B	8189	OR	Mowat Construction Company	2013	Yes
16/3W	SR 16 OVER HOV	0018189A	8189	OR	Mowat Construction Company	2014	Yes
16/7S-E	S SPRAGUE RAMP	0017594E	7594	OR	Guy F. Atkinson Construction	2010	No
303/4A	MANETTE BRIDGE	0017926A	7926	OR	Manson-Mowat, A Joint Venture	2011	No
2/8.5N-W	N-W RAMP (BICKFORD AVE) OVER US 2	0018286A	8286	NW	Granite Construction Company	2013	Yes
529/25	EBEY SLOUGH	0017948A	7948	NW	Granite Construction Company	2012	No
9/133	SR 9 OVER HARVEY CRK RD	0017267A	7267	NW	Scarsella Bros., Inc.	2008	No
9/134	PILCHUCK CREEK	0018363A	8383	NW	Granite Construction Company	2014	Yes

Figure 15 - Map of North Trip Bridges

BRIDGE DECK SUMMARIES

The cracking of each bridge was evaluated as described in the previous section and grouped into the following categories:

- Single Span Prestressed Girder Bridges
- Two-Span Prestressed Girder Bridges
- Multi-Span Prestressed Girder Bridges
- Multi-Span Steel Plate Girder Bridges

Summaries of each bridge are included in the following sections. For more information on each bridge, see Appendices A through D.

SINGLE SPAN PRESTRESSED GIRDER BRIDGES

Table 2 summarizes and ranks the average crack intensity for each of the single span prestressed girder bridges evaluated. See Appendix A for more information.

Table 2 - Single Span Prestressed Bridge Summary

Br. No.	Bridge Name	Contract	Year	Perform.	Intensity	Cement.	Shrink.
90/105.SS	GOLD CREEK ANIMAL CROSSING EB	7852	2010	No	40%	735	--
90/105.SN	GOLD CREEK ANIMAL CROSSING WB	7852	2012	No	32%	735	--
5/302E	PRAIRIE CREEK NB	7465	2009	No	18%	735	--
9/133	SR 9 OVER HARVEY CRK RD	7267	2008	No	8%	735	--
5/302W	PRAIRIE CREEK SB	7465	2010	No	4%	735	--
5/229	MELLON STREET COUPLET	8473	2014	Yes	< 1%	580	0.028%
101/31	MIDDLE NEMAH RIVER	8344	2014	Yes	0%	610	0.018%

The bridge decks for single span prestressed girder bridges are typically placed in one placement from abutment to abutment.

BRIDGES 90/105.5S & 90/105.5N (GOLD CREEK ANIMAL CROSSING)

These bridges are parallel bridges carrying I-90 over an animal crossing in Kittitas County. Bridge 90/105.5S was constructed in 2010 and Bridge 90/105.5N was constructed in 2012. Both bridges were constructed as part of the **I-90 Hyak to Snowshed Vicinity Phase 1B – Add Lanes and Bridges** contract. The contract used the 2008 WSDOT Standard Specifications which include the **traditional** bridge deck concrete requirements. See Figures 16 & 17 for the crack intensity diagrams for these bridges. See Figure 18 for pictures depicting the range of cracking represented by the crack intensity diagrams. Both of these bridges are uniformly cracked with the worse cracking intensity occurring near the abutments.

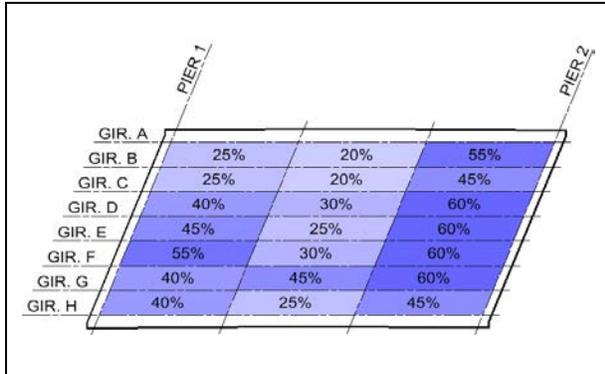


Figure 16 - Bridge 90/105.5S Crack Intensity Diagram

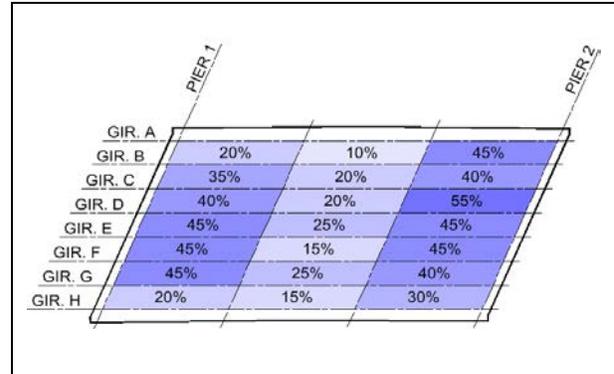


Figure 17 - Bridge 90/105.5N Crack Intensity Diagram

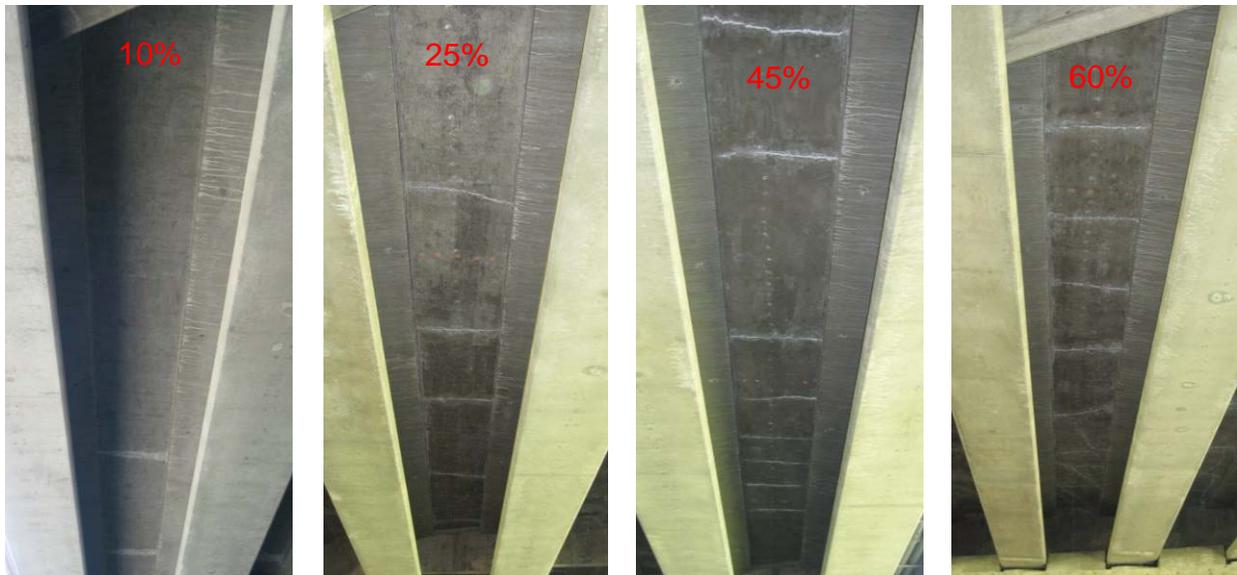


Figure 18 - Range of Deck Cracking for Bridges 90/105.5S & 90/105.5N

BRIDGES 5/302E & 5/302W (PRAIRIE CREEK)

These bridges are parallel bridges carrying I-5 over Prairie Creek in Thurston County. Bridge 5/302W was constructed in 2008 and Bridge 5/302E was constructed in 2009. Both bridges were constructed as part of the I-5 Grand Mound to Maytown Stage One – Add Lanes contract. The contract used the 2006 WSDOT Standard Specifications which include the traditional bridge deck concrete requirements. See Figures 19 & 20 for the crack intensity diagrams for these bridges. See Figure 21 for pictures depicting the range of cracking represented by the crack intensity diagrams.

Half of Bridge 5/302E performed well but the other half performed poorly. This bridge was constructed in stages with a longitudinal construction joint for staging. Bridge 5/302W performed well with relatively low cracking.

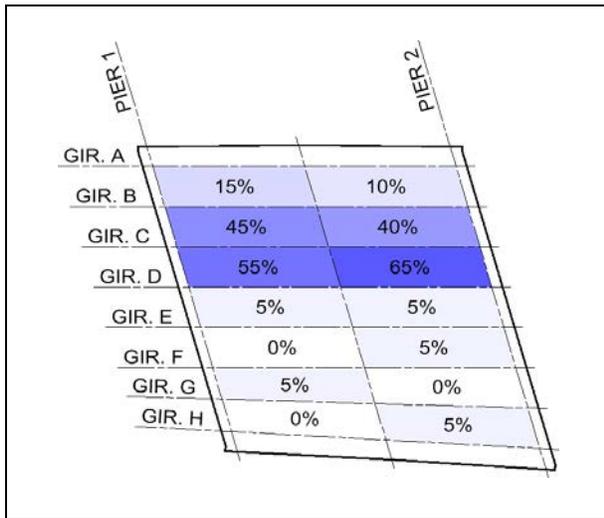


Figure 19 - Bridge 5/302E Crack Intensity Diagram

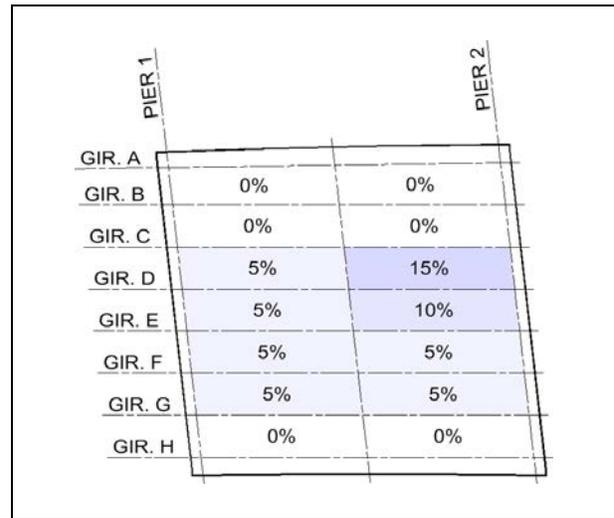


Figure 20 - Bridge 5/302W Crack Intensity Diagram



Figure 21 - Range of Deck Cracking for Bridges 5/302E & 5/302W

BRIDGE 9/133 (HARVEY CREEK ROAD)

This bridge carries SR 9 over Harvey Creek and Harvey Creek Road in Snohomish County. It was constructed in 2014 as part of the **SR 9 Schloman Road to 256th ST NE and 268th ST Intersection** contract. The contract used the 2006 WSDOT Standard Specifications which include the **traditional** bridge deck concrete requirements. See Figure 22 for the crack intensity diagram for this bridge. See Figure 23 for pictures depicting the range of cracking represented by the crack intensity diagrams. This bridge deck performed very well except for a section near Pier 1. This is a trend that showed up many times during this study.

	PIER 1		PIER 2		
GIR. A					
GIR. B	10%	0%	10%	5%	0%
GIR. C	45%	0%	0%	0%	0%
GIR. D	25%	0%	5%	5%	5%
GIR. E	35%	0%	5%	10%	5%
GIR. F	25%	0%	5%	5%	5%

Figure 22 - Bridge 9/133 Crack Intensity Diagram

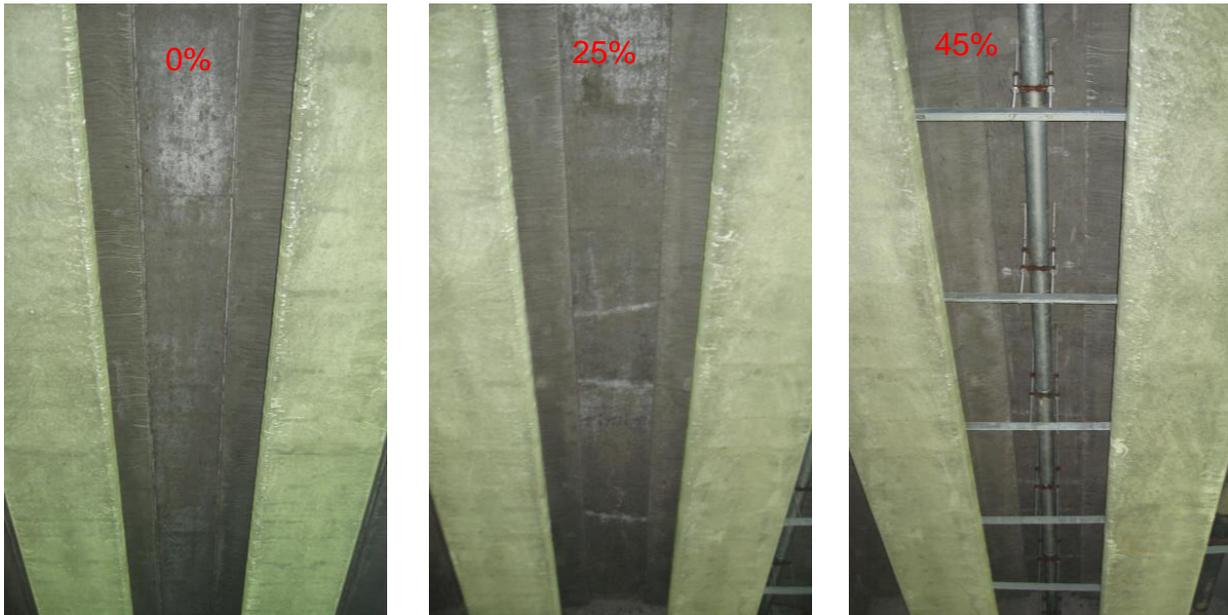


Figure 23 - Range of Deck Cracking for Bridge 9/133

BRIDGE 5/229 (MELLEN STREET COUPLET)

This bridge connects multiple ramps over I-5 in Centralia. It was constructed in 2008 as part of the **I-5 Mellen Street to Blakeslee Junction – Stage 2** contract. The contract used the 2012 WSDOT Standard Specifications with Special Provisions which include the **performance based** bridge deck concrete requirements. See Figure 24 for the crack intensity diagram for this bridge. The bays labeled “X X X” were not inspected due to limited access hindered by I-5 traffic. See Figure 25 for pictures depicting the range of cracking represented by the crack intensity diagrams (crack circled). This bridge deck performed very well with only one crack seen.

	PIER 1			PIER 2
GIR. A				
GIR. B	0%	X X X	0%	0%
GIR. C	0%	X X X	0%	0%
GIR. D	5%	X X X	0%	0%
GIR. E	0%	X X X	0%	0%

Figure 24 - Bridge 5/229 Crack Intensity Diagram



Figure 25 - Range of Deck Cracking for Bridge 5/229

BRIDGE 101/31 (MIDDLE NEMAH RIVER)

This bridge carries US 101 over the Middle Nemah River in Pacific County. It was constructed in 2014 as part of the **US 101 Middle Nemah River Br. Replace Bridge** contract. The contract used the 2012 WSDOT Standard Specifications with Special Provisions which include the **performance based** bridge deck concrete requirements. See Figure 26 for the crack intensity diagram for this bridge. See Figure 27 for pictures depicting the range of cracking represented by the crack intensity diagrams. This bridge deck had no visible cracks.

	PIER 1			PIER 2
GIR. A				
GIR. B	0%	0%	0%	0%
GIR. C	0%	0%	0%	0%
GIR. D	0%	0%	0%	0%
GIR. E	0%	0%	0%	0%

Figure 26 - Bridge 101/31 Crack Intensity Diagram



Figure 27 - Range of Deck Cracking for Bridge 101/31

TWO-SPAN PRESTRESSED GIRDER BRIDGES

Table 3 summarizes and ranks the average crack intensity for each of the two-span prestressed girder bridges evaluated. See Appendix B for more information.

Table 3 - Two-Span Prestressed Bridge Summary

Br. No.	Bridge Name	Contract	Year	Perform.	Intensity	Cement.	Shrink.
16/7S-E	S SPRAGUE RAMP	7594	2010	No	59%	735	--
195/117	CHENEY SPOKANE RD OVER US 195	8378	2014	Yes	10%	0	0.000%
395/442W	US 395 OVER US 2	7610	2011	No	10%	735	--
16/3W	SR 16 OVER HOV	8189	2014	Yes	9%	565	0.028%
2/8.5N-W	N-W RAMP (BICKFORD AVE) OVER US 2	8286	2013	Yes	6%	610	0.032%
395/441N-E	N-E RAMP OVER N-N RAMP	7610	2011	Yes	< 1%	565	0.034%

The bridge decks for two-span prestressed girder bridge decks are typically placed in two placements (one each span) with closure pours over the middle pier.

BRIDGE 16/7S-E (SOUTH SPRAGUE RAMP)

This bridge carries the ramp from SR 16 to Sprague Street as part of the Nalley Valley interchange in Tacoma. It was constructed in 2010 as part of the I-5/SR 16 WB Nalley Valley I/C contract and connects into another bridge at Pier 1. The contract used the 2008 WSDOT Standard Specifications which include the traditional bridge deck concrete requirements. See Figure 28 for the crack intensity diagram for this bridge. See Figure 29 for pictures depicting the range of cracking represented by the crack intensity diagrams. This bridge deck has very severe cracking throughout and is one of the worst looking bridge decks evaluated for this study.

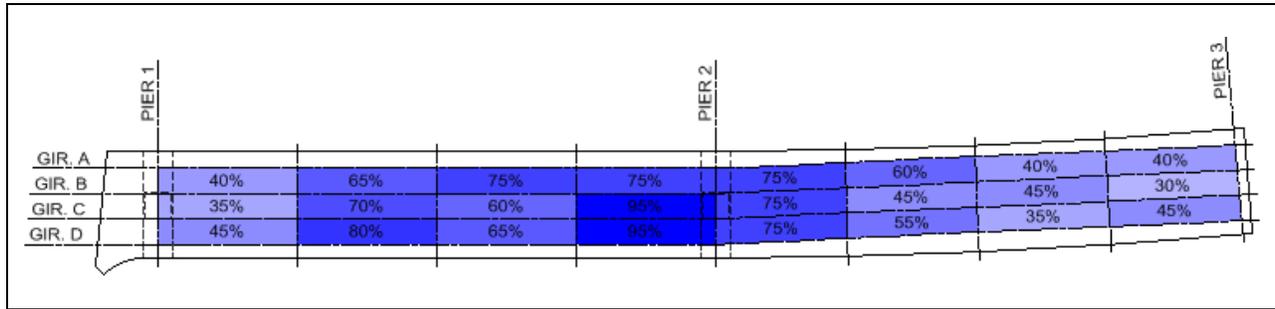


Figure 28 - Bridge 16/7S-E Crack Intensity Diagram

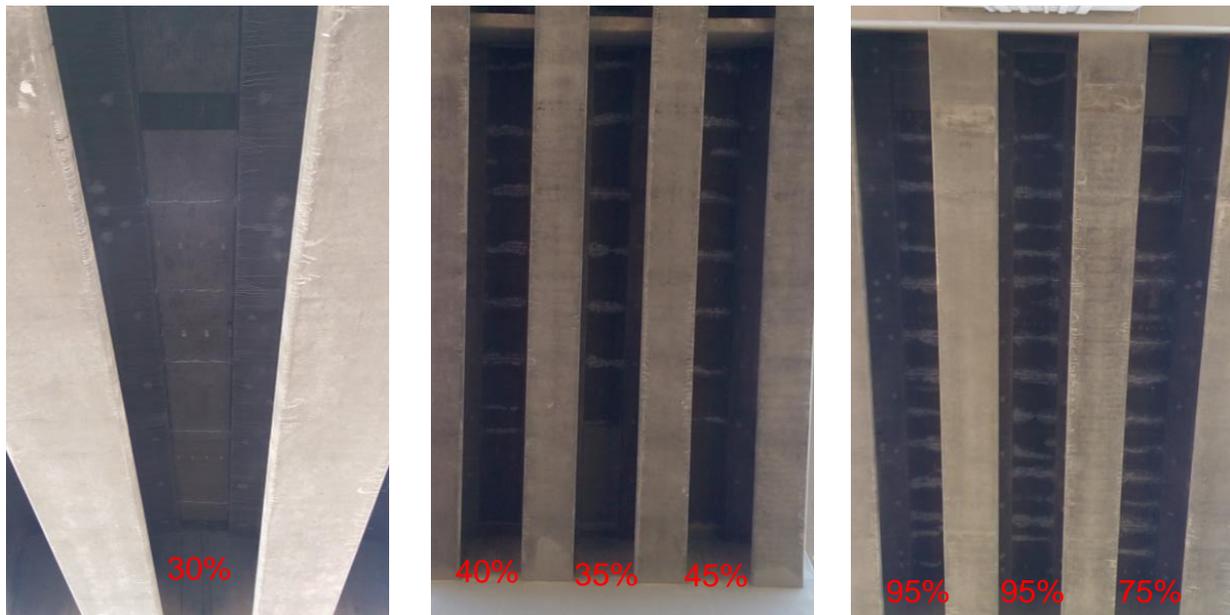


Figure 29 - Range of Deck Cracking for Bridge 16/7S-E

BRIDGE 195/117 (CHENEY-SPOKANE ROAD)

This bridge carries traffic over US 195 at the Cheney-Spokane Road Interchange in Spokane. It was constructed in 2014 as part of the **US 195 Cheney-Spokane Rd – New Interchange** contract. The contract used the 2012 WSDOT Standard Specifications with Special Provisions which include the **performance based** bridge deck concrete requirements. See Figure 30 for the crack intensity diagram for this bridge. See Figure 31 for pictures depicting the range of cracking represented by the crack intensity diagrams (cracks circled). This bridge deck performed well except for a section in Span 1 near Pier 2.

	PIER 1			PIER 2			PIER 3
GIR. A							
GIR. B	0%	10%	15%	0%	15%	5%	
GIR. C	0%	5%	35%	5%	10%	10%	
GIR. D	5%	5%	30%	10%	10%	5%	
GIR. E	5%	5%	20%	10%	5%	10%	

Figure 30 - Bridge 195/117 Crack Intensity Diagram

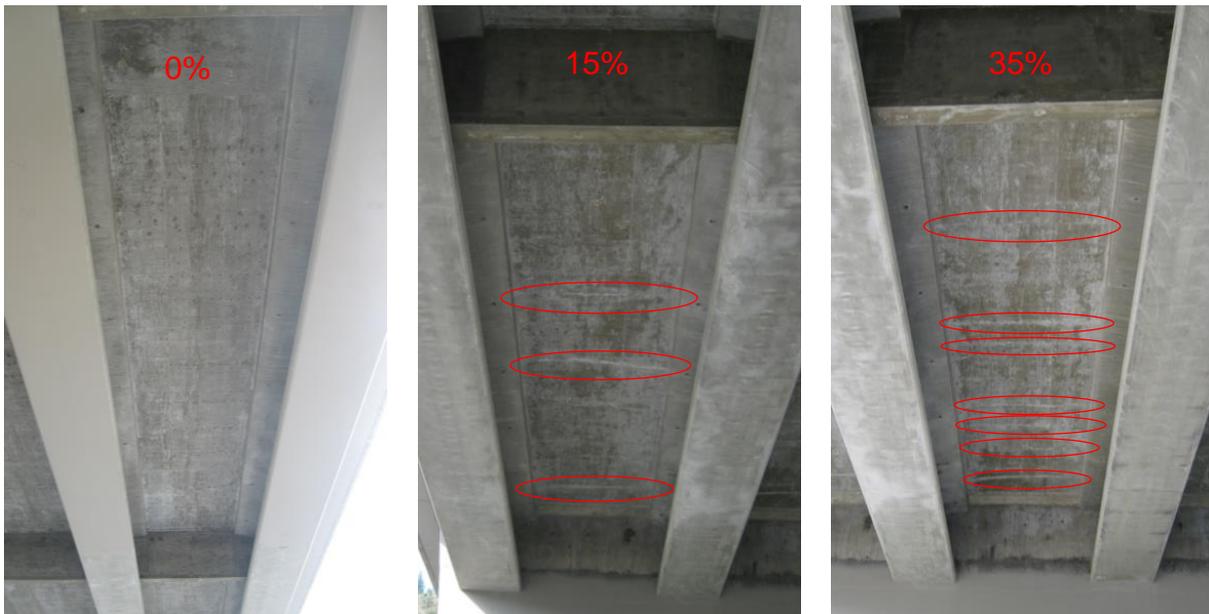


Figure 31 - Range of Deck Cracking for Bridge 195/117

BRIDGE 395/442W (US 395 OVER US 2)

This bridge carries US 395 southbound over US 2 in Spokane County. It was constructed in 2011 as part of the **US 395 NSC – US 2 Lowering** contract. The contract used the 2008 WSDOT Standard Specifications which include the **traditional** bridge deck concrete requirements. See Figure 32 for the crack intensity diagram for this bridge. See Figure 33 for pictures depicting the range of cracking represented by the crack intensity diagrams (cracks circled). This bridge deck performed well overall but had more cracking near Pier 2 in both spans.

	PIER 1		PIER 2		PIER 3	
GIR. A						
GIR. B	15%	5%	20%	25%	0%	0%
GIR. C	20%	0%	20%	30%	15%	0%
GIR. D	0%	0%	10%	10%	5%	0%

Figure 32 - Bridge 395/442W Crack Intensity Diagram



Figure 33 - Range of Deck Cracking for Bridge 395/442W

BRIDGE 16/3W (SR 16 OVER HOV)

This bridge carries traffic over the future HOV connector between I-5 and SR 16 as part of the Nalley Valley Interchange in Tacoma. It was constructed in 2014 as part of the **I-5 / SR 16 EB Nalley Valley - HOV** contract. The contract used the 2010 WSDOT Standard Specifications with Special Provisions which include the **performance based** bridge deck concrete requirements. See Figure 34 for the crack intensity diagram for this bridge. See Figure 35 for pictures depicting the range of cracking represented by the crack intensity diagrams. This bridge deck performed very well overall but had more cracking near Pier 2 in Span 1 and near the Pier 3 abutment.

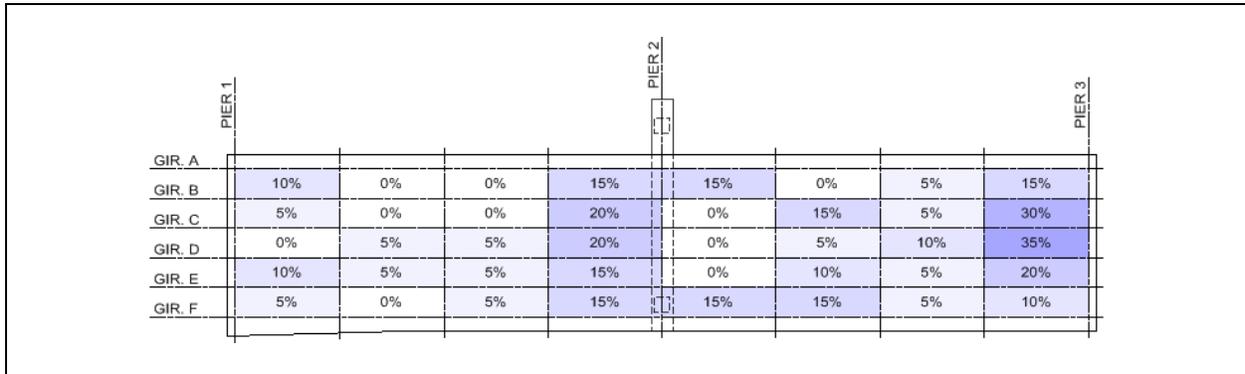


Figure 34 - Bridge 16/3W Crack Intensity Diagram



Figure 35 - Range of Deck Cracking for Bridge 16/3W

BRIDGE 2/8.5N-W (BICKFORD AVE OVER US 2)

This bridge carries traffic over US 2 at the Bickford Ave Interchange in Snohomish County. It was constructed in 2013 as part of the **US 2 Bickford Avenue I/C Safety and Culvert Replacement** contract. The contract used the 2012 WSDOT Standard Specifications with Special Provisions which include the **performance based** bridge deck concrete requirements. See Figure 36 for the crack intensity diagram for this bridge. See Figure 37 for pictures depicting the range of cracking represented by the crack intensity diagrams. This bridge deck performed well with highest cracking intensity occurring near Pier 2 in Span 1.

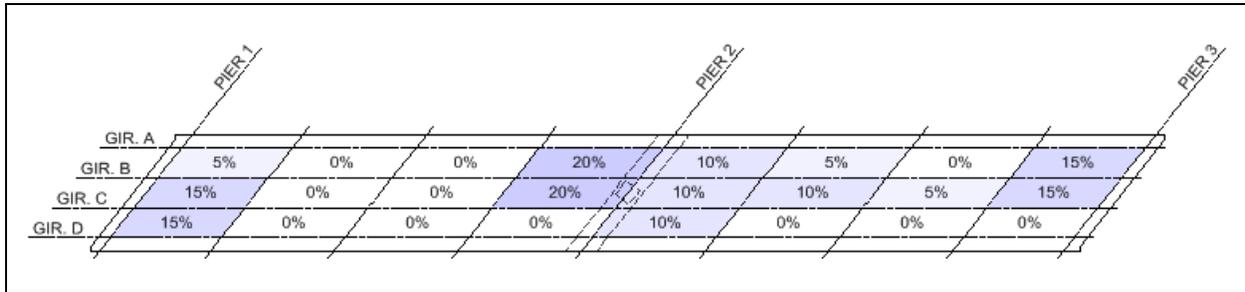


Figure 36 - Bridge 2/8.5N-W Crack Intensity Diagram



Figure 37 - Range of Deck Cracking for Bridge 2/8.5N-W

395/441N-E (N-E RAMP OVER N-N RAMP)

This bridge carries traffic from US 395 to US 2 in Spokane County. It was constructed in 2011 as part of the **US 395 NSC - US 2 Lowering** contract. The contract used the 2008 WSDOT Standard Specifications with Special Provisions which include the **performance based** bridge deck concrete requirements for this bridge only. It was the first bridge to use the revised bridge deck concrete requirements. See Figure 38 for the crack intensity diagram for this bridge. See Figure 39 for pictures depicting the range of cracking represented by the crack intensity diagrams. This bridge deck performed very well and only one small diagonal crack near the Pier 3 abutment was observed.

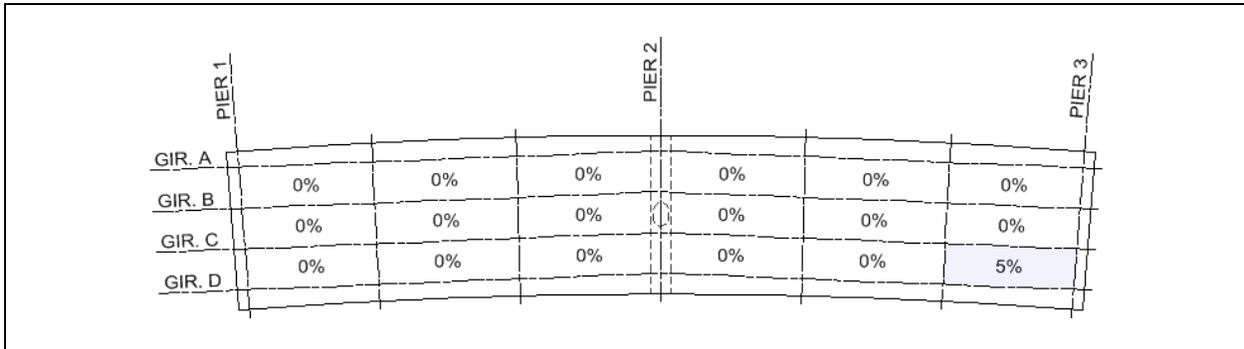


Figure 38 - Bridge 395/441N-E Crack Intensity Diagram



Figure 39 - Range of Deck Cracking for Bridge 395/441N-E

MULTI-SPAN PRESTRESSED GIRDER BRIDGES

Table 4 summarizes and ranks the average crack intensity for each of the multi-span prestressed girder bridges evaluated. See Appendix C for more information.

Table 4 - Multi-Span Prestressed Girder Bridge Summary

Br. No.	Bridge Name	Contract	Year	Perform.	Intensity	Cement.	Shrink.
303/4A	MANETTE BRIDGE	7926	2011	No	73%	735	--
90/106N	GOLD CREEK WB	7852	2012	No	44%	735	--
6/115	S FORK CHEHALIS R	7587	2009	No	32%	735	--
5/234W	I-5 OVER BLAKESLEE JCT RR	8272	2013	Yes	9%	580	0.030%
105/4	NORTH RIVER	8345	2014	Yes	7%	610	0.018%
105/3	SMITH CREEK	8345	2013	Yes	6%	610	0.018%
6/8	WILLAPA RIVER	8464	2014	Yes	5%	610	0.018%
5/232NCD	SKOOKUMCHUCK RIVER NCD	8272	2013	Yes	2%	580	0.030%
5/232SCD	SKOOKUMCHUCK RIVER SCD	8272	2013	Yes	1%	580	0.030%
101/44	BONE RIVER	8292	2013	Yes	1%	610	0.018%

Similar to the two-span prestressed girder bridges, the multi-span prestressed girder bridge decks are typically placed in multiple placements (one each span) with closure pours over the interior piers.

BRIDGE 303/4A (MANETTE BRIDGE)

This bridge connects the City of Bremerton to the neighborhood of Manette over the Port Washington Narrows. It was formerly SR 303 but is no longer part of the state route system. It was constructed in 2011 as part of the **Manette Bridge 303/4A Bridge Replacement** contract. The bridge superstructure consists of precast prestressed spliced girders with a cast-in-place bridge deck. The girder segments were post-tensioned together before the deck was placed. The contract used the 2010 WSDOT Standard Specifications which include the **traditional** bridge deck concrete requirements. See Figure 40 for the crack intensity diagram for this bridge (spans 3, 4, and 5 not shown). Cracks in Spans 2 thru 5 were not counted due to limited access, but based on a visual comparison the rest of the bridge is similar to the approaches. See Figure 41 for pictures depicting the range of cracking represented by the crack intensity diagrams. This bridge deck performed very poorly and is the worst of the bridge decks evaluated for this report.

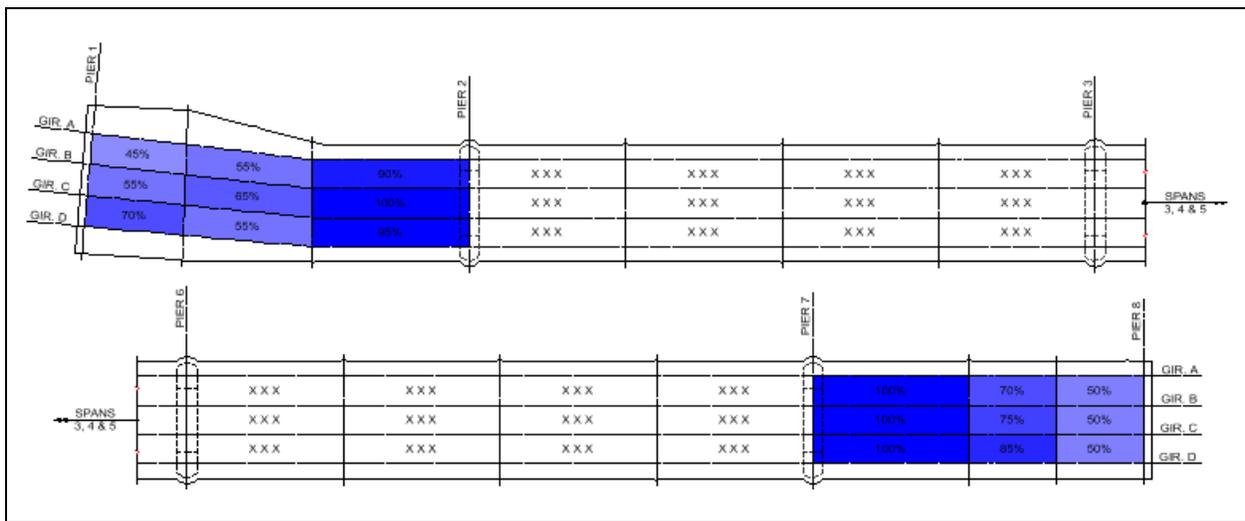


Figure 40 - Bridge 303/4A Crack Intensity Diagram

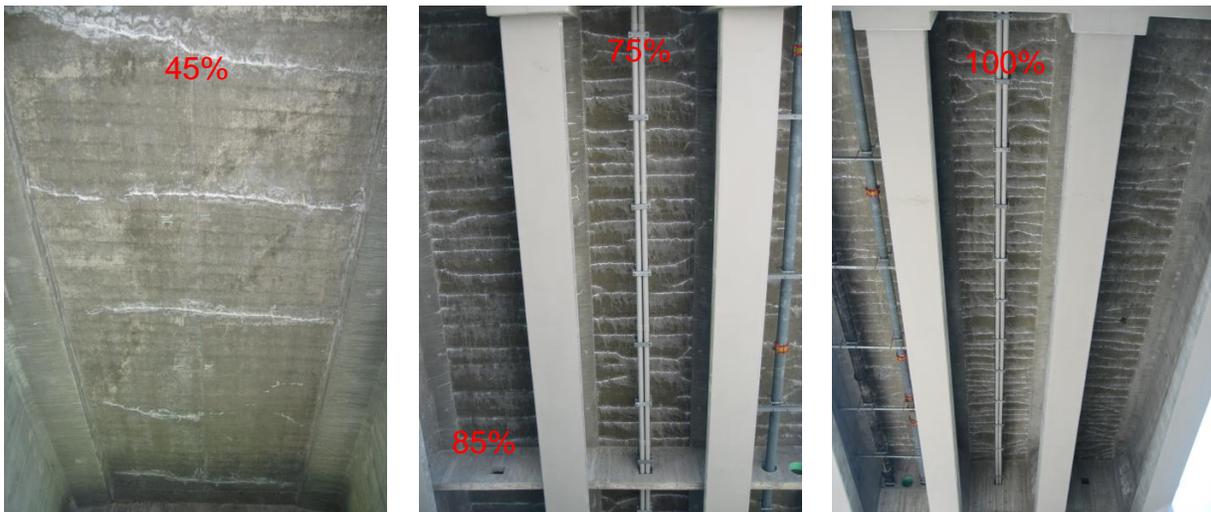


Figure 41 - Range of Deck Cracking for Bridge 303/4A

BRIDGE 90/106N (GOLD CREEK BRIDGE)

This bridge carries I-90 over Gold Creek in Kittitas County and was constructed in 2012 as part of the **I-90 Hyak to Snowshed Vicinity Phase 1B – Add Lanes and Bridges** contract. The contract used the 2008 WSDOT Standard Specifications which include the **traditional** bridge deck concrete requirements. See Figure 42 for the crack intensity diagrams for this bridge. See Figure 43 for pictures depicting the range of cracking represented by the crack intensity diagrams. This bridge deck generally performed poor to very poor. While not evaluated for this report, the parallel bridge (90/106S) was similar.

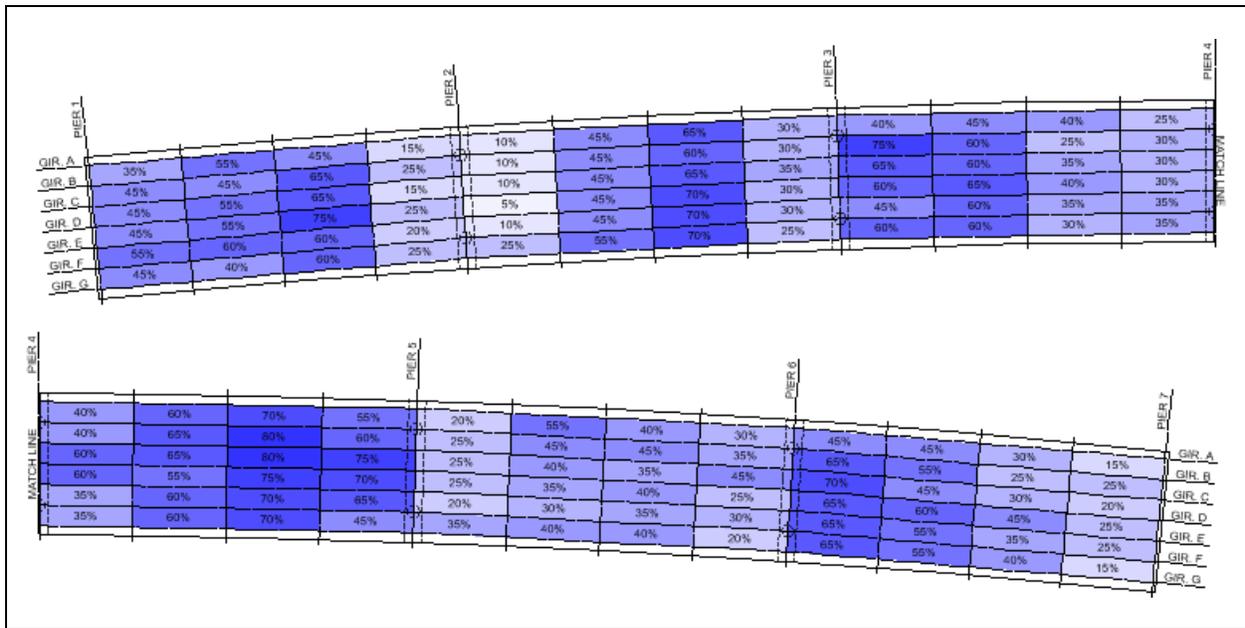


Figure 42 - Bridge 90/106N Crack Intensity Diagram

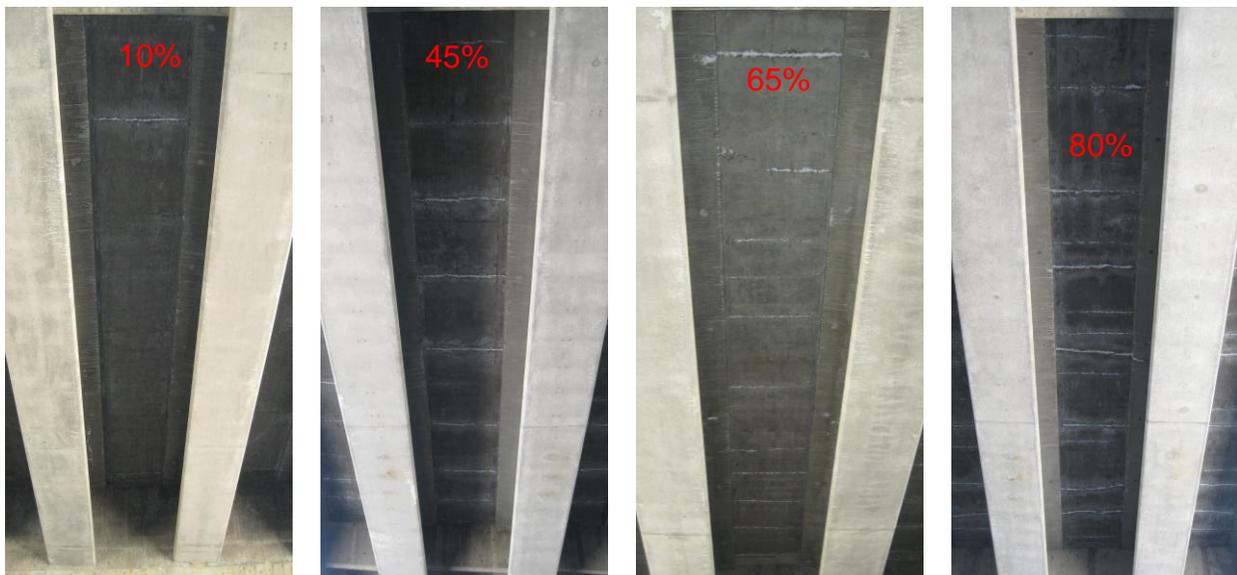


Figure 43 - Range of Deck Cracking for Bridge 90/106N

BRIDGE 6/115 (SOUTH FORK CHEHALIS RIVER)

This bridge carries SR 6 over South Fork Chehalis River in Lewis County and was constructed in 2009 as part of the **SR 6 So. Fork Chehalis River Bridge** contract. The contract used the 2008 WSDOT Standard Specifications which include the **traditional** bridge deck concrete requirements. See Figure 44 for the crack intensity diagrams for this bridge. See Figure 45 for pictures depicting the range of cracking represented by the crack intensity diagrams. This bridge deck had portions that performed well and portions that performed very poor.

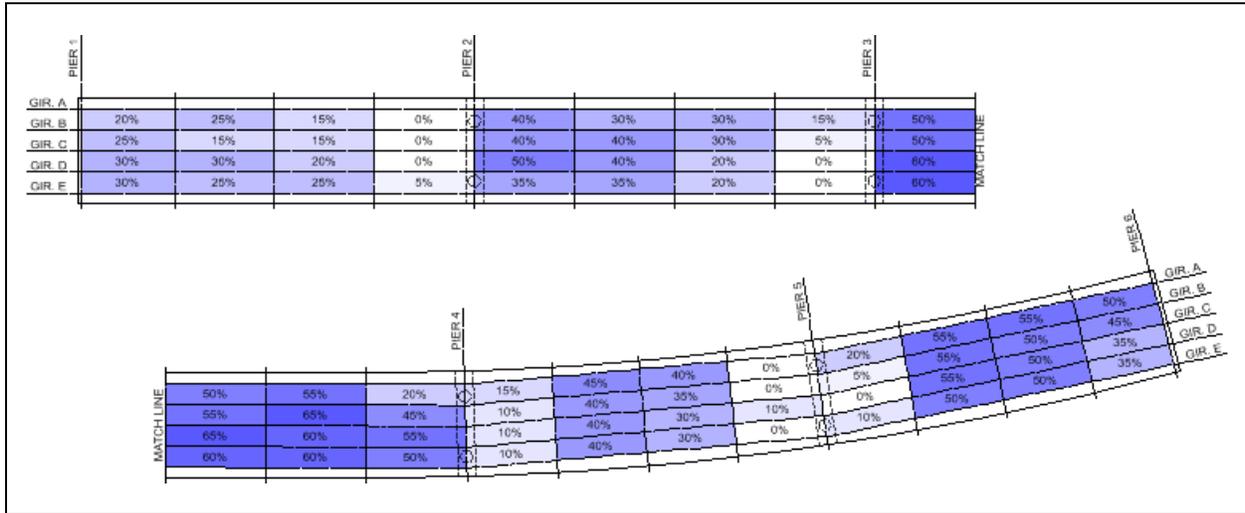


Figure 44 - Bridge 6/115 Crack Intensity Diagram



Figure 45 - Range of Deck Cracking for Bridge 6/115

BRIDGE 5/234W (I-5 OVER BLAKESLEE RAILROAD JUNCTION)

This bridge carries southbound I-5 over West Reynolds Avenue in Centralia. It was constructed in 2013 as part of the **I-5 Mellen Street to Blakeslee Junction – Stage 1** contract. The contract used the 2012 WSDOT Standard Specifications with Special Provisions which include the **performance based** bridge deck concrete requirements. See Figure 46 for the crack intensity diagram for this bridge. See Figure 47 for pictures depicting the range of cracking represented by the crack intensity diagrams (cracks circled). Spans 1 & 2 of this bridge deck performed well while Span 3 performed very well.

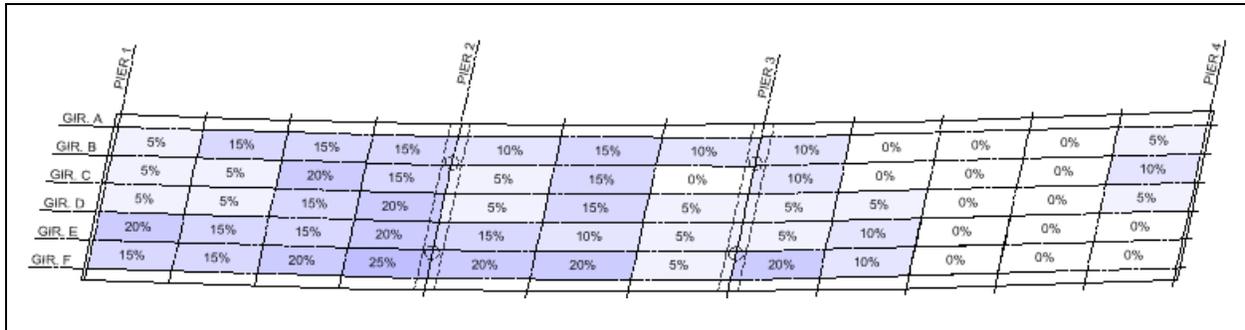


Figure 46 - Bridge 5/234W Crack Intensity Diagram



Figure 47 - Range of Deck Cracking for Bridge 5/234W

BRIDGE 105/4 (NORTH RIVER)

This bridge carries SR 105 over North River in Pacific County. It was constructed in 2014 as part of the **SR 105 Smith Creek and North River Replace Bridges** contract. The contract used the 2012 WSDOT Standard Specifications with Special Provisions which include the **performance based** bridge deck concrete requirements. See Figure 48 for the crack intensity diagram for this bridge. Cracks in portions of Span 1 and all of Spans 2 & 3 were not counted due to limited access. See Figure 49 for pictures depicting the range of cracking represented by the crack intensity diagrams. The bridge deck performed well near the piers and very well near the abutments.

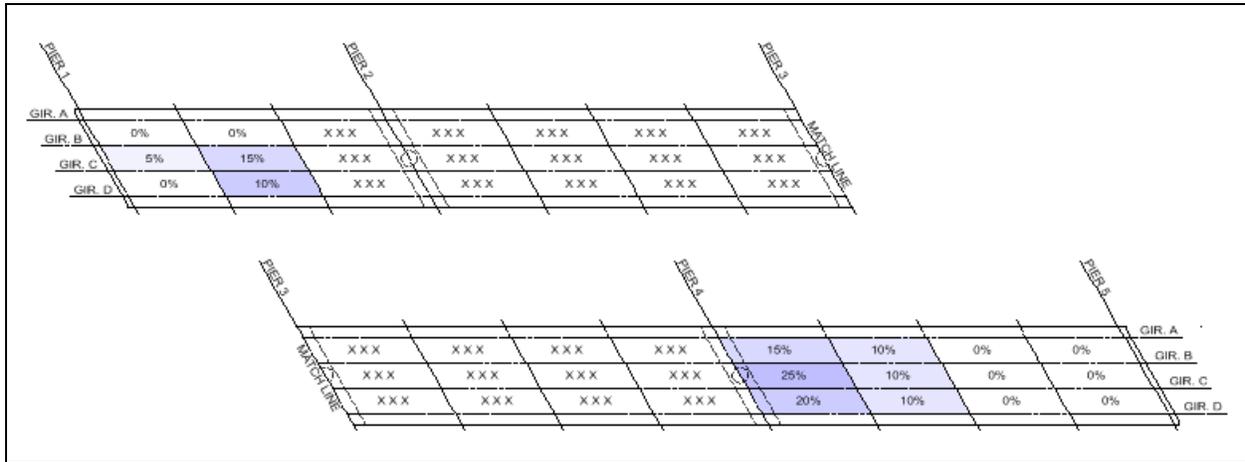


Figure 48 - Bridge 105/4 Crack Intensity Diagram



Figure 49 - Range of Deck Cracking for Bridge 105/4

BRIDGE 105/3 (SMITH CREEK)

This bridge carries SR 105 over Smith Creek. It was constructed in 2013 as part of the **SR 105 Smith Creek and North River Replace Bridges** contract. The contract used the 2012 WSDOT Standard Specifications with Special Provisions which required the **performance based** bridge deck concrete requirements. See Figure 50 for the crack intensity diagram for this bridge. Cracks in Span 2 were not counted due to limited access. See Figure 51 for pictures depicting the range of cracking represented by the crack intensity diagrams. The bridge deck performed well near the piers and very well near the abutments.

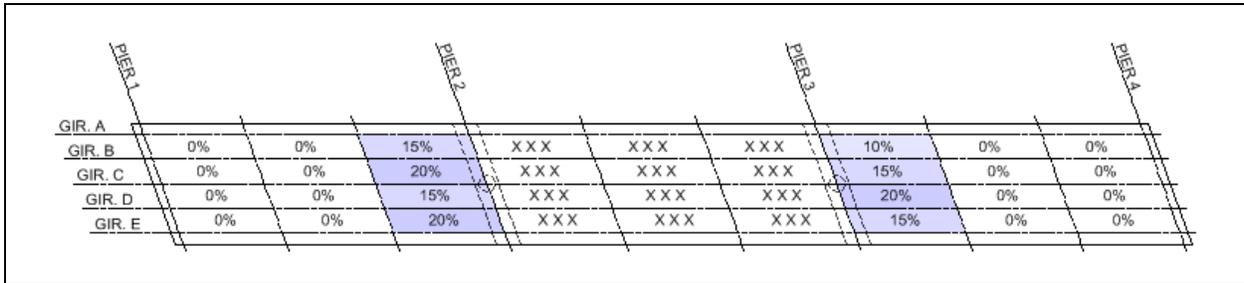


Figure 50 - Bridge 105/3 Crack Intensity Diagram



Figure 51 - Range of Deck Cracking for Bridge 105/3

BRIDGE 6/8 (WILLAPA RIVER)

This bridge carries SR 6 over Willapa River. It was constructed in 2014 as part of the **SR 6 Willapa River Bridge Replace Bridge** contract. The contract used the 2012 WSDOT Standard Specifications with Special Provisions which include the **performance based** bridge deck concrete requirements. See Figure 52 for the crack intensity diagram for this bridge. See Figure 53 for pictures depicting the range of cracking represented by the crack intensity diagrams. The bridge deck performed generally very well.

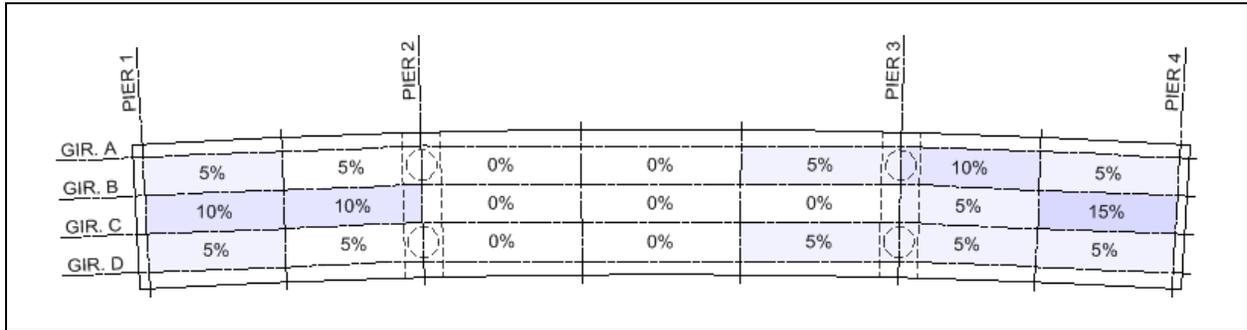


Figure 52 - Bridge 6/8 Crack Intensity Diagram



Figure 53 - Range of Deck Cracking for Bridge 6/8

BRIDGES 5/232NCD AND 5/232SCD (SKOOKUMCHUCK RIVER CD)

These parallel bridges are collector distributors for I-5 over the Skookumchuck River. They were constructed in 2013 as part of the **I-5 Mellen Street to Blakeslee Junction – Stage 1** contract. The contract used the 2012 WSDOT Standard Specifications with Special Provisions which include the **performance based** bridge deck concrete requirements. See Figures 54 & 55 for the crack intensity diagram for these bridges. Cracks were not counted for the middle of Span 2 for Bridge 5/232NCD due to limited access. See Figure 56 for pictures depicting the range of cracking represented by the crack intensity diagrams. The bridge decks for these bridges performed very well.

	PIER 1		PIER 2				PIER 3		PIER 4
GIR. A									
GIR. B	0%	0%	0%	X X X	X X X	0%	0%	0%	
GIR. C	5%	0%	0%	X X X	X X X	0%	0%	5%	
GIR. D	10%	5%	0%	X X X	X X X	10%	0%	0%	
GIR. E	5%	5%	0%	X X X	X X X	0%	0%	0%	

Figure 54 - Bridge 5/232NCD Crack Intensity Diagram

	PIER 1		PIER 2				PIER 3		PIER 4
GIR. A									
GIR. B	0%	0%	0%	0%	0%	0%	0%	5%	0%
GIR. C	0%	0%	0%	0%	0%	0%	0%	0%	0%
GIR. D	0%	0%	0%	0%	0%	0%	0%	0%	0%
GIR. E	0%	0%	0%	0%	0%	10%	5%	5%	

Figure 55 - Bridge 5/232SCD Crack Intensity Diagram



Figure 56 - Range of Deck Cracking for Bridges 5/232NCD & 5/232SCD

101/44 (BONE RIVER)

This bridge carries US 101 over Bone River. It was constructed in 2013 as part of the **US 101 Bone River Bridge Replace Bridge** contract. The contract used the 2012 WSDOT Standard Specifications with Special Provisions which include the **performance based** bridge deck concrete requirements. See Figure 57 for the crack intensity diagram for this bridge. Cracks in Span 2 were not counted due to limited access. See Figure 58 for pictures depicting the range of cracking represented by the crack intensity diagrams (cracks circled). The bridge deck performed very well.

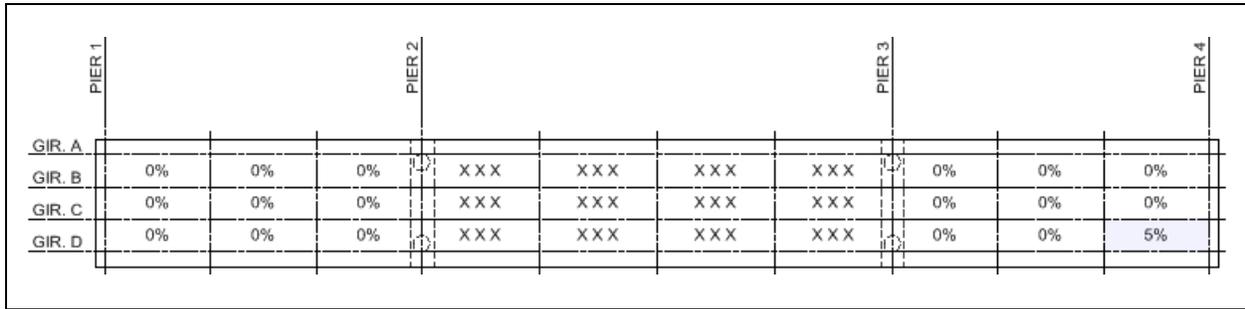


Figure 57 - Bridge 101/44 Crack Intensity Diagram



Figure 58 - Range of Deck Cracking for Bridge 101/44

MULTI-SPAN STEEL PLATE GIRDER BRIDGES

Table 5 summarizes and ranks the average crack intensity for each of the multi-span steel plate girder bridges evaluated. See Appendix D for more information.

Table 5 - Multi-Span Steel Plate Girder Bridge Summary

Br. No.	Bridge Name	Contract	Year	Perform.	Intensity	Cement.	Shrink.
5/434SCD	SBCD OVER SR 16 HOV & RAMPS	8189	2013	Yes	36%	565	0.028%
529/25	EBEY SLOUGH	7948	2012	No	36%	735	--
2/651W-S	W-S RAMP OVER US 2/US 395	7610	2011	No	13%	735	--
9/134	PILCHUCK CREEK	8383	2014	Yes	7%	611	0.031%

Unlike prestressed girder bridges, steel plate girder bridges do not place bridge deck concrete by span. They have a specific placement order with transverse construction joints within each span. See Figure 59 for an example.

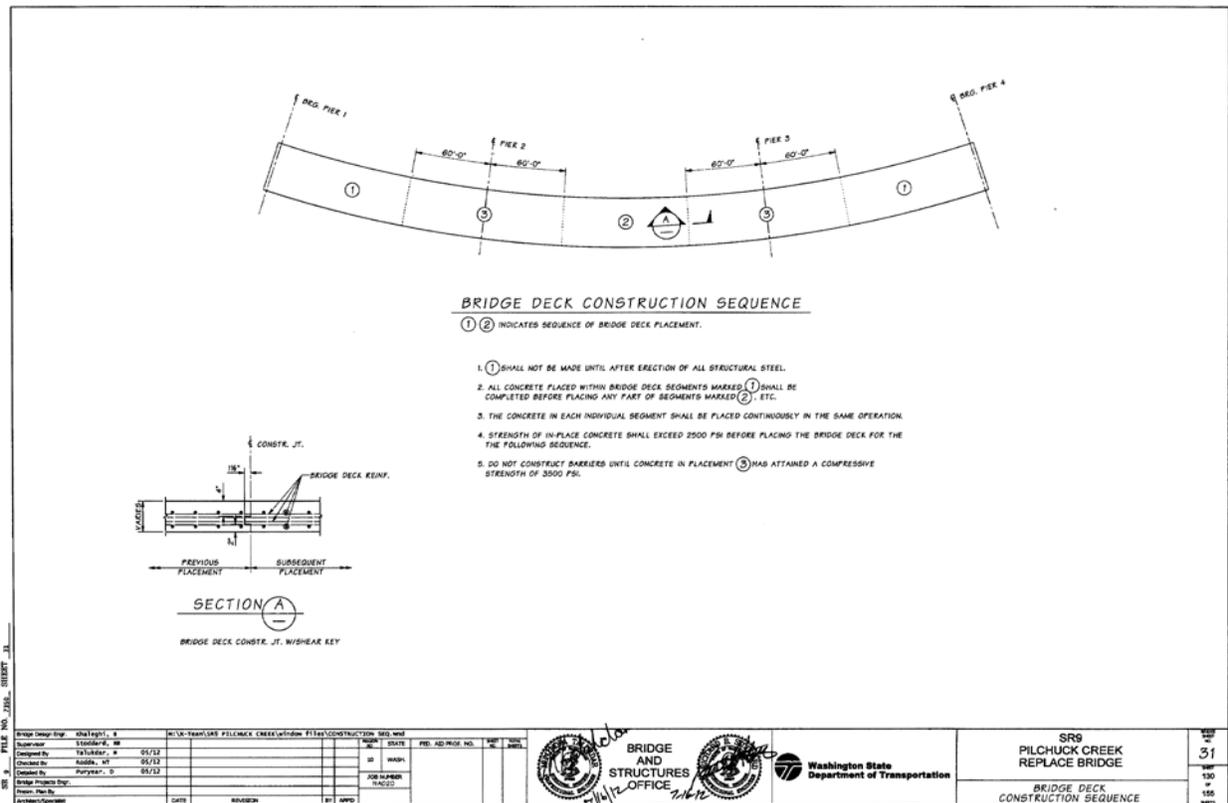


Figure 59 - Steel Plate Girder Bridge Deck Construction Joints

529/25 (EBEY SLOUGH)

This bridge carries SR 529 over Ebey Slough in Marysville and was constructed in 2012 as part of the **SR 529 Ebey Slough Br. – Replace Bridge** contract. The contract used the 2010 WSDOT Standard Specifications which include the **traditional** bridge deck concrete requirements. See Figure 62 for the crack intensity diagrams for this bridge. Cracks were not counted in the majority of the interior spans due to limited access. See Figure 63 for pictures depicting the range of cracking represented by the crack intensity diagrams (spans 2 and 3 not shown). This bridge deck performed poor to very poor.

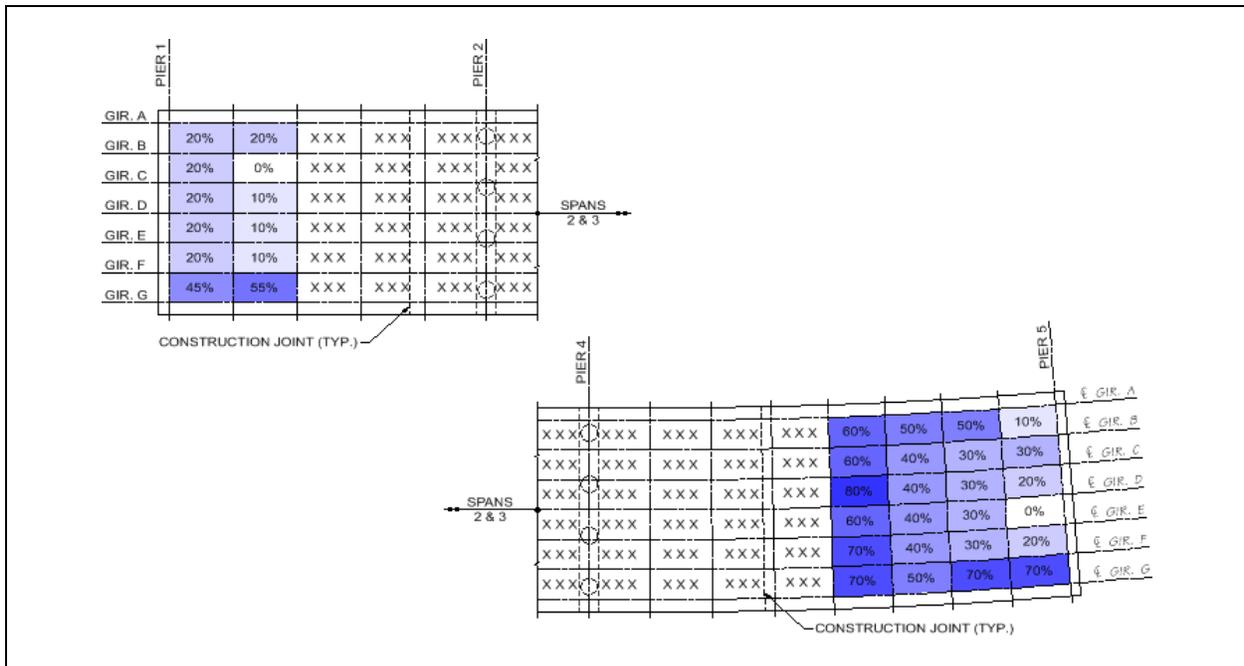


Figure 62 - Bridge 529/25 Crack Intensity Diagram

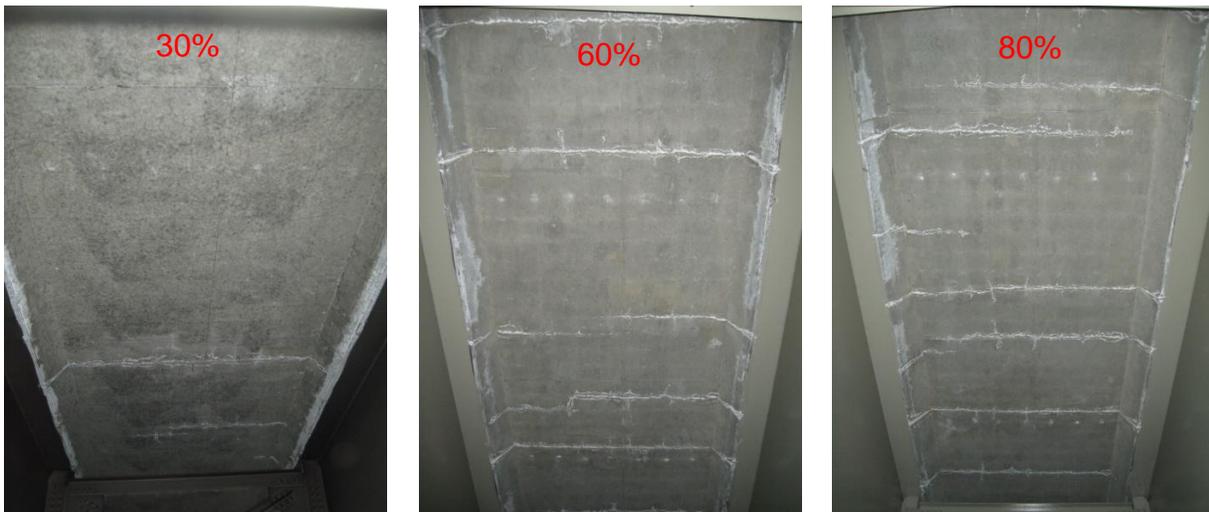


Figure 63 - Range of Deck Cracking for Bridge 529/25

2/651W-S (W-S RAMP OVER US 2 / US 395)

This bridge carries traffic from US 395 to US 2 in Spokane County and was constructed in 2012 as part of the **US 395 NSC – US 2 Lowering** contract. The contract used the 2008 WSDOT Standard Specifications which include the **traditional** bridge deck concrete requirements. See Figure 64 for the crack intensity diagrams for this bridge. See Figure 65 for pictures depicting the range of cracking represented by the crack intensity diagrams. This bridge deck performance ranged from well to poor with some spots of very poor.

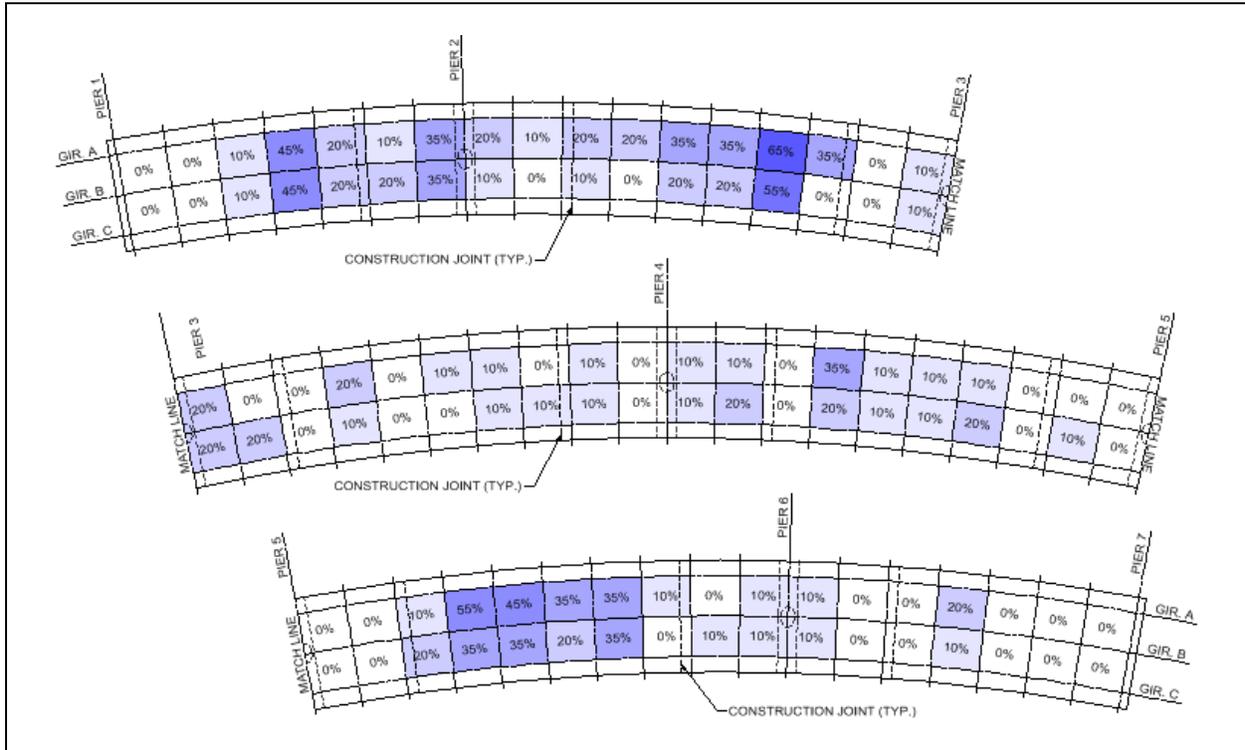


Figure 64 - Bridge 2/651W-S Crack Intensity Diagram



Figure 65 - Range of Deck Cracking for Bridge 2/651W-S

9/134 (PILCHUCK CREEK)

This bridge carries SR 9 over Pilchuck Creek. It was constructed in 2014 as part of the **SR 9 Pilchuck Creek Replace Bridge** contract. The contract used the 2012 WSDOT Standard Specifications with Special Provisions which include the **performance based** bridge deck concrete requirements. See Figure 66 for the crack intensity diagram for this bridge. See Figure 67 for pictures depicting the range of cracking represented by the crack intensity diagrams. The bridge deck performed very well throughout most of the bridge with a few areas of good to poor performance near the construction joints.



Figure 66 - Bridge 9/134 Crack Intensity Diagram



Figure 67 - Range of Deck Cracking for Bridge 9/134

BRIDGE DECK EVALUATION SUMMARY

Table 6 ranks all the bridges evaluated from most severe to least severe average crack intensity. Also listed are total maximum and minimum crack intensity, total cementitious content and shrinkage test results at 28-days.

Table 6 – Bridges Ranked by Average Crack Intensity

Br. No.	Bridge Name	Contract	Year	Perform.	Average Crack Intensity	Min. Crack Intensity	Max. Crack Intensity	Total Cement.	Shrink at 28-days
303/4A	MANETTE BRIDGE	7926	2011	No	73%	45%	100%	735	--
16/7S-E	S SPRAGUE RAMP	7594	2010	No	59%	30%	95%	735	--
90/106N	GOLD CREEK WB	7852	2012	No	44%	5%	80%	735	--
90/105.5S	GOLD CREEK ANIMAL CROSSING EB	7852	2010	No	40%	20%	60%	735	--
5/434SCD	SBCD OVER SR 16 HOV & RAMPS	8189	2013	Yes	36%	0%	100%	565	0.028%
529/25	EBEY SLOUGH	7948	2012	No	36%	0%	80%	735	--
6/115	S FORK CHEHALIS R	7587	2009	No	32%	0%	65%	735	--
90/105.5N	GOLD CREEK ANIMAL CROSSING WB	7852	2012	No	32%	10%	55%	735	--
5/302E	PRAIRIE CREEK NB	7465	2009	No	18%	0%	65%	735	--
2/651W-S	W-S RAMP OVER US 2/US 395	7610	2011	No	13%	0%	65%	735	--
195/117	CHENEY SPOKANE RD OVER US 195	8378	2014	Yes	10%	0%	33%	no records found	
395/442W	US 395 OVER US 2	7610	2011	No	10%	0%	30%	735	--
5/234W	I-5 OVER BLAKESLEE JCT RR	8272	2013	Yes	9%	0%	25%	580	0.030%
16/3W	SR 16 OVER HOV	8189	2014	Yes	9%	0%	35%	565	0.028%
9/133	SR 9 OVER HARVEY CRK RD	7267	2008	No	8%	0%	45%	735	--
9/134	PILCHUCK CREEK	8383	2014	Yes	7%	0%	45%	611	0.031%
105/4	NORTH RIVER	8345	2014	Yes	7%	0%	25%	610	0.018%
2/8.5N-W	N-W RAMP (BICKFORD AVE) OVER US 2	8286	2013	Yes	6%	0%	20%	610	0.032%
105/3	SMITH CREEK	8345	2013	Yes	6%	0%	20%	610	0.018%
6/8	WILLAPA RIVER	8464	2014	Yes	5%	0%	15%	610	0.018%
5/302W	PRAIRIE CREEK SB	7465	2010	No	4%	0%	15%	735	--
5/232NCD	SKOOKUMCHUCK RIVER NCD	8272	2013	Yes	2%	0%	10%	580	0.030%
5/232SCD	SKOOKUMCHUCK RIVER SCD	8272	2013	Yes	1%	0%	10%	580	0.030%
5/229	MELLON STREET COUPLET	8473	2014	Yes	< 1%	0%	5%	580	0.028%
395/441N-E	N-E RAMP OVER N-N RAMP	7610	2011	Yes	< 1%	0%	5%	565	0.034%
101/44	BONE RIVER	8292	2013	Yes	< 1%	0%	5%	610	0.018%
101/31	MIDDLE NEMAH RIVER	8344	2014	Yes	0%	0%	0%	610	0.018%

In general, the performance based concrete specification resulted in fewer restraint cracks in bridge decks than the traditional concrete specification. A few of the traditional bridge decks performed similar to the performance based bridge decks, but this appears to be the exception, not the rule. Only one of the performance based concrete decks had a high intensity of cracking. It is unclear what contributed to the poor performance of this particular bridge deck.

What is apparent from this study is that cracking of bridge decks is variable within same bridge. In some cases, it appears to be variable within the same concrete placement. This indicates that there are many variables that affect the cracking performance of a bridge deck that change during the construction of the bridge.

As a measure of overall success, 10% average crack intensity could be defined as good performance. For individual bays, a possible scale for bridge deck cracking performance could be:

Good = 0% to 25% Fair = 25% to 50% Bad = 50% to 100%

DECK CONCRETE SPECIFICATION EVALUATION

Overall, the current performance based specification appears to be providing good results in a practical manner. There is no evidence that the performance based limits need to be changed. It does not appear that Contractors have had issues achieving them and the superstructure lump sum costs do not appear to have increased dramatically.

There are areas of the specification that could be improved as it relates to specifying shrinkage reducing admixtures, reporting test results and monitoring deck temperatures. As they are currently written, there is much inconsistency with how these elements are provided to WSDOT.

SHRINKAGE REDUCING AD-MIXTURE

Shrinkage reducing admixtures (SRA) are used to meet the shrinkage limits in the specification. All of the performance based bridges evaluated had SRA in the deck concrete. Contractors are required to submit their mix design on WSDOT form 350-040 which allows estimated ranges for admixtures. See Appendix A through D for concrete mix designs submitted for the performance based bridge decks.

Some of the concrete mix design submittals received for this report list a range for the SRA (e.g. 1 – 150 oz/cy). This could lead to a concrete mix being tested for shrinkage with SRA at the high end of the range but being placed in the field with SRA at the low end of the range. To correct this potential issue, the SRA dose should be listed as one number on the Concrete Mix Design form (or a very narrow range), and the SRA used in the shrinkage test should match.

TEST REPORT FOR SHRINKAGE

Shrinkage tests are required to be performed in accordance with AASHTO T 160 (or equivalent ASTM C 157) and submitted following the reporting requirements of these procedures; however, there is much inconsistency in the shrinkage test reports submitted. See Appendix A through D for shrinkage test reports submitted for the performance based bridge decks.

In general, the shrinkage test is performed in the following way:

- Three specimens are cast in molds
- Specimens are removed from the molds a day after casting
- Specimens are measured for the initial length reading
- Specimens are stored in lime-saturated water until they have reached an age of 28-days
- Specimens are measured for a length reading at the end of the curing (drying day zero)
- Specimens are stored in air and allowed to shrink
- All three specimens are measured at 4, 7, 14 and 28 days
- These readings are converted into length change percentages (or microstrains)
- The average length change of the three specimens is reported

See Figure 68 for a typical shrinkage report.

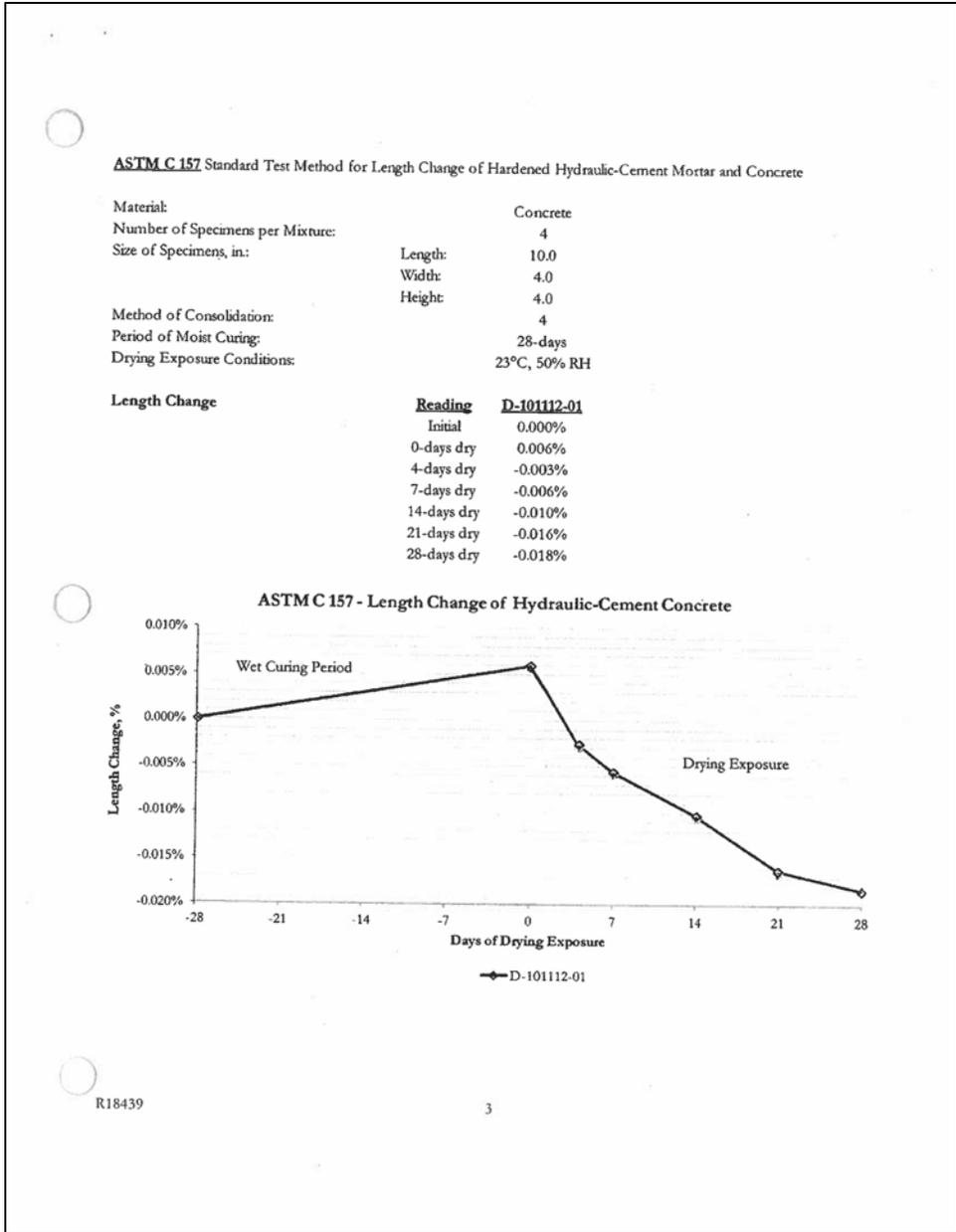


Figure 68 - Shrinkage Test Report

The information included in the shrinkage reports received for this study did not always include length change values at each of the days specified in the test procedure; one report only listed a single value. In addition, the values for the individual test specimens were not always given. Most of the reports only listed the average of the three specimens.

To ensure proper conformance with the performance limit, consistent information needs to be provided for review and acceptance.

TEMPERATURE MONITORING

Contractors are required to embed temperature monitors and record deck temperatures for seven days after concrete placement and submit the data to WSDOT. There is a limit on concrete temperature at the time of placement, but there are no contractual limits associated with the temperature of the deck concrete after placement (as it sets and cures). Contractors are also required to measure ambient air temperature near the embedded temperature monitors.

One of the expectations going into this study was to correlate concrete temperatures to performance. No correlation could be found because temperature data received for this study varied and was often incomplete or obviously in error. For example, multi-span bridges evaluated in this study often only had one set of temperature readings even though there are multiple deck placements. A couple sets of temperature data had very high and very low temperatures (500°F+ to -32°F) which are obviously in error.

Additionally, when good temperature data was received, it was difficult to identify where the temperature readings were taken. This made it challenging to correlate the temperature with deck performance in local areas. The visual inspections performed for this study indicate that performance can vary significantly within in the same concrete placement and exact placement of the temperature readings could have been very informative.

Peak temperature or differences between concrete temperature and ambient temperature could correlate with deck performance. Good documentation of these temperatures in a consistent format could help identify possible performance limits to place on peak temperature or temperature difference.

RECOMMENDATIONS

Based on the visual inspection, concrete submittals and temperature data for the bridges evaluated in this study, the following recommendations are suggested to continue achieving reduced early-age cracks in bridge decks. Additional suggestions are provided to aid in the continuation of collection of data to further refine or justify the performance limits required.

1. No current changes to the performance limits, aggregate size, curing method or texturing methods are recommended.
2. Continuation of bridge deck evaluation is recommended. Suggest using the same method as outlined in this report for bridges which the underside of the deck is visible. Perhaps a team or individual can be tasked with collecting data and evaluating the bridge decks shortly after they are completed. A spreadsheet similar to those used for this evaluation can be utilized to record information for future bridges.
3. Development of an evaluation method for bridges which the underside of the deck is not visible (deck bulb-tee's) is recommended.
4. It is recommended that a form is provided to the Contractor for the required test results for ease of tracking and comparison.
5. Locating the embedded temperature monitors in the contract plans is recommended. Multiple temperature monitors should be included for each deck placement. At a minimum, one at each end and one mid-span. The embedded monitors should be located as close to mid-slab thickness as possible.
6. Temperature monitor data could be very informative and it is recommended that the data received from the Contractor should include, at a minimum, the following elements: date and time which concrete placement started, where concrete placement started, location of monitor, temperature measurements at hour max intervals. Perhaps a form can be provided for ease of review.
7. It is recommended that peak temperature and maximum temperature limits be established. This may provide a tool to reject a deck that performs very poorly due to extreme temperature or temperature differences. While no evidence of type of this behavior was seen in this study, adding contractual limits requirements may result in better temperature data.
8. Information on the temperature changes over time for a specific concrete mix may be useful during the mix design phase. It could be used to compare one mix to the other and possibly aid in developing performance based limits that can be added to the concrete mix design requirements. See the "SR 520 – ACME Project Final Findings Report" dated November 30, 2010 for examples of temperature data collection during the mix design phase.

APPENDIX A

SINGLE SPAN PRESTRESSED GIRDER BRIDGES

BRIDGE 90/105.5S (GOLD CREEK ANIMAL CROSSING EB)

BRIDGE 90/105.5N (GOLD CREEK ANIMAL CROSSING WB)

BRIDGE 5/302E (PRAIRIE CREEK NB)

BRIDGE 5/302W (PRAIRIE CREEK SB)

BRIDGE 9/133 (SR 9 OVER HARVEY CREEK ROAD)

BRIDGE 5/229 (MELLEN STREET COUPLET)

BRIDGE 101/31 (MIDDLE NEMAH RIVE)

BRIDGE 90/105.5S (GOLD CREEK ANIMAL CROSSING EB)

Bridge #	90/105.5S	Bridge Name	Gold Creek Animal Crossing EB		Structure ID	0017852A	
Contract #	7852	Region	SC	Project Engineer	Will Smith	Performance Deck Concrete?	No
Contractor	Max J. Kuney Company		Concrete Supplier		Deck Placement		≈ 2010
Bridge Description	Single Span (118.5'), 8-WF50G Girders, 3-Lanes (56' wide roadway)						



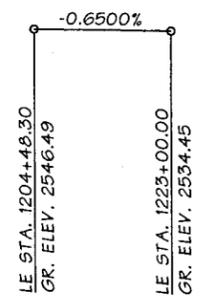
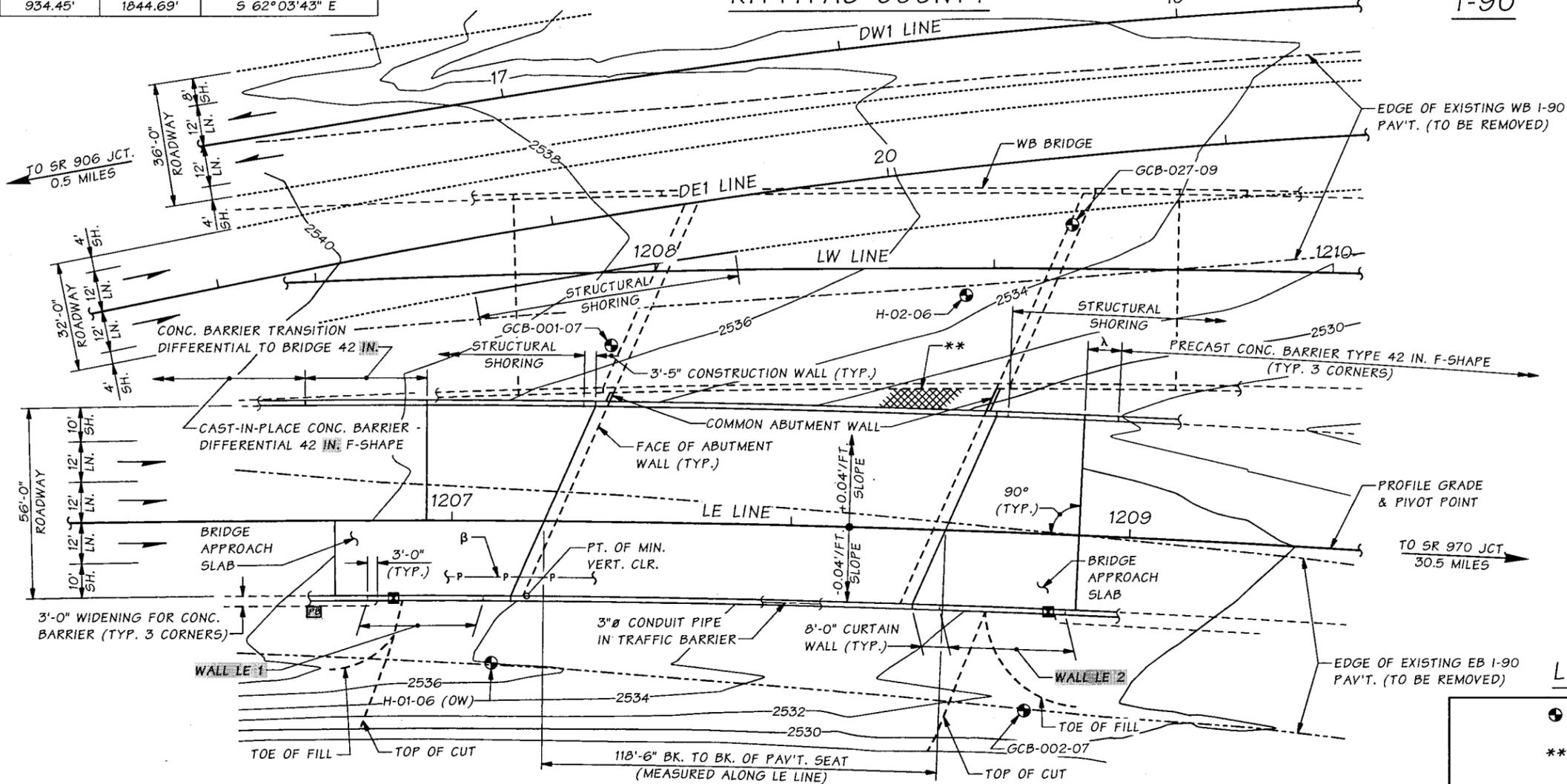
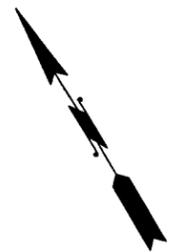
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2. Field Notes
3. Crack Summary
4. Crack Intensity Diagram

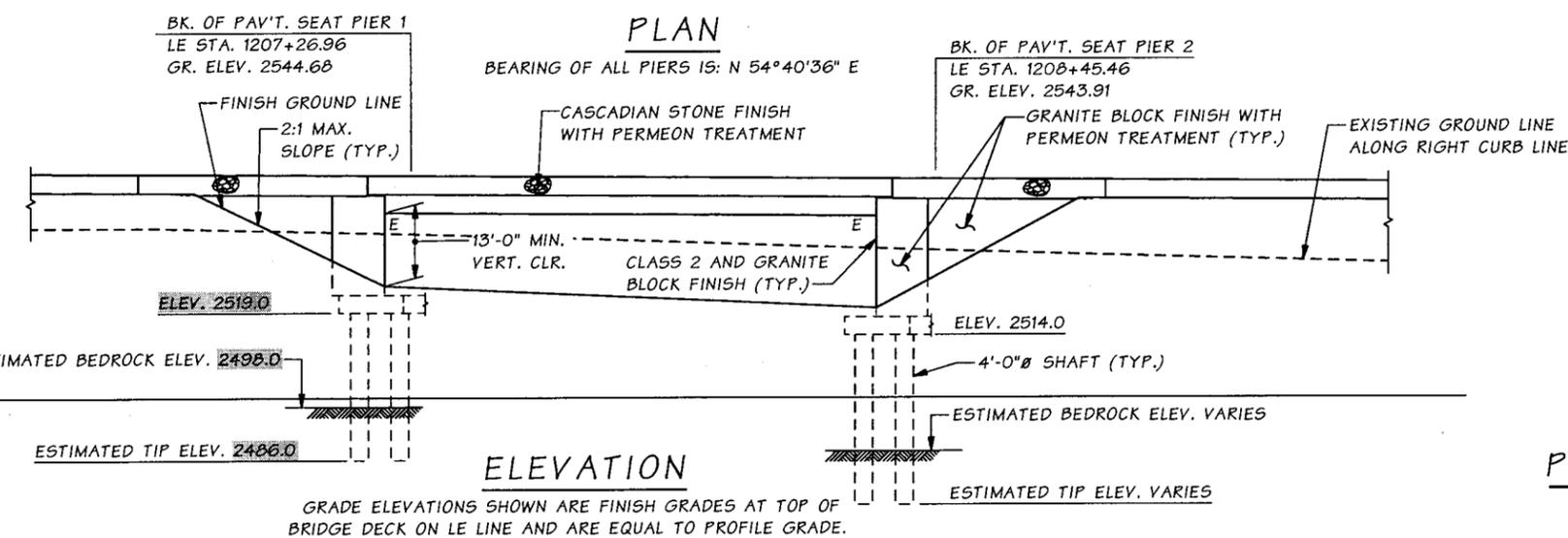
SEC. 15, T.22N., R.11E., W.M.
KITTITAS COUNTY

LE LINE CURVE DATA					
P.I. STA.	Δ	RADIUS	TANGENT	LENGTH	BACK TANGENT BEARING
1213+82.75	22°33'36" RT.	4685.00'	934.45'	1844.69'	S 62°03'43" E

1-90



LE LINE PROFILE



ELEVATION

LEGEND

- SOIL BORING LOCATION
- ** MEDIAN NET (BETWEEN BRIDGES)
- JUNCTION BOX NEMA 4X 5.5. (TYP.)
- β 4" CONDUIT & 2 - 6" CONDUIT
- P- POWER
- λ CONC. BARRIER TRANSITION CAST-IN-PLACE TO 42 IN. F-SHAPE (TYP. 3 CORNERS)
- ▣ PULL BOX

DATUM
NAVD 88

P.C. GIRDERS (WF50G)
LOADING: HL-93

SR 90 FILE NO. 7257 SHEET BA1

Bridge Design Engr.	Khaleghi, B	M:\X-Team\I-90 HYAK - SS VIC\GOLD CR ANIMAL BR EB>window files\LAYOUT.WND
Supervisor	Stoddard, RB	
Designed By	Bingle, J	07/09
Checked By	PRG/JD	10/09
Detailed By	Bontemps, W	07/09
Bridge Projects Engr.	Lewis, R	08/08
Prelim. Plan By	Wei, J.	08/08
Architect/Specialist	PDK, BSA, GAW	08/08

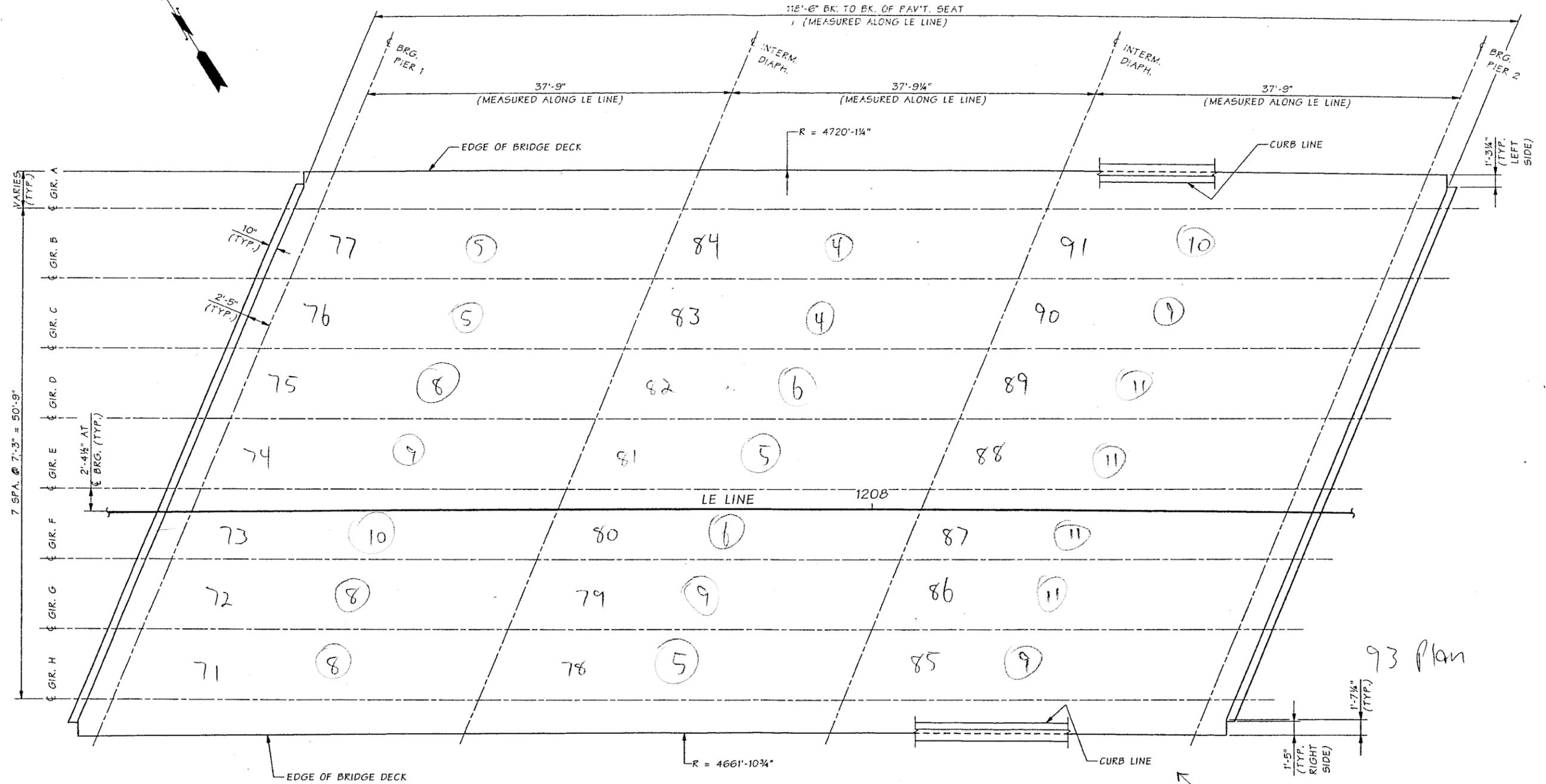
REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
10	WASH.			
JOB NUMBER		09Y019		

BRIDGE AND STRUCTURES OFFICE

I-90
HYAK TO SNOWSHED VICINITY PHASE 1B -
ADD LANES AND BRIDGES
GOLD CR ANIMAL CROSSING BRIDGE EB
LAYOUT

BRIDGE SHEET NO.	BA1
SHEET NO.	484
OF	808
SHEETS	

C. S. 190115 ~ PROJ. NO. XL2779G ~ SOUTH CENTRAL REGION ~ I-90 ~ MP 55.30 TO MP 55.32 ~ GOLD CR ANIMAL CROSSING BRIDGE EB



FRAMING PLAN

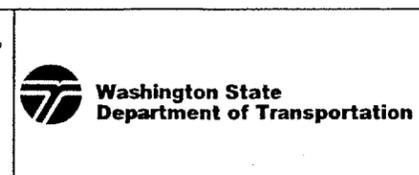
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 BEARING OF GIRDERS IS : S 57°55'46" E

SR 90 FILE NO. 7257 SHEET BA16

Bridge Design Engr.	Khaleghi, B	M:\X-Team\I-90 HYAK - SS VIC\GOLD CR ANIMAL BR EB\window files\FRAMING PLAN.WND			
Supervisor	Stoddard, RB	REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.
Designed By	Bingle, J 05/09	10	WASH.		TOTAL SHEETS
Checked By	Dao, J 10/09	JOB NUMBER 09Y019			
Detailed By	Bontemps, W 06/09				
Bridge Projects Engr.		DATE	REVISION	BY	APPD
Prelim. Plan By					
Architect/Specialist					

BRIDGE AND STRUCTURES OFFICE

10-15-09 10/14/09



I-90
 HYAK TO SNOWSHED VICINITY PHASE 1B -
 ADD LANES AND BRIDGES
 GOLD CR ANIMAL CROSSING BRIDGE EB
FRAMING PLAN

BRIDGE SHEET NO.	BA16
SHEET	499
OF	808
SHEETS	

90/105.55



Bridge #	90/105.5S	Bridge Name	Gold Creek Animal Crossing EB			Structure ID	0017852A	
Contract #	7852	Region	SC	Project Engineer	Will Smith	Performance Deck Concrete?	No	
Contractor	Max J. Kuney Company		Concrete Supplier				Deck Placement	≈ 2010
Bridge Description	Single Span (118.5'), 8-WF50G Girders, 3-Lanes (56' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

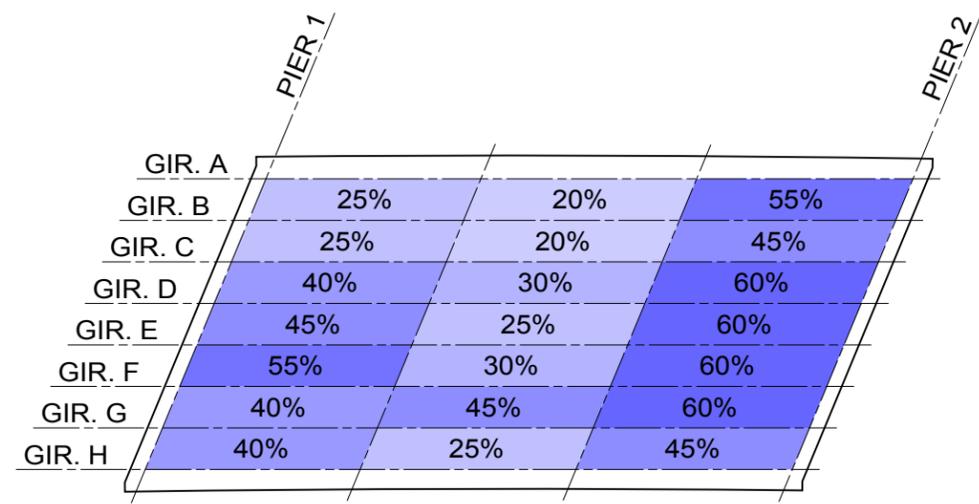
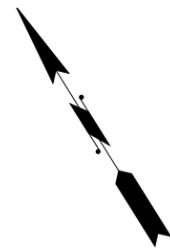
N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	40%
Min. =	20%
Max. =	60%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	37.75	7.25	5	19	25%
1	1	B	C	37.75	7.25	5	19	25%
1	1	C	D	37.75	7.25	8	19	40%
1	1	D	E	37.75	7.25	9	19	45%
1	1	E	F	37.75	7.25	10	19	55%
1	1	F	G	37.75	7.25	8	19	40%
1	1	G	H	37.75	7.25	8	19	40%
1	2	A	B	37.75	7.25	4	19	20%
1	2	B	C	37.75	7.25	4	19	20%
1	2	C	D	37.75	7.25	6	19	30%
1	2	D	E	37.75	7.25	5	19	25%
1	2	E	F	37.75	7.25	6	19	30%
1	2	F	G	37.75	7.25	9	19	45%
1	2	G	H	37.75	7.25	5	19	25%
1	3	A	B	37.75	7.25	10	19	55%
1	3	B	C	37.75	7.25	9	19	45%
1	3	C	D	37.75	7.25	11	19	60%
1	3	D	E	37.75	7.25	11	19	60%
1	3	E	F	37.75	7.25	11	19	60%
1	3	F	G	37.75	7.25	11	19	60%
1	3	G	H	37.75	7.25	9	19	45%



CRACKING INTENSITY ~ BRIDGE 90/105.5S

100% = CRACK EVERY 2 FT.

LESS CRACKING

MORE CRACKING



BRIDGE NUMBER	90/105.5S
BRIDGE NAME	GOLD CREEK ANIMAL CROSSING EB
INSPECTION DATE	5/20/2015
DECK CONCRETE	TRADITIONAL

BRIDGE 90/105.5N (GOLD CREEK ANIMAL CROSSING WB)

Bridge #	90/105.5N	Bridge Name	Gold Creek Animal Crossing WB		Structure ID	0017852B		
Contract #	7852	Region	SC	Project Engineer	Will Smith	Performance Deck Concrete?	No	
Contractor	Max J. Kuney Company		Concrete Supplier		Deck Placement			≈ 2012
Bridge Description	Single Span (120'), 8-WF50G Girders, 3-Lanes (56' wide roadway)							



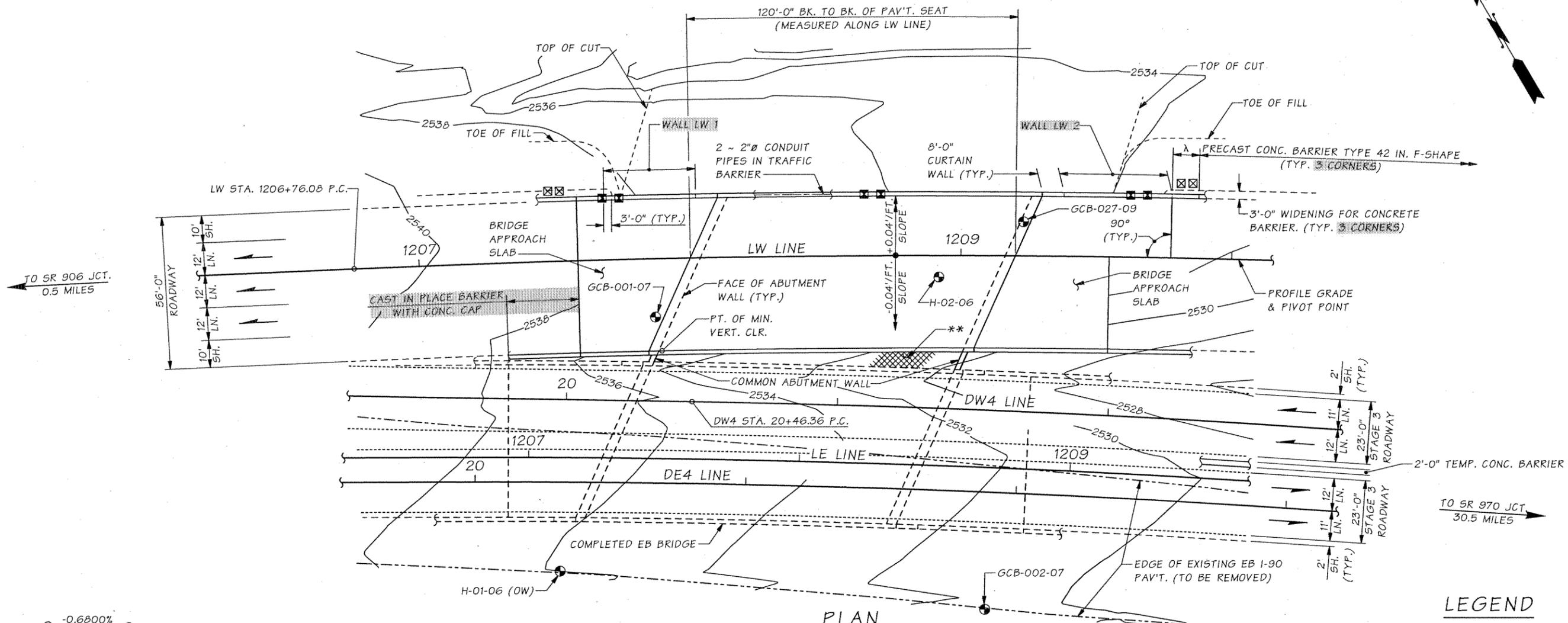
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2. Field Notes
3. Crack Summary
4. Crack Intensity Diagram

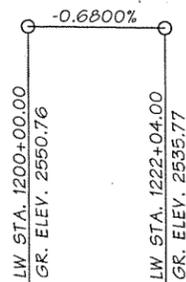
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SEC. 15, T.22N., R.11E., W.M.
KITTITAS COUNTY

1-90

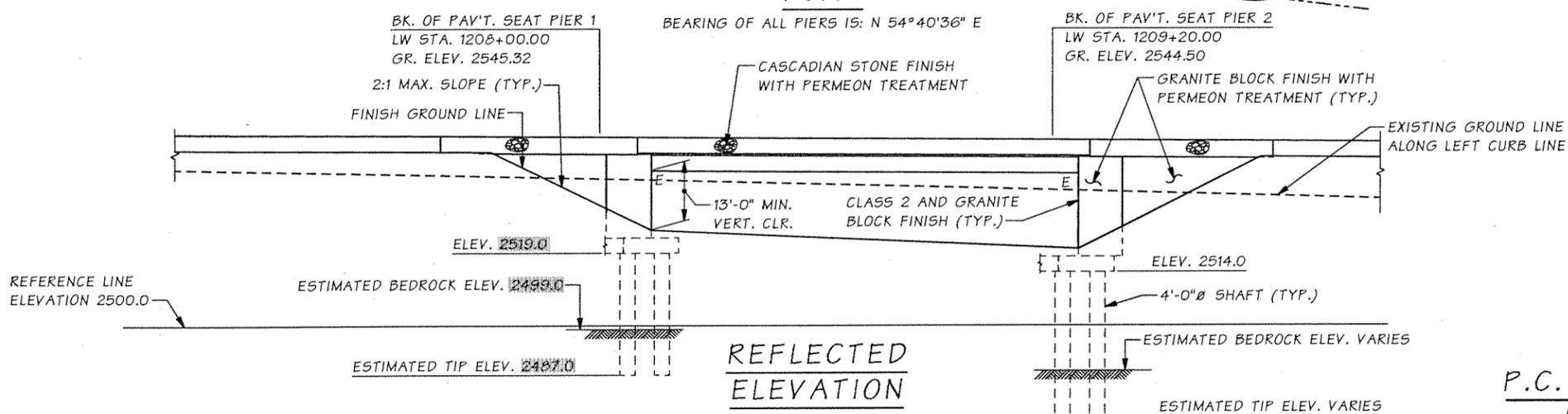


PLAN



LW LINE PROFILE

DATUM
NAVD 88



REFLECTED ELEVATION

LEGEND

- ⊕ SOIL BORING LOCATION
- ** MEDIAN NET (BETWEEN BRIDGES)
- ⊠ JUNCTION BOX (TYP.)
- ⊠ JUNCTION BOX NEMA 4X 5.5. (TYP.)
- λ CONC. BARRIER TRANSITION CAST-IN-PLACE TO 42 IN. F-SHAPE (TYP.)

P.C. GIRDERS (WF50G)
LOADING: HL-93

SR 90 FILE NO. 7257 SHEET 881

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Supervisor Stoddard, RB		10	WASH.			
Designed By Bingle, J	07/09	JOB NUMBER 09Y019				
Checked By PRG/JD	10/09					
Detailed By Bontemps, W	07/09					
Bridge Projects Engr. Lewis, R	08/08	CHANGED ELEV'S, WALL NAMES AND LENGTHS, JP				
Prelim. Plan By Wei, J.	07/08	AND ADDED CALLOUTS				
Architect/Specialist PDK, BSA, GAW	08/08	DATE	REVISION	BY	APP'D	

GRADE ELEVATIONS SHOWN ARE FINISH GRADES AT TOP OF BRIDGE DECK ON LW LINE AND ARE EQUAL TO PROFILE GRADE.

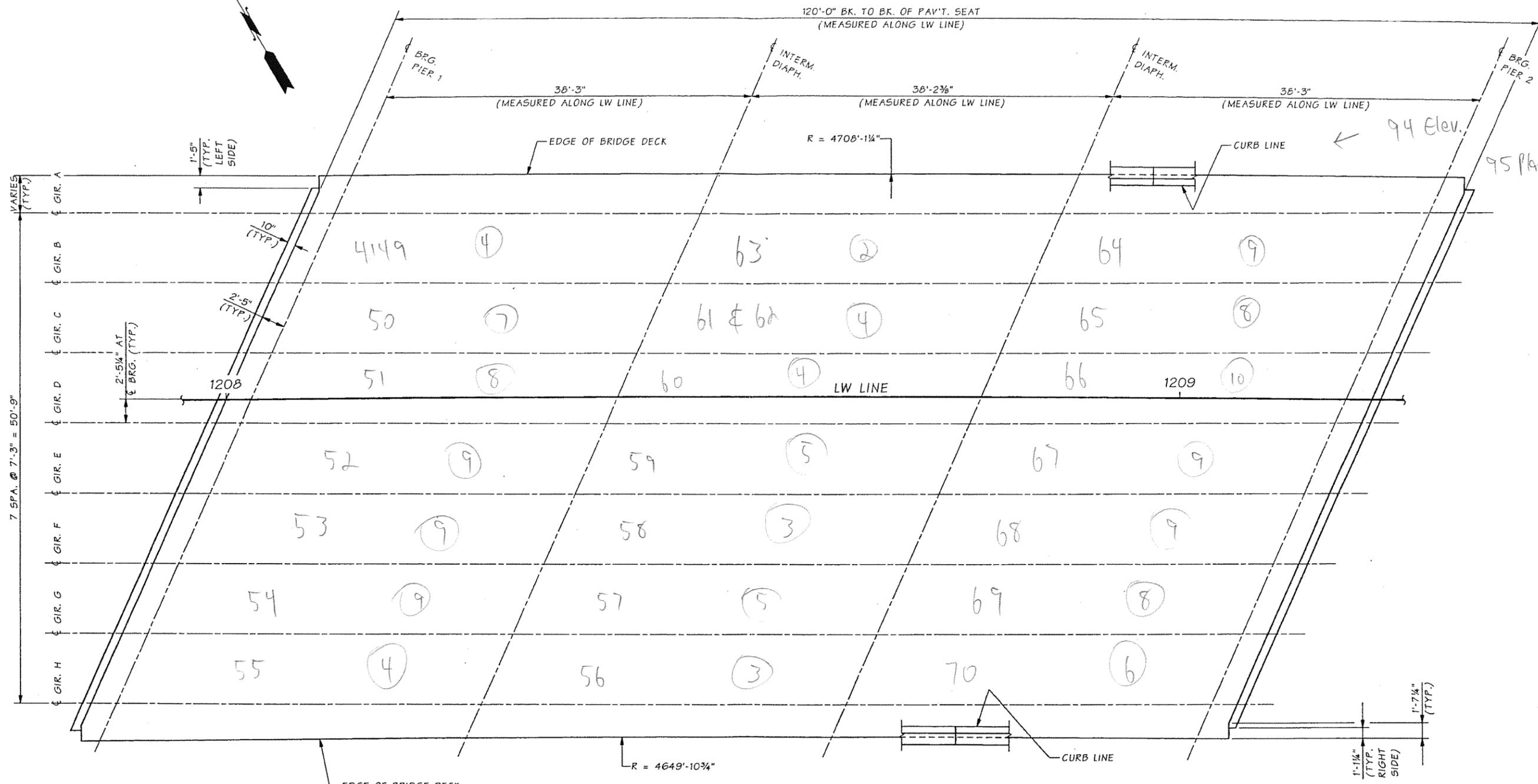
BRIDGE AND STRUCTURES OFFICE



I-90
HYAK TO SNOWSHED VICINITY PHASE 1B -
ADD LANES AND BRIDGES
GOLD CR ANIMAL CROSSING BRIDGE WB
LAYOUT

BRIDGE SHEET NO. BB1
SHEET 519 OF 808 SHEETS

C. S. 190115 ~ PROJ. NO. XL2779B ~ SOUTH CENTRAL REGION ~ I-90 ~ MP 55.31 TO MP 55.33 ~ GOLD CR ANIMAL CROSSING BRIDGE WB



FRAMING PLAN

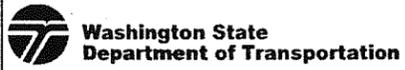
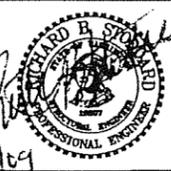
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 BEARING OF GIRDERS IS : S 59°35'14" E

SR 90 FILE NO. 7257 SHEET BB15

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Designed By	Bingle, J 05/09	10	WASH.		TOTAL SHEETS
Checked By	Dao, J 10/09	JOB NUMBER 09Y019			
Detailed By	Bontemps, W 06/09	DATE REVISION BY APPD			
Bridge Projects Engr.					
Prelm. Plan By					
Architect/Specialist					



BRIDGE AND STRUCTURES OFFICE



I-90
 HYAK TO SNOWSHED VICINITY PHASE 1B -
 ADD LANES AND BRIDGES
 GOLD CR ANIMAL CROSSING BRIDGE WB
 FRAMING PLAN

BRIDGE SHEET NO.	BB15
SHEET OF	533 OF 808
SHEETS	

90/105.5 N



Bridge #	90/105.5N	Bridge Name	Gold Creek Animal Crossing WB			Structure ID	0017852B	
Contract #	7852	Region	SC	Project Engineer	Will Smith	Performance Deck Concrete?	No	
Contractor	Max J. Kuney Company		Concrete Supplier			Deck Placement	≈ 2012	
Bridge Description	Single Span (120'), 8-WF50G Girders, 3-Lanes (56' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

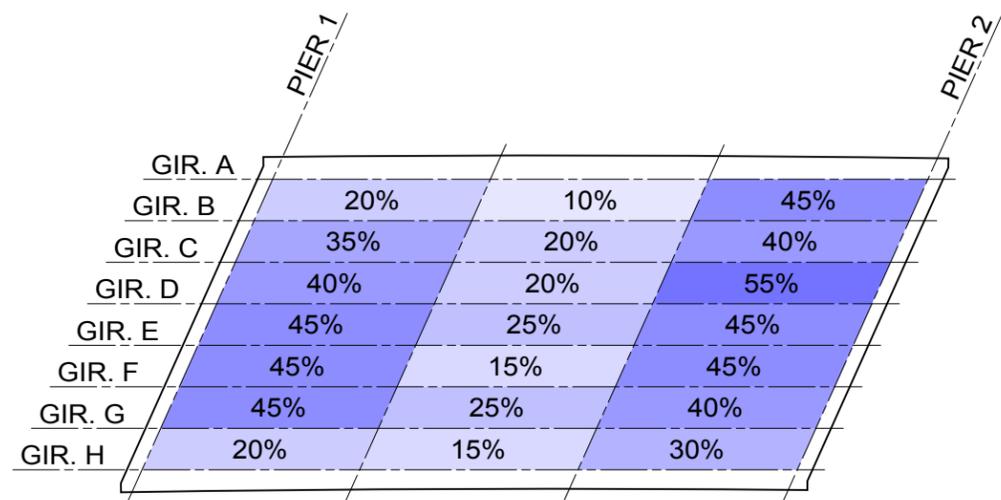
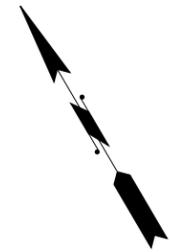
N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	32%
Min. =	10%
Max. =	55%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	38.25	7.25	4	19	20%
1	1	B	C	38.25	7.25	7	19	35%
1	1	C	D	38.25	7.25	8	19	40%
1	1	D	E	38.25	7.25	9	19	45%
1	1	E	F	38.25	7.25	9	19	45%
1	1	F	G	38.25	7.25	9	19	45%
1	1	G	H	38.25	7.25	4	19	20%
1	2	A	B	38.25	7.25	2	19	10%
1	2	B	C	38.25	7.25	4	19	20%
1	2	C	D	38.25	7.25	4	19	20%
1	2	D	E	38.25	7.25	5	19	25%
1	2	E	F	38.25	7.25	3	19	15%
1	2	F	G	38.25	7.25	5	19	25%
1	2	G	H	38.25	7.25	3	19	15%
1	3	A	B	38.25	7.25	9	19	45%
1	3	B	C	38.25	7.25	8	19	40%
1	3	C	D	38.25	7.25	10	19	55%
1	3	D	E	38.25	7.25	9	19	45%
1	3	E	F	38.25	7.25	9	19	45%
1	3	F	G	38.25	7.25	8	19	40%
1	3	G	H	38.25	7.25	6	19	30%



CRACKING INTENSITY ~ BRIDGE 90/105.5N

100% = CRACK EVERY 2 FT.

LESS CRACKING

MORE CRACKING



BRIDGE NUMBER	90/105.5N
BRIDGE NAME	GOLD CREEK ANIMAL CROSSING WB
INSPECTION DATE	5/20/2015
DECK CONCRETE	TRADITIONAL

BRIDGE 5/302E (PRAIRIE CREEK NB)

Bridge #	5/302E	Bridge Name	Prairie Creek NB	Structure ID	0017465A		
Contract #	7465	Region	SW	Project Engineer	McNutt/Engel	Performance Deck Concrete?	No
Contractor	Scarsella Bros.	Concrete Supplier		Deck Placement	≈ 2009		
Bridge Description	Single-Span (77'), 8-WF42G Girders, 4-Lanes (variable width roadway abt. 70' wide)						



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1. Layout Plan Sheet
2. Field Notes
3. Crack Summary
4. Crack Intensity Diagram



Bridge #	5/302E	Bridge Name	Prairie Creek NB			Structure ID	0017465A	
Contract #	7465	Region	SW	Project Engineer	McNutt/Engel	Performance Deck Concrete?	No	
Contractor	Scarsella Bros.		Concrete Supplier			Deck Placement	≈ 2009	
Bridge Description	Single-Span (77'), 8-WF42G Girders, 4-Lanes (variable width roadway abt. 70' wide)							

L = length between diaphragms (or length of "bay")

S = girder spacing

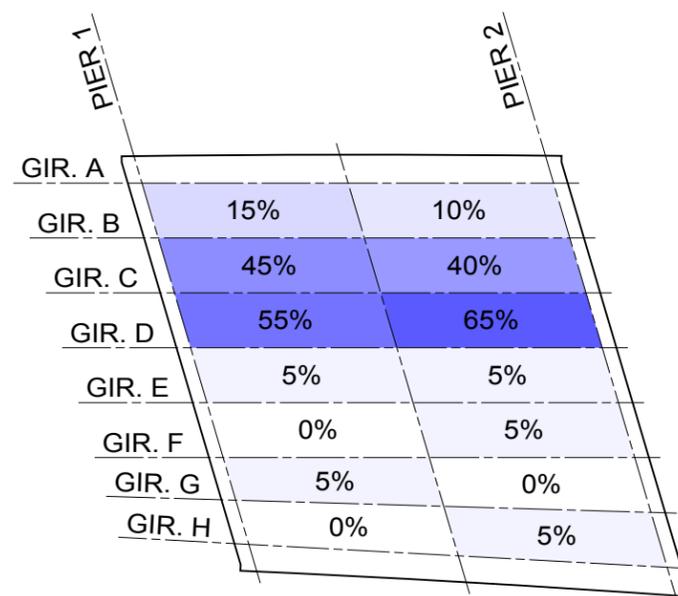
N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	18%
Min. =	0%
Max. =	65%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	36.00	5.50	3	18	15%
1	1	B	C	36.00	5.50	8	18	45%
1	1	C	D	36.00	5.50	10	18	55%
1	1	D	E	36.00	5.50	1	18	5%
1	1	E	F	36.00	5.50	0	18	0%
1	1	F	G	36.00	3.50	1	18	5%
1	1	G	H	36.00	3.50	0	18	0%
2	2	A	B	36.00	5.50	2	18	10%
2	2	B	C	36.00	5.50	7	18	40%
2	2	C	D	36.00	5.50	12	18	65%
2	2	D	E	36.00	5.50	1	18	5%
2	2	E	F	36.00	5.50	1	18	5%
2	2	F	G	36.00	4.50	0	18	0%
2	2	G	H	36.00	4.50	1	18	5%



CRACKING INTENSITY ~ BRIDGE 5/302E

100% = CRACK EVERY 2 FT.

LESS CRACKING

MORE CRACKING

BRIDGE NUMBER	5/302E
BRIDGE NAME	PRAIRIE CREEK NB
INSPECTION DATE	4/8/2015
DECK CONCRETE	TRADITIONAL

BRIDGE 5/302W (PRAIRIE CREEK SB)

Bridge #	5/302W	Bridge Name	Prairie Creek SB		Structure ID	0017465B	
Contract #	7465	Region	SW	Project Engineer	McNutt/Engel	Performance Deck Concrete?	No
Contractor	Scarsella Bros.			Concrete Supplier	Unknown	Deck Placement	≈ 2010
Bridge Description	Single-Span (80'), 8-WF42G Girders, 4-Lanes (variable wdth roadway abt. 76' wide)						



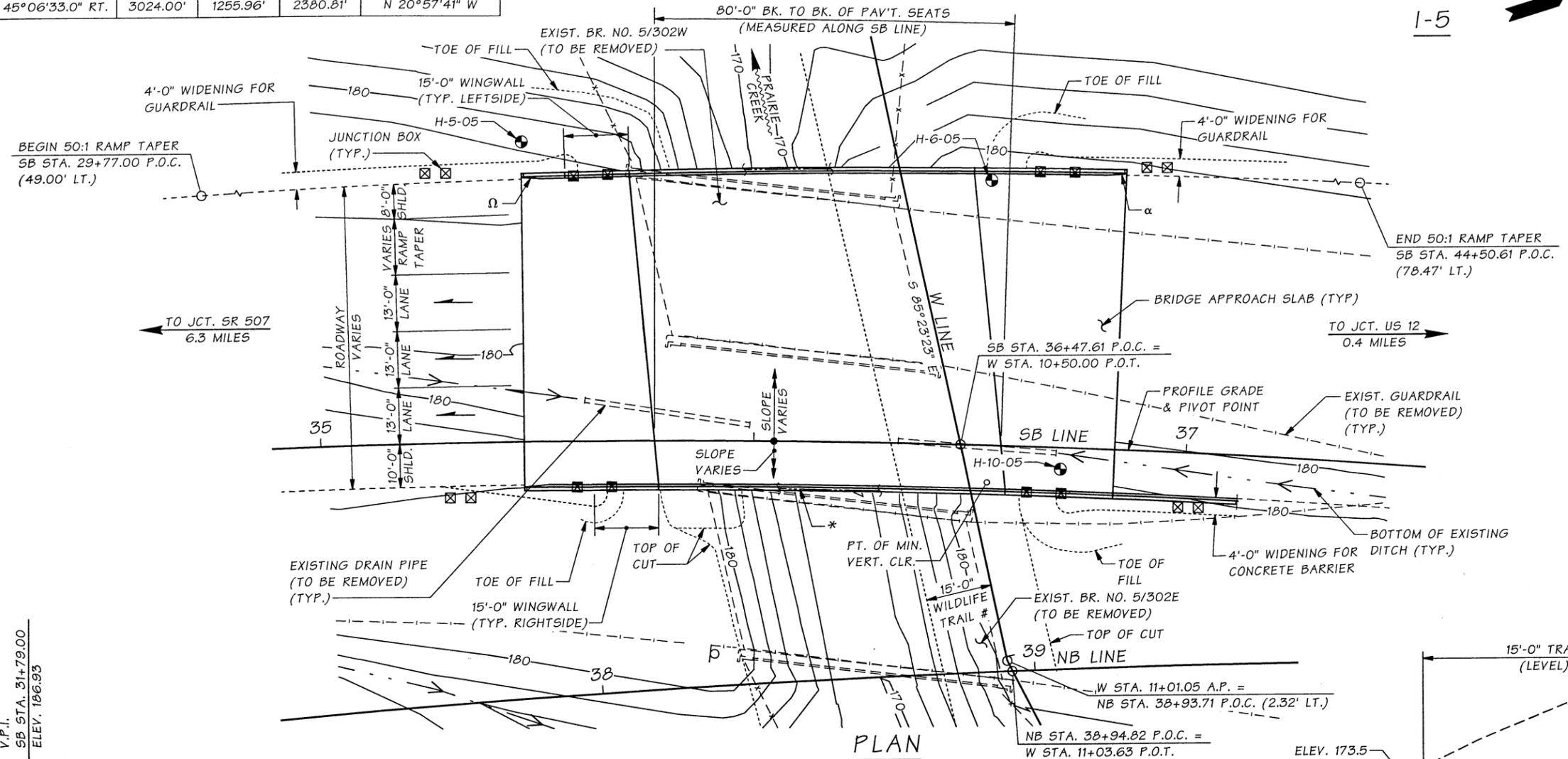
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1. Layout Plan Sheet
2. Field Notes
3. Crack Summary
4. Crack Intensity Diagram

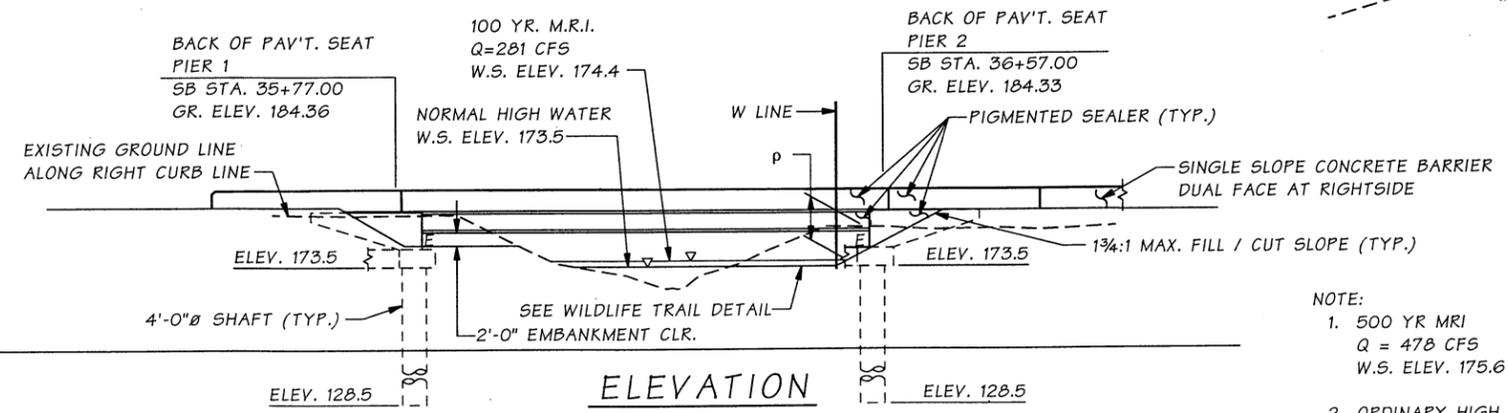
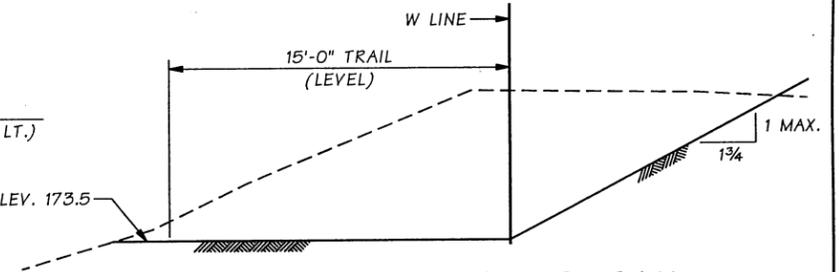
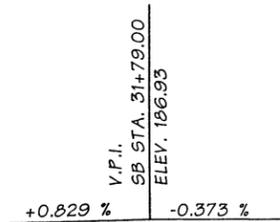
CURVE DATA					
P.I. STATION	Δ	RADIUS	TANGENT	LENGTH	BK. TANGENT BRG.
SB 29+88.49	45°06'33.0" RT.	2380.00'	988.49'	1873.78'	N 20°57'41" W
NB 32+55.96	45°06'33.0" RT.	3024.00'	1255.96'	2380.81'	N 20°57'41" W

SEC. 12, T.15N., R.3W., W.M.
THURSTON COUNTY

1-5



- * 2 ~ 2"Ø CONDUIT PIPES IN TRAFFIC BARRIER FOR FULL LENGTH OF BRIDGE & WINGWALLS (TYP.)
- # SEE WILDLIFE TRAIL DETAIL.
- p 4.5' MIN. VERT. CLR.
- Ω CONNECTION TYPE "F" (SEE STD. PLAN C-5)
- α BEAM GUARDRAIL (TYPE 31) TRANSITION SECTION TYPE 21 (SEE STD. PLAN C-25.20-00)
- ⊕ TEST HOLE
- ⊠ JUNCTION BOX NEMA 4X 5.5. (TYP.)



WILDLIFE TRAIL DETAIL
LOOKING BACK ON STATION

LEGEND

- ⊕ IDENTIFIES SECTION, VIEW OR DETAIL
- ⊠ TAKEN OR SHOWN ON BRIDGE SHEET PW15
- ⊕ TAKEN OR SHOWN ON THE SAME SHEET

P.C. GIRDERS (WF42G)
LOADING: HL-93

- NOTE:
- 500 YR MRI
Q = 478 CFS
W.S. ELEV. 175.6
 - ORDINARY HIGH WATER LEVEL
ELEV. 171.4

GRADE ELEVATIONS SHOWN ARE FINISH GRADES AT TOP OF ROADWAY SLAB ON SB LINE AND ARE EQUAL TO PROFILE GRADE. SEE STD. PLAN H-9 FOR EMBANKMENT DETAILS AT BRIDGE ENDS.

SB LINE PROFILE

DATUM
NAVD 1988

SR 5 JOB NO. 7412 SHEET PW1

Bridge Design Engr.	Khaloghi, B	M:\X-Team\GRAND MOUND TO MAYTOWN\PRAIRIE CR. BR. 5-302 w\window files\LAYOUT.WND	REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
Supervisor	Anderson, MW		10	WASH.			
Designed By	Pickett, A	06/06	JOB NUMBER				
Checked By	JB/LHT	12/06	07C501				
Detailed By	Bontemps, W	06/06					
Bridge Projects Engr.	Kirker, KN	08/05					
Prelim. Plan By	Chu, A	04/05					
Architect/Specialist	PDK/BK	08/05	DATE	REVISION	BY	APPD	

BRIDGE AND STRUCTURES OFFICE
11-21-07 EXPIRES 5/19/08



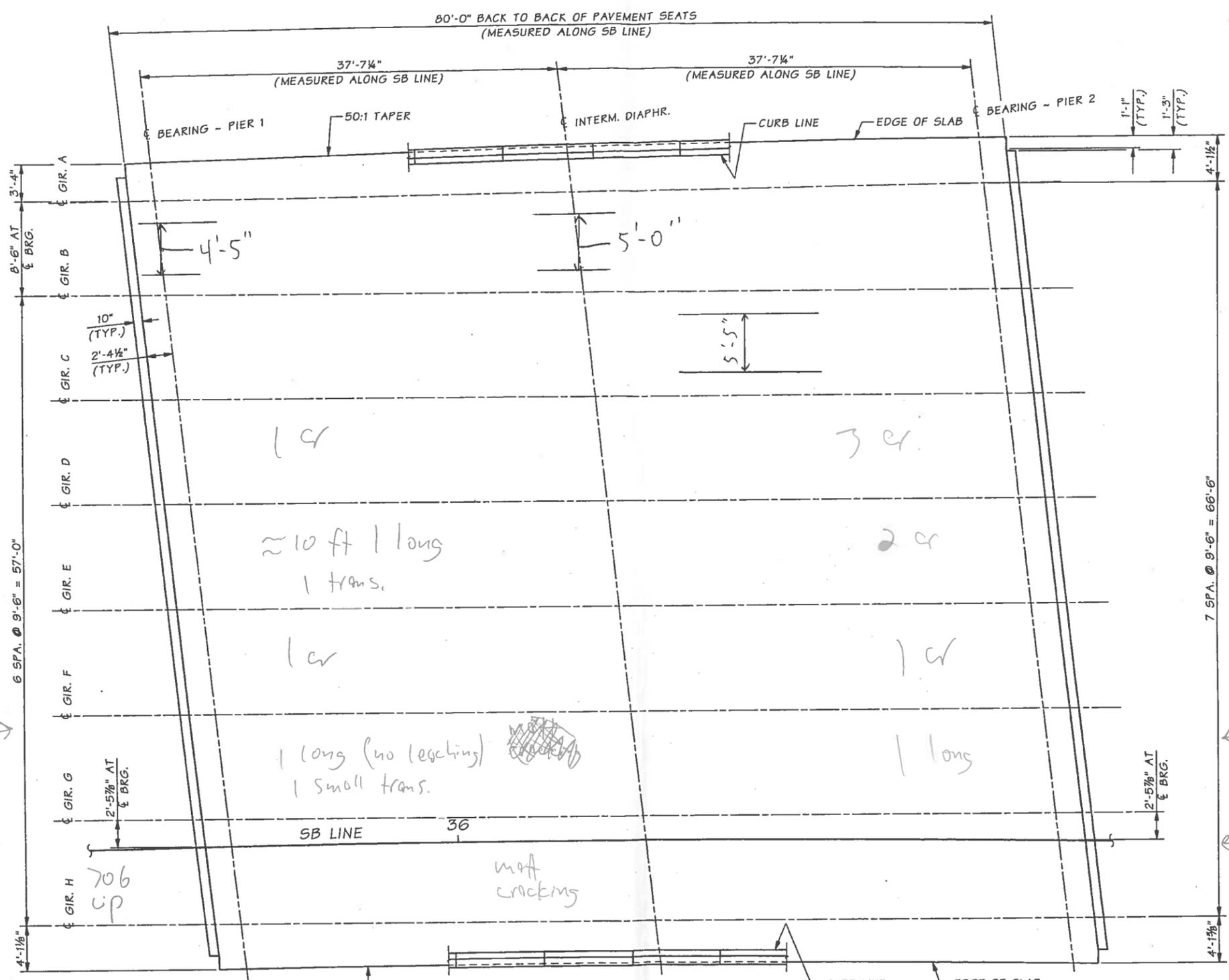
I-5 GRAND MOUND TO MAYTOWN STAGE ONE - ADD LANES PRAIRIE CREEK BRIDGE NO. 5/302W		BRIDGE SHEET NO. PW1
LAYOUT		SHEET 656 OF 772 SHEETS

C.S. 3401 ~ PROJ. NO. 013451D ~ OLYMPIC REGION ~ I-5 ~ GRAND MOUND TO MAYTOWN ~ PRAIRIE CREEK BRIDGE NO. 5/302W REPL.



91 →
 ← 92
 93 →
 ← 94
 95 →
 ← 96
 ← 97
 98 →
 ← 99
 700 →
 ← 701
 702 →
 ← 703
 704 →
 ← 705

← 74
 ← 75
 76 →
 ← 77
 78 →
 ← 79
 80 →
 ← 81
 ← 82
 83 →
 ← 84
 85 →
 ← 86
 87 →
 ← 88
 89 →
 ← 90



707 Elev
 708 deck

FRAMING PLAN

BEARING OF PIERS IS N 78°30'00" W
 BEARING OF GIRDER A IS N 17°13'59" E
 BEARING OF GIRDERS B THRU H IS N 17°57'57" E

SR 5 JOB NO. 7412 SHEET PW16

Bridge Design Engr.	Khaleghi, B	M:\X-Team\GRAND MOUND TO MAYTOWN\RAIRIE CR. BR. 5-302 W>window files\FRAMING PLAN.WND
Supervisor	Anderson, MW	
Designed By	Pickett, A	09/06
Checked By	Single, J	12/06
Detailed By	Bontemps, W	09/06
Bridge Projects Engr.		
Prelim. Plan By		
Architect/Specialist		
DATE	REVISION	BY APPD

BRIDGE AND STRUCTURES OFFICE 11/20/06
 11/19/07

Washington State Department of Transportation

I-5
 GRAND MOUND TO MAYTOWN
 STAGE ONE - ADD LANES
 PRAIRIE CREEK BRIDGE NO. 5/302W
 FRAMING PLAN

BRIDGE SHEET NO. PW16
 SHEET 671 OF 772 SHEETS



Bridge #	5/302W	Bridge Name	Prairie Creek SB			Structure ID	0017465B	
Contract #	7465	Region	SW	Project Engineer	McNutt/Engel	Performance Deck Concrete?	No	
Contractor	Scarsella Bros.		Concrete Supplier	Unknown		Deck Placement	≈ 2010	
Bridge Description	Single-Span (80'), 8-WF42G Girders, 4-Lanes (variable width roadway abt. 76' wide)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	4%
Min. =	0%
Max. =	15%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	36.00	5.00	0	18	0%
1	1	B	C	36.00	5.50	0	18	0%
1	1	C	D	36.00	5.50	1	18	5%
1	1	D	E	36.00	5.50	1	18	5%
1	1	E	F	36.00	5.50	1	18	5%
1	1	F	G	36.00	5.50	1	18	5%
1	1	G	H	36.00	5.50	0	18	0%
2	2	A	B	36.00	5.00	0	18	0%
2	2	B	C	36.00	5.50	0	18	0%
2	2	C	D	36.00	5.50	3	18	15%
2	2	D	E	36.00	5.50	2	18	10%
2	2	E	F	36.00	5.50	1	18	5%
2	2	F	G	36.00	5.50	1	18	5%
2	2	G	H	36.00	5.50	0	18	0%



	PIER 1	PIER 2
GIR. A		
GIR. B	0%	0%
GIR. C	0%	0%
GIR. D	5%	15%
GIR. E	5%	10%
GIR. F	5%	5%
GIR. G	5%	5%
GIR. H	0%	0%

CRACKING INTENSITY ~ BRIDGE 5/302W

100% = CRACK EVERY 2 FT.

LESS CRACKING



MORE CRACKING

BRIDGE NUMBER	5/302W
BRIDGE NAME	PRAIRIE CREEK SB
INSPECTION DATE	4/8/2015
DECK CONCRETE	TRADITIONAL

BRIDGE 9/133 (SR 9 OVER HARVEY CREEK ROAD)

Bridge #	9/133	Bridge Name	SR 9 over Harvey Creek Road		Structure ID	0017267A	
Contract #	7267	Region	NW	Project Engineer	Janice Fahning	Performance Deck Concrete?	No
Contractor	Scarsella Brothers		Concrete Supplier		Deck Placement		≈ 2008
Bridge Description	Single Span (180'), 6-WF83G Girders, 2-Lane (40' wide roadway)						



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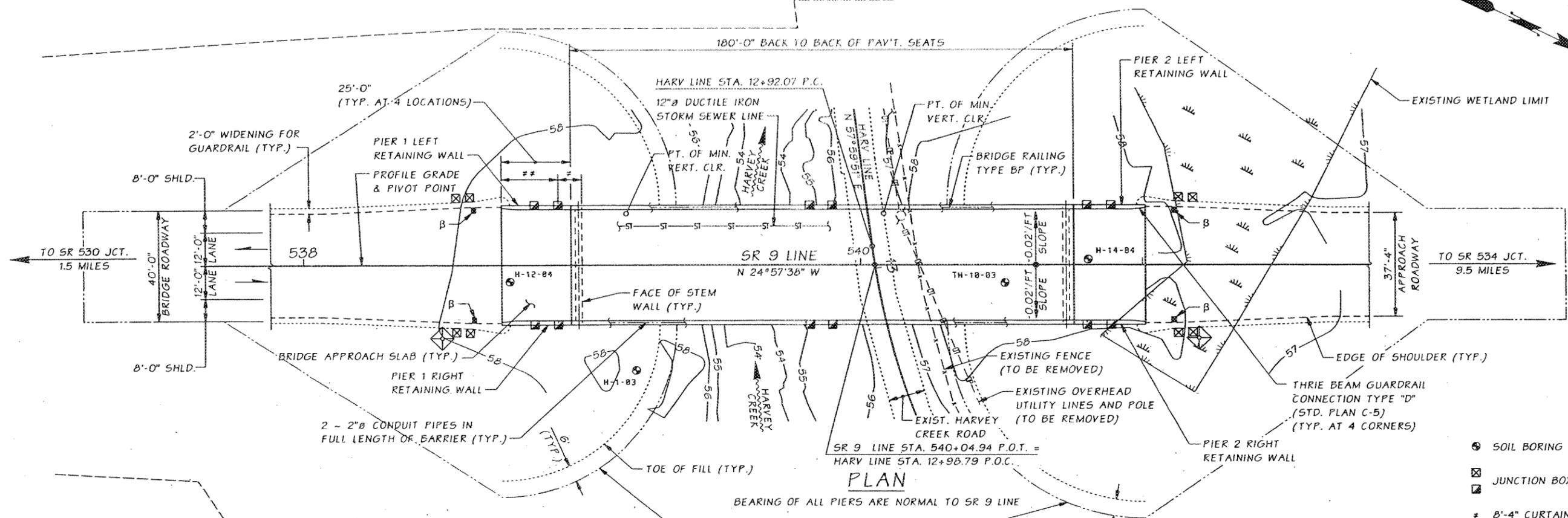
1. Layout Plan Sheet
2. Field Notes
3. Crack Summary
4. Crack Intensity Diagram

CURVE DATA

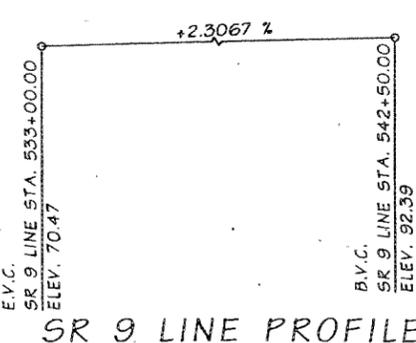
P.I. STATION	Δ	RADIUS	TANGENT	LENGTH	BK TANGENT BRG.
HARV 13+36.97	20°21'51" LT.	250.00'	44.90'	88.86'	N 57°59'51" E

SEC. 35, T.32N., R.5E., W.M.
SNOHOMISH COUNTY

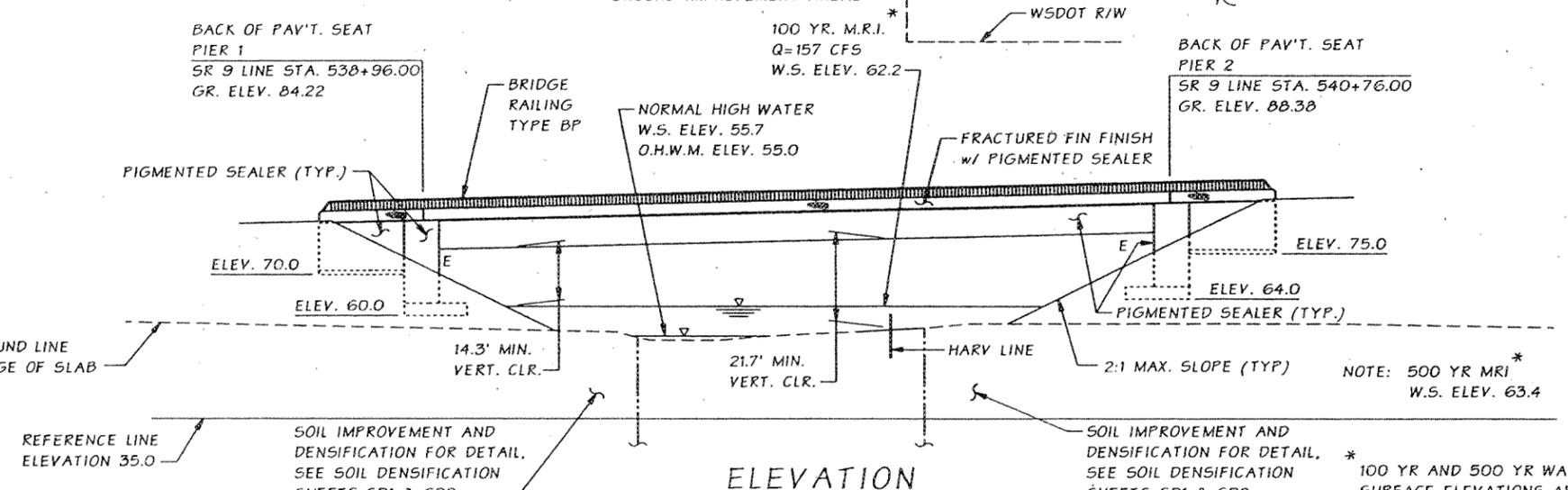
SR 9



PLAN



DATUM
NAVD 1988



GRADE ELEVATIONS SHOWN ARE FINISH GRADES AT TOP OF ROADWAY SLAB ON SR 9 LINE AND ARE EQUAL TO PROFILE GRADE. SEE STD. PLAN H-9 FOR EMBANKMENT DETAILS AT BRIDGE ENDS.

LEGEND

- ⊙ SOIL BORING LOCATION
- ⊠ JUNCTION BOXES
- * 8'-4" CURTAIN WALL (TYP. AT 4 LOCATIONS)
- ** 20'-6" RETAINING WALL (TYP. AT 4 LOCATIONS)
- β CATCH BASIN, SEE DRAINAGE PLANS FOR DETAILS.
- ⊙ IDENTIFIES SECTION, VIEW OR DETAIL
- ⊙ B 15 TAKEN OR SHOWN ON BRIDGE SHEET 15
- ⊙ B - TAKEN OR SHOWN ON THE SAME SHEET

P.C. GIRDERS (W83G)
LOADING: HL-93

SHEET 1

Bridge Design Engr.	Khaleghi, B	M:\Y-Team\SR9 HARVEY CREEK RD\window files\LAYOUT.WND
Supervisor	Stoddard, RB	
Designed By	Lee, CS	09/06
Checked By	Hinns, GEC	09/06
Detailed By	Footo, N	09/06
Bridge Projects Engr.	Lewis, RA	09/06
Prelim. Plan By	Lee, CS	09/06
Architect/Specialist	Kindersaan, P	09/06

REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
10	WASH.			
JOB NUMBER				
06A033				

BRIDGE AND STRUCTURES OFFICE

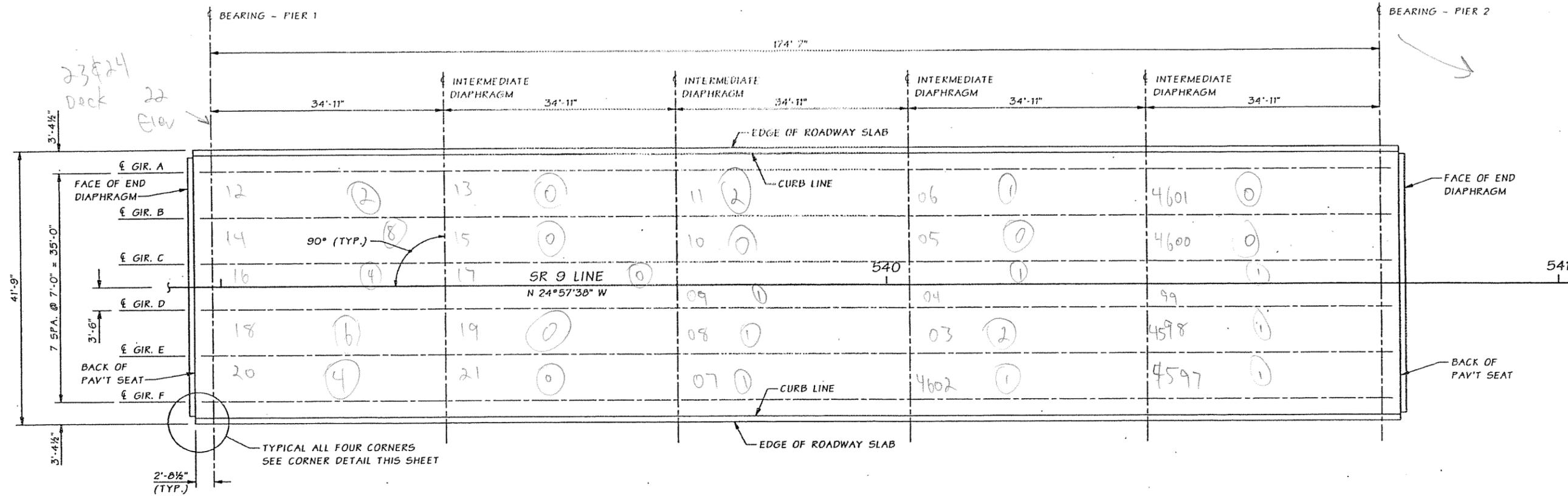
Washington State Department of Transportation

SR 9
SCHLOMAN ROAD TO 256TH ST NE
AND 268TH ST INTERSECTION
HARVEY CREEK BRIDGE

LAYOUT

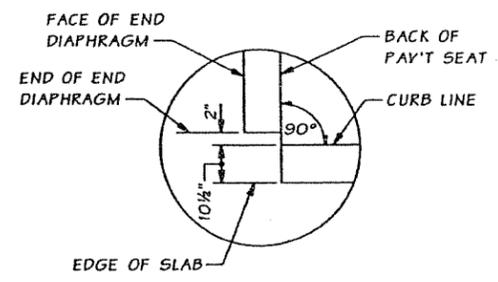
BRIDGE SHEET NO.	1
SHEET	216
OF	267
SHEETS	

C.S. 3135 - PROJ. NO. XL 1273A - NORTHWEST REGION - SR 9 - SCHLOMAN ROAD VICINITY TO 256TH ST. NE & 268TH ST. NE - HARVEY CR. RD/ARMSTRONG CR. OVERCROSSING



FRAMING PLAN

BEARING OF PIERS AND DIAPHRAGMS IS NORMAL TO SR 9 LINE



CORNER DETAIL

SR 9 JOB NO. SHEET 17

Bridge Design Engr.	Khaleghi, B	M:\Y-Team\SR9 HARVEY CREEK RD\window files\FRAMING PLAN.WND		RECORD NO.	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
Supervisor	Stoddard, RB			10	WASH.			
Designed By	Lee, CS	09/06						
Checked By	HINNS, GEC	09/06						
Detailed By	Foote, N	09/06						
Bridge Projects Engr.								
Prekm. Plan By								
Architect/Specialist								
DATE	REVISION	BY	APP'D					

BRIDGE AND STRUCTURES OFFICE

Professional Engineer Seal: **SHYUAN-SHEW**, No. 0074, Expires 2/6/08

Professional Engineer Seal: **SHYUAN-SHEW**, No. 0074, Expires 6/5/08

Professional Engineer Seal: **SHYUAN-SHEW**, No. 0074, Expires 6/5/08

Washington State Department of Transportation

SR 9
SCHLOMAN ROAD TO 256TH ST NE
AND 268TH ST INTERSECTION
HARVEY CREEK BRIDGE

FRAMING PLAN

BRIDGE SHEET NO.	17
SHEET	232
OF	267
SHEETS	

Fri Dec 06 14:41:54 2006



Bridge #	9/133	Bridge Name	SR 9 over Harvey Creek Road			Structure ID	0017267A	
Contract #	7267	Region	NW	Project Engineer	Janice Fahning	Performance Deck Concrete?	No	
Contractor	Scarsella Brothers		Concrete Supplier				Deck Placement	≈ 2008
Bridge Description	Single Span (180'), 6-WF83G Girders, 2-Lane (40' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	8%
Min. =	0%
Max. =	45%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	34.92	7.00	2	17	10%
1	1	B	C	34.92	7.00	8	17	45%
1	1	C	D	34.92	7.00	4	17	25%
1	1	D	E	34.92	7.00	6	17	35%
1	1	E	F	34.92	7.00	4	17	25%
1	2	A	B	34.92	7.00	0	17	0%
1	2	B	C	34.92	7.00	0	17	0%
1	2	C	D	34.92	7.00	0	17	0%
1	2	D	E	34.92	7.00	0	17	0%
1	2	E	F	34.92	7.00	0	17	0%
1	3	A	B	34.92	7.00	2	17	10%
1	3	B	C	34.92	7.00	0	17	0%
1	3	C	D	34.92	7.00	1	17	5%
1	3	D	E	34.92	7.00	1	17	5%
1	3	E	F	34.92	7.00	1	17	5%
1	4	A	B	34.92	7.00	1	17	5%
1	4	B	C	34.92	7.00	0	17	0%
1	4	C	D	34.92	7.00	1	17	5%
1	4	D	E	34.92	7.00	2	17	10%
1	4	E	F	34.92	7.00	1	17	5%
1	5	A	B	34.92	7.00	0	17	0%
1	5	B	C	34.92	7.00	0	17	0%
1	5	C	D	34.92	7.00	1	17	5%
1	5	D	E	34.92	7.00	1	17	5%
1	5	E	F	34.92	7.00	1	17	5%



	PIER 1		PIER 2		
GIR. A					
GIR. B	10%	0%	10%	5%	0%
GIR. C	45%	0%	0%	0%	0%
GIR. D	25%	0%	5%	5%	5%
GIR. E	35%	0%	5%	10%	5%
GIR. F	25%	0%	5%	5%	5%

CRACKING INTENSITY ~ BRIDGE 9/133

100% = CRACK EVERY 2 FT.

LESS CRACKING

MORE CRACKING



BRIDGE NUMBER	9/133
BRIDGE NAME	SR 9 OVER HARVEY CREEK ROAD
INSPECTION DATE	5/22/2015
DECK CONCRETE	TRADITIONAL

BRIDGE 5/229 (MELLEN STREET COUPLET)

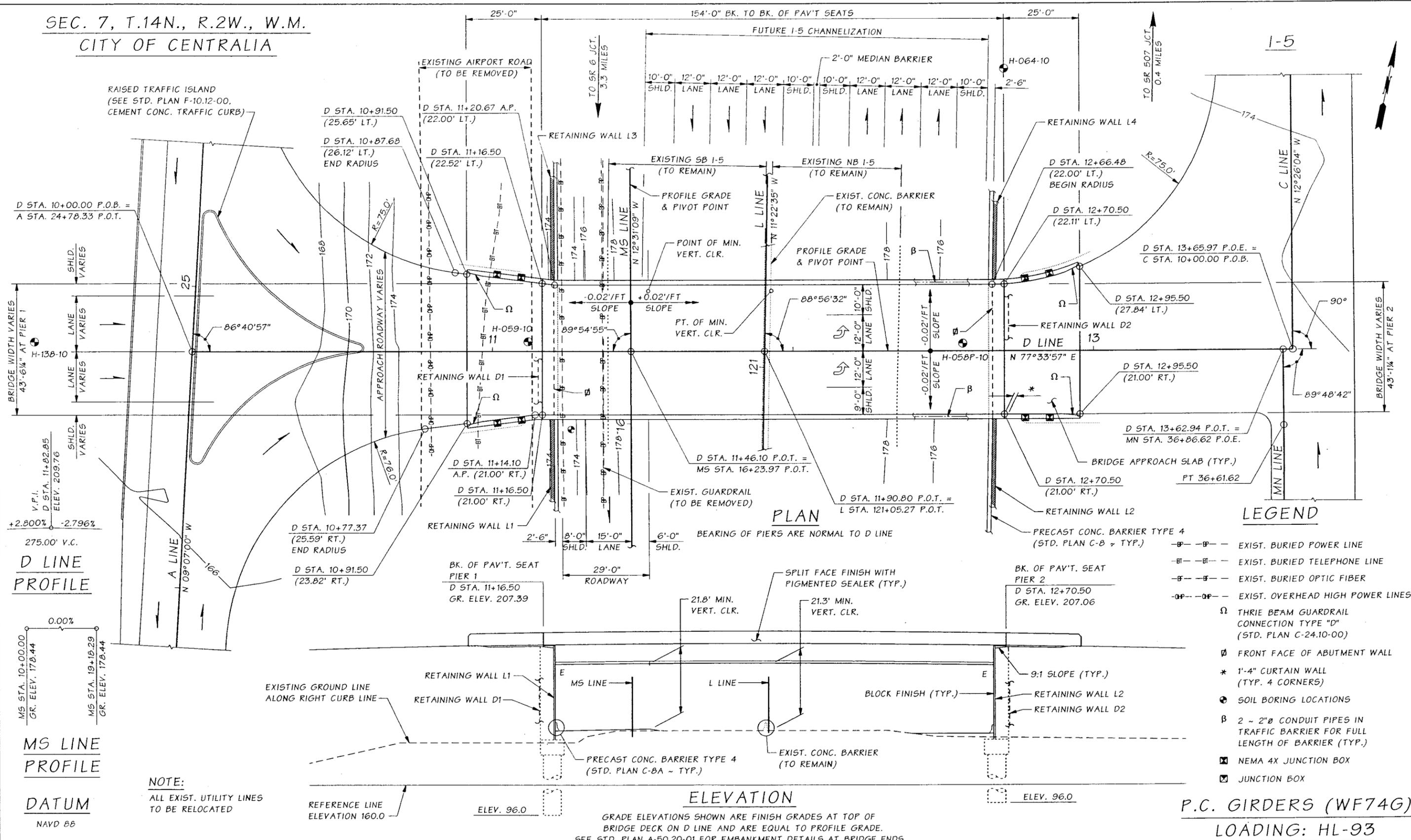
Bridge #	5/229	Bridge Name	Mellen Street Couplet Bridge		Structure ID	0018473B	
Contract #	8473	Region	SW	Project Engineer	Colin Newell	Performance Deck Concrete?	YES
Contractor	Scarella Bros.	Concrete Supplier	Miles Sand & Gravel		Deck Placement	4/18/2014	
Bridge Description	Single-Span (154'), 5-WF74G Girders, 2-Lanes (43' wide roadway)						



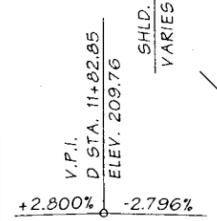
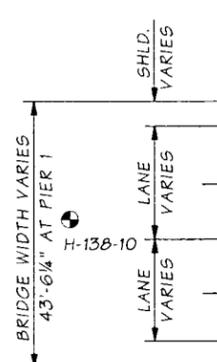
CONTENTS

1. Layout Plan Sheet
2. Mix Design Summary
3. Concrete Mix Design Form
4. Concrete Test Results
5. Field Notes
6. Crack Summary
7. Crack Intensity Diagram

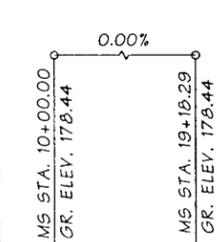
SEC. 7, T.14N., R.2W., W.M.
CITY OF CENTRALIA



D STA. 10+00.00 P.O.B. =
A STA. 24+78.33 P.O.T.



D LINE PROFILE



MS LINE PROFILE

DATUM
NAVD 88

NOTE:
ALL EXIST. UTILITY LINES
TO BE RELOCATED

REFERENCE LINE
ELEVATION 160.0

ELEV. 96.0

ELEVATION

GRADE ELEVATIONS SHOWN ARE FINISH GRADES AT TOP OF
BRIDGE DECK ON D LINE AND ARE EQUAL TO PROFILE GRADE.
SEE STD. PLAN A-50.20-01 FOR EMBANKMENT DETAILS AT BRIDGE ENDS.

P.C. GIRDERS (WF74G)
LOADING: HL-93

SR 5 FILE NO. 7479 SHEET C1

Bridge Design Engr.	Khaleghi, B	M:\X-Team\MELLEN TO BLAKESLEE JCT\COUPLER BR>window files\LAYOUT.wnd			
Supervisor	Khaleghi, B	REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.
Designed By	Chu, A	10	WASH.		TOTAL SHEETS
Checked By	Nash, PM				
Detailed By	DL/DJM				
Bridge Projects Engr.	Lewis, RA	JOB NUMBER	13X300		
Prelim. Plan By	Wei, J				
Architect/Specialist	PDK/BSA/GAW	DATE	REVISION	BY	APPD

BRIDGE AND STRUCTURES OFFICE

Washington State Department of Transportation

3/27/13

I-5
MELLEN STREET TO
BLAKESLEE JUNCTION - STAGE 2
COUPLER BRIDGE OVER I-5
LAYOUT

BRIDGE SHEET NO. C1
SHEET 783 OF 904 SHEETS



Contractor Scarcella Bros		Submitted By SB Structures	Date 3-26-2014
Concrete Supplier Miles Sand & Gravel		Plant Location Rochester	
Contract Number 8473	Contract Name I-5/Mellen Street to Blakeslee Junction - Stage 2		

This mix is to be used in the following Bid Item No(s): 86 & 87

Concrete Class: (check one only)

- 3000
 4000
 4000^a
 4000^aP
 4000W
 Concrete Overlay
 Cement Concrete Pavement^d
 Other Shrinkage Reducer

Remarks: _____

Mix Design No. 0444AFL2 Plant No. 222

Cementitious Materials	Source	Type, Class or Grade	Sp. Gr.	Lbs/cy
Cement	Ash Grove	I-II	3.15	464
Fly Ash ^a	Lafarge	F	2.54	116
GGBFS (Slag)				
Latex				
Microsilica				

Concrete Admixtures	Manufacturer	Product	Type	Est. Range (oz/cy)
Air Entrainment	BASF	MB-AE-90		1-15
Water Reducer				
High-Range Water Reducer	BASF	Glenium 7500	F	23-40
Set Retarder				
Other Shrinkage Reducer	BASF	MasterLife SRA		32

Water (Maximum) 233 lbs/cy Is any of the water Recycled or Reclaimed? Yes^e No

Water Cementitious Ratio (Maximum) 0.40 Mix Design Density 145.5 lbs/cf^d

Design Performance	1	2	3	4	5	Average ^f
28 Day Compressive Strength (cylinders) psi	4,920	5,420	5,330	6,290	5,860	5,560
14 Day Flexural ^d Strength (beams) psi						

Agency Use Only (Check appropriate Box)

- This Mix Design MEETS CONTRACT SPECIFICATIONS and may be used on the bid items noted above
 This Mix Design DOES NOT MEET CONTRACT SPECIFICATIONS and is being returned for corrections

Reviewed By: _____ PE Signature _____ Date _____

Aggregate Information

Concrete Aggregates	Component 1	Component 2	Component 3	Component 4	Component 5	Combined Gradation
WSDOT Pit No.	B-333	B-333	B-333	B-333		
WSDOT ASR 14-day Results (%) ^b	<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No				
Grading ^c	4	57	8	Class 2		
Percent of Total Aggregate						100%
Specific Gravity	2.71	2.69	2.68	2.65		
Lbs/cy (ssd)	480	1040	500	1100		

Percent Passing

2 inch	100	100	100	100		100
1-1/2 inch	100	100	100	100		100
1 inch	32.6	100	100	100		89.6
3/4 inch	1.6	80.0	100	100		78.2
1/2 inch	0.4	30.1	100	100		61.4
3/8 inch	0.2	7.8	88.6	100		52.1
No. 4	0.1	0.3	22.4	99.4		38.8
No. 8	0.1	0.2	1.4	90.2		32.1
No. 16	0.1	0.1	0.2	70		24.8
No. 30	0.1	0.1	0.2	44.1		15.6
No. 50	0.1	0.1	0.2	20		7.1
No. 100	0.1	0.1	0.2	6		2.2
No. 200	0.1	0.1	0.2	1.7		0.7

Fineness Modulus: 2.70 (Required for Class 2 Sand)

ASR Mitigation Method Proposed^b: _____

Notes:

- a Required for Class 4000D and 4000P mixes.
- b Alkali Silica Reactivity Mitigation is required for sources with expansions over 0.20% - Indicate method for ASR mitigation. For expansion of 0.21% - 0.45%, acceptable mitigation can be the use of low alkali cement or 25% type F fly ash. Any other proposed mitigation method or for pits with greater than 0.45% expansion, proof of mitigating measure, either ASTM C1260 / AASHTO T303 test results must be attached. If ASTM C 1293 testing has been submitted indicating 1-year expansion of 0.04% or less, mitigation is not required.
- c AASHTO No. 467, 57, 67, 7, 8; WSDOT Class 1, Class 2; or combined gradation. See Standard Specification 9-03.1.
- d Required for Cement Concrete Pavements.
- e Attach test results indicating conformance to Standard Specification 9-25.1.
- f Actual Average Strength as determined from testing or estimated from ACI 211.

Carlson Testing, Inc.

Bend Office (541) 330-9155
Geotechnical Office (503) 601-8250
Eugene Office (541) 345-0289
Salem Office (503) 589-1252
Tigard Office (503) 684-3460

October 25, 2013
T1309423

Ashgrove Cement
5 Centerpoint Dr. Suite 350
Lake Oswego, OR 97035

Attn: Dave Berg

Re: **Modulus of Elasticity - ASTM C469**
Miles Sand & Gravel Special 4000D
Report Reference # D-092313-1
WSDOT 4000D Specifications

As requested, Carlson Testing Inc. has completed modulus of elasticity testing on the 6x12 concrete cylinders referenced above. The lab cylinders were cast on September 23, 2013 and delivered to our Tigard facility. Twenty eight day modulus testing was done on October 21, 2013. Following are the results:

Modulus of Elasticity Testing: ASTM C469

AGE OF SPECIMEN	AVE PSI	MODULUS - CYL A	MODULUS - CYL B	AVERAGE MODULUS ELASTICITY
28 DAYS	4160	5.18E + 06	5.28E + 06	5.23E + 06

*Attached are the modulus graphs

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If there are any further questions regarding this matter, please do not hesitate to contact this office.

Respectfully submitted,

CARLSON TESTING, INC.



Greg Leeper
Project Manager

(Attachments)

ASH GROVE CEMENT COMPANY

TECHNICAL SERVICE

Portland Lab
3737 N. Port Center Way
Portland, OR 97217

ASTM C 157 - Standard Test Method for Length Change of Hardened Hydraulic-Cement Mortar and Concrete

Subject

On 2/12/2013 we performed a laboratory trial batch for drying shrinkage testing for Mr. Keith Muhich with Miles Sand & Gravel.

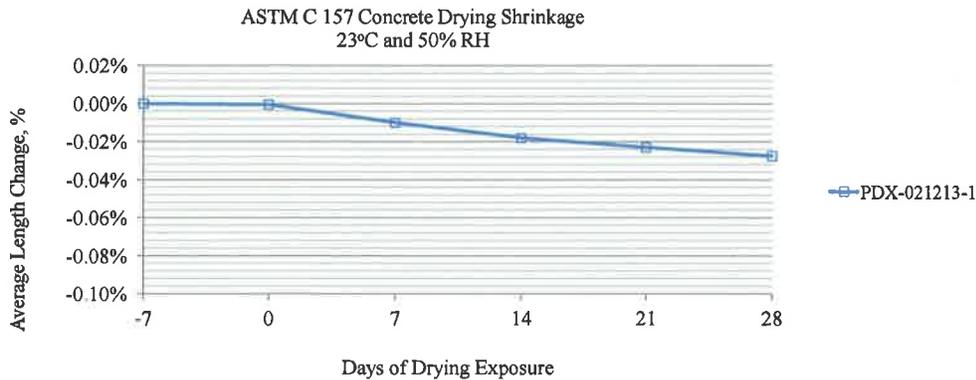
Summary

The concrete laboratory trial batch was prepared according to your mix design 4000D with 0.25 gallon of SRA per cubic yard. The beams were cured in standard water bath for 28 days prior to drying exposure.

Test Results

Length Change, %: Age, days **PDX-021213-1**

Initial	0.000%
0	0.000%
7	-0.010%
14	-0.018%
21	-0.023%
28	-0.028%



Submitted by,

David Burg

David Burg
Technical Services Manager

The statements in this report are based on information provided by customer(you), on laboratory tests and observations. They are intended solely for informational use by our customer. This report is not intended for publication or other distribution, and does not constitute, nor may it be used as any form of expert opinion. By providing these test results to you, Ash Grove makes no express or implied warranties of any kind concerning the results or conclusions of its material testing. If you require such information, you should consult an independent commercial testing laboratory. Any unauthorized use, disclosure, manipulation, or copying of this report, is strictly prohibited.



Ash Grove Technical Center
 11011 Cody Street, Suite 125
 Overland Park, Kan. 66210
 July 26, 2013 – Preliminary Report
 August 26, 2013 – Final Report

Report No.: R18785
Work Order No.: WO-130315

SUBJECT

On July 8, 2013, a request for technical service was issued on behalf of Mr. Keith Muhich of Miles Sand and Gravel in Auburn, Washington. Mr. Dave Burg requested that the Technical Center conduct AASHTO T 277 testing on the two supplied cylinders, 1 @ 28 days, and 2 @ 56 days of age.

SAMPLE IDENTIFICATION

<u>Sample No.</u>	<u>Sample Description</u>	<u>Date Received</u>
S-130851	(3) 4x8 Concrete Cylinders, Cast 6-27-13, labeled WSDOT 4000D mix design.	07/08/2013

TEST RESULTS

AASHTO T 277 - Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration
Accelerated Cure

<u>Sample No.</u>	<u>Diameter, in.</u>	<u>Charge Passed, C</u>	<u>Corrected Charge, C</u>	<u>Qualitative Equivalent</u>	<u>Date of Test</u>	<u>Age, days</u>
S-130851 *	4.03	987	855	Very Low	07/25/2013	28

* Acc. Curing started at 11 days of age.
 Cylinders were received at 11 days of age.

AASHTO T 277 - Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration
Standard Cure

<u>Sample No.</u>	<u>Diameter, in.</u>	<u>Charge Passed, C</u>	<u>Corrected Charge, C</u>	<u>Qualitative Equivalent</u>	<u>Date of Test</u>	<u>Age, days</u>
S-130851	4.02	1,297	1,129	Low	08/22/2013	56
S-130851	4.03	1,236	1,070	Low	08/22/2013	56

Note: Corrected Charge = Charge Passed X (95/diameter in mm)²
 1 in. = 25.4 mm

**Chloride Ion Penetrability Based on Charge Passed
(Excerpted from AASHTO T 277)**

<u>Charge Passed (coulombs)</u>	<u>Chloride Ion Penetrability</u>
> 4,000	High
2,000 – 4,000	Moderate
1,000 – 2,000	Low
100 – 1,000	Very Low
< 100	Negligible

METHODOLOGY

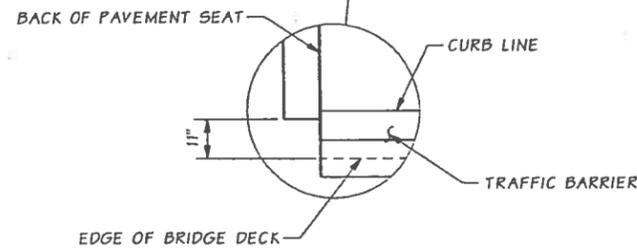
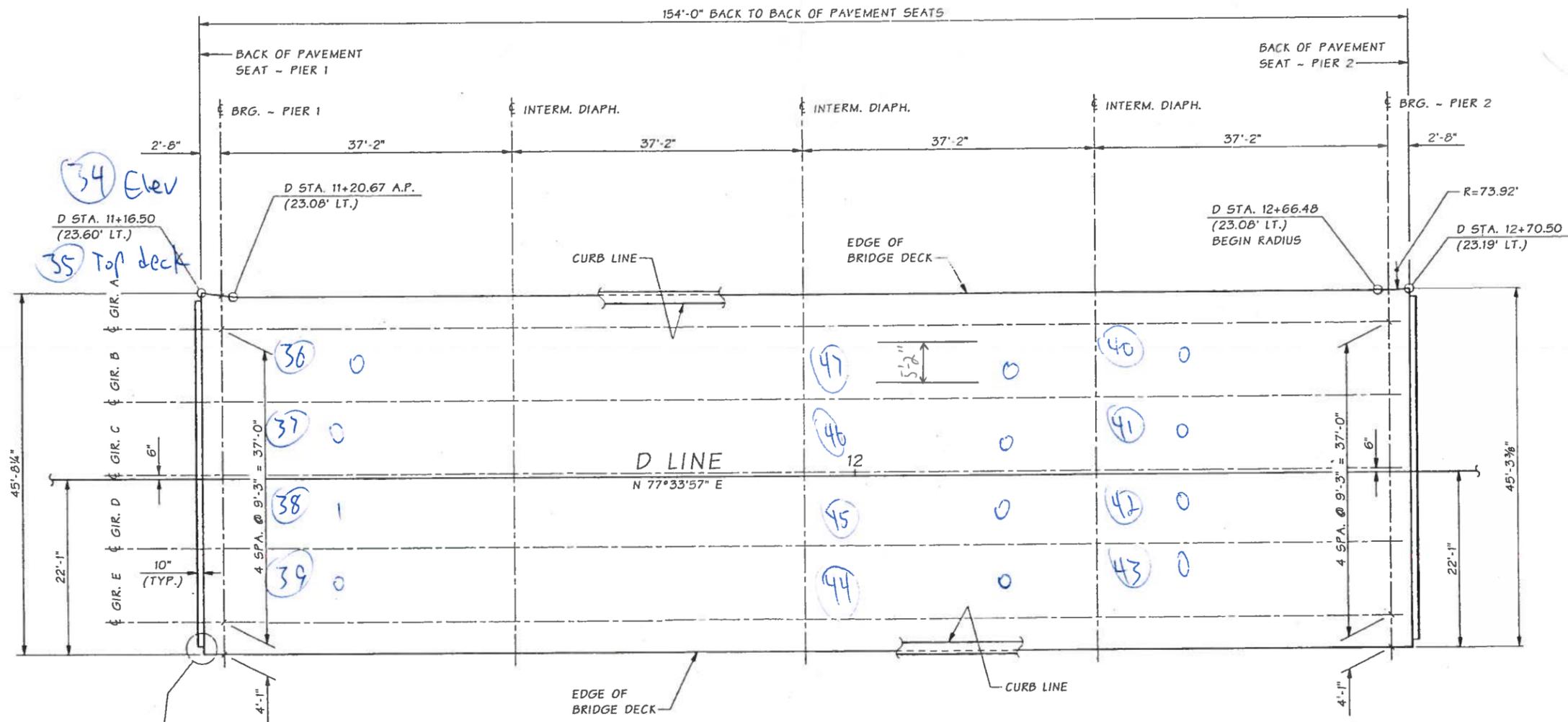
AASHTO T 277 Standard Test Method for Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration by Bruce Payne.

Submitted by,

Kristen Freeman

Kristen Freeman
Geologist/Petrographer

The statements in this report are based on information provided by our customer (You), on laboratory tests and observations. They are intended solely for informational use by our customer. This report is not intended for publication or other distribution, and does not constitute, nor may it be used as any form of expert opinion. By providing these test results to You, Ash Grove makes no express or implied warranties of any kind concerning the results or conclusions of its material testing. If You require such information, You should consult an independent commercial testing laboratory. Any unauthorized use, disclosure, manipulation, or copying of this report, in any form, is strictly prohibited.



NOTE:
OTHERS CORNERS SIMILAR.

FRAMING PLAN

BEARING OF PIERS ARE NORMAL TO D LINE

SR 5 FILE NO. 7479 SHEET C13

Bridge Design Engr.	khalleghi, B	M:\X-Team\MELLEN TO BLAKESLEE JCT\COUPLER BR>window files\FRAMING PLANS.wnd			
Supervisor	khalleghi, B	REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.
Designed By	Chu, A 05/11	10	WASH.		
Checked By	Nash, PM 10/12	JOB NUMBER 13X300			
Detailed By	McCarthy, DJ 05/11				
Bridge Projects Engr.					
Prelim. Plan By					
Architect/Specialist	DATE	REVISION	BY	APPD	



BRIDGE AND STRUCTURES OFFICE



I-5
MELLEN STREET TO
BLAKESLEE JUNCTION - STAGE 2
COUPLER BRIDGE OVER I-5
FRAMING PLAN

BRIDGE SHEET NO.
C13
SHEET 795 OF 904 SHEETS



Bridge #	5/229	Bridge Name	Mellen Street Couplet Bridge			Structure ID	0018473B	
Contract #	8473	Region	SW	Project Engineer	Colin Newell	Performance Deck Concrete?	YES	
Contractor	Scarella Bros.		Concrete Supplier	Miles Sand & Gravel		Deck Placement	4/18/2014	
Bridge Description	Single-Span (154'), 5-WF74G Girders, 2-Lanes (43' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr} / N_{100} (rounded to the nearest 5%)

Avg. =	0%
Min. =	0%
Max. =	5%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	37.17	9.25	0	19	0%
1	1	B	C	37.17	9.25	0	19	0%
1	1	C	D	37.17	9.25	1	19	5%
1	1	D	E	37.17	9.25	0	19	0%
1	2	A	B	37.17	9.25	#N/A	19	#N/A
1	2	B	C	37.17	9.25	#N/A	19	#N/A
1	2	C	D	37.17	9.25	#N/A	19	#N/A
1	2	D	E	37.17	9.25	#N/A	19	#N/A
1	3	A	B	37.17	9.25	0	19	0%
1	3	B	C	37.17	9.25	0	19	0%
1	3	C	D	37.17	9.25	0	19	0%
1	3	D	E	37.17	9.25	0	19	0%
1	4	A	B	37.17	9.25	0	19	0%
1	4	B	C	37.17	9.25	0	19	0%
1	4	C	D	37.17	9.25	0	19	0%
1	4	D	E	37.17	9.25	0	19	0%



	PIER 1			PIER 2
GIR. A				
GIR. B	0%	X X X	0%	0%
GIR. C	0%	X X X	0%	0%
GIR. D	5%	X X X	0%	0%
GIR. E	0%	X X X	0%	0%

CRACKING INTENSITY ~ BRIDGE 5/229

100% = CRACK EVERY 2 FT.

X X X = CRACKS NOT COUNTED DUE TO LIMITED ACCESS

LESS CRACKING

MORE CRACKING



BRIDGE NUMBER	5/229
BRIDGE NAME	MELLEN STREET COUPLET BRIDGE
INSPECTION DATE	4/8/2015
DECK CONCRETE	PERFORMANCE BASED

BRIDGE 101/31 (MIDDLE NEMAH RIVER)

Bridge #	101/31	Bridge Name	Middle Nemah River	Structure ID	0018464A		
Contract #	8344	Region	SW	Project Engineer	Lori Figone	Performance Deck Concrete?	YES
Contractor	SB Structures	Concrete Supplier	Bayview Redi Mix, Inc	Deck Placement	1/14/2014		
Bridge Description	Single-Span, 5-WF50G Girders (127' bridge length), 2-Lanes (36' wide roadway)						



CONTENTS

1. Layout Plan Sheet
2. Mix Design Summary
3. Concrete Mix Design Form
4. Concrete Test Results
5. Field Notes
6. Crack Summary
7. Crack Intensity Diagram

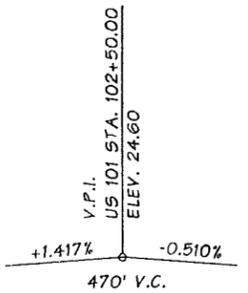
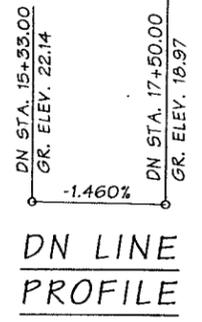
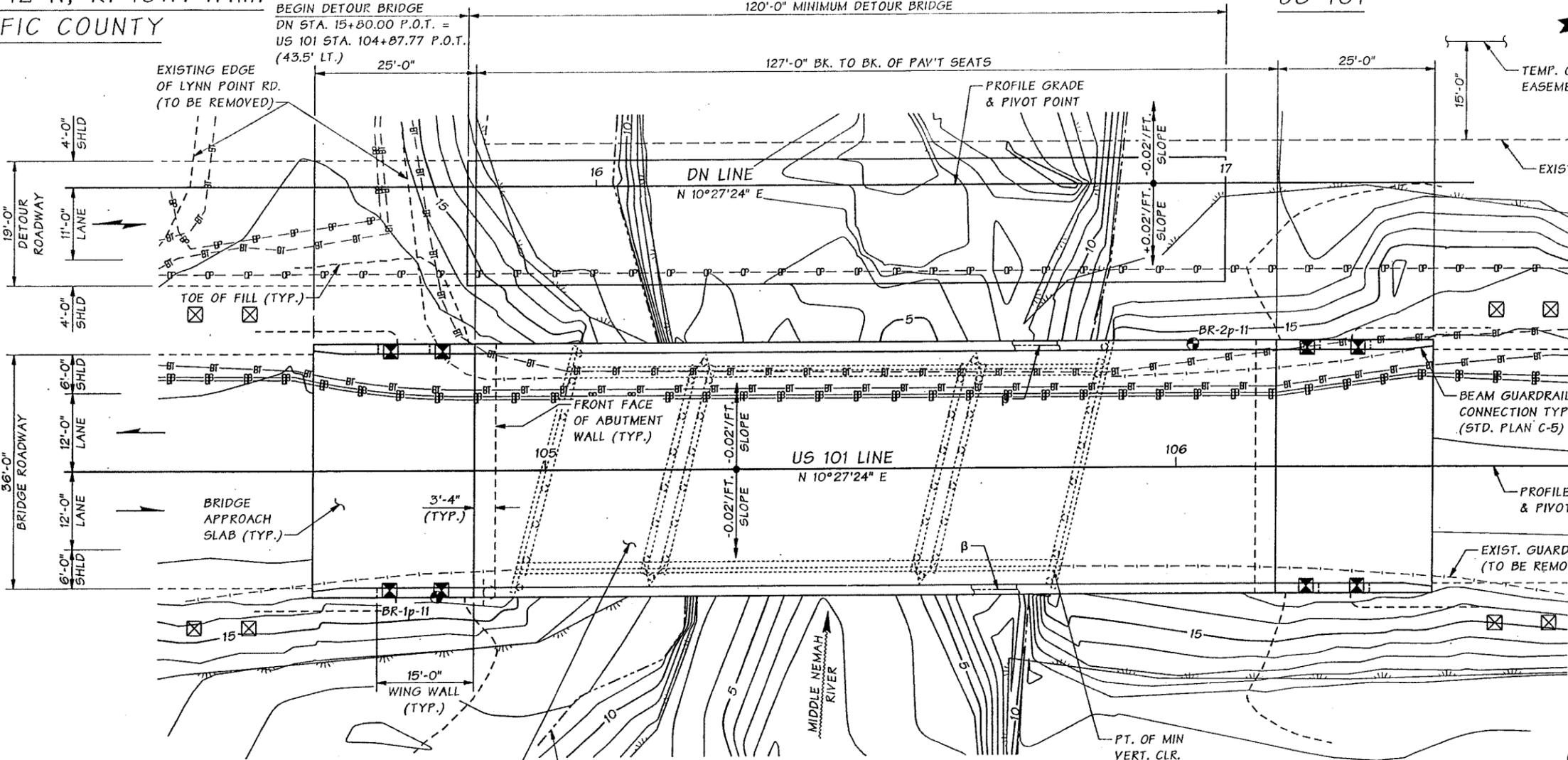
SEC. 27, T. 12 N, R. 10W. W.M.
PACIFIC COUNTY

US 101



DETOUR BRIDGE NOTE:

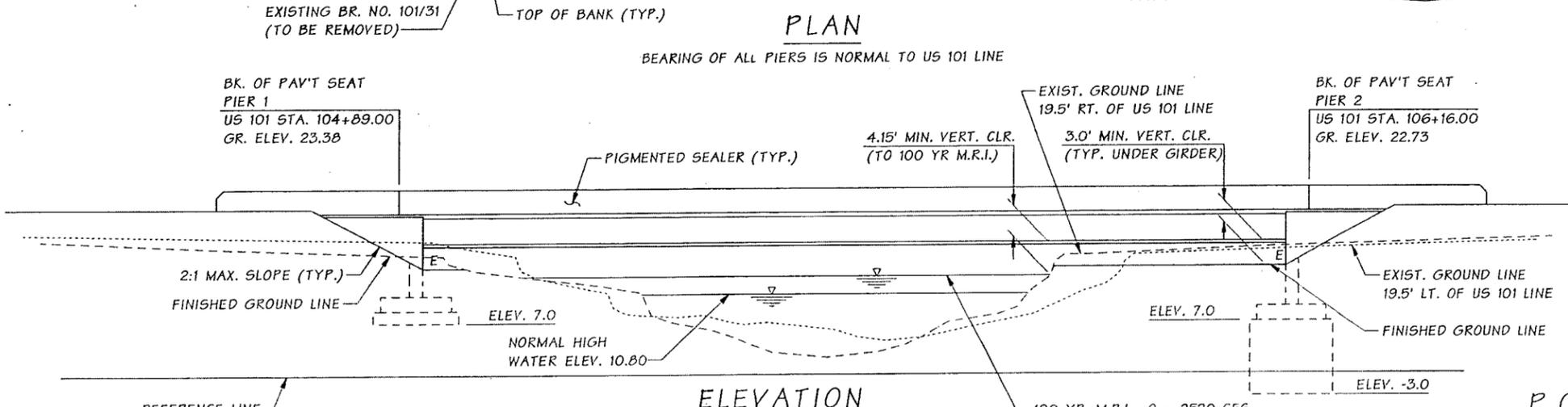
- MIN. HORIZONTAL CLEAR SPAN SHALL CLEAR NORMAL HIGH W.S. LIMIT.
- MIN. VERT. CLR. SHALL CLEAR NORMAL HIGH W.S. ELEV.



DATUM
NAVD 88

LEGEND

- B 2 - 2" CONDUIT PIPES IN TRAFFIC BARRIER
- EXIST. OVERHEAD POWER (TO BE RELOCATED)
- EXIST. UNDERGROUND TELEPHONE CABLE (TO BE RELOCATED)
- EXIST. UNDERGROUND POWER (TO BE RELOCATED)
- WETLAND BOUNDARY
- ⊙ SOIL BORING
- ⊠ JUNCTION BOX NEMA 4X 5.5
- ⊡ JUNCTION BOX



ELEVATION

GRADE ELEVATIONS SHOWN ARE FINISH GRADES AT TOP OF BRIDGE DECK ON US 101 LINE AND ARE EQUAL TO PROFILE GRADE. SEE STD. PLAN A-50.10-00 FOR EMBANKMENT DETAILS AT BRIDGE ENDS.

P.C. GIRDERS (WF50G)
LOADING: HL-93

SR US101 FILE NO. 7061 SHEET BR1

Bridge Design Engr.	Khaloghi, B	M:\Y-Team\US 101 - NEMAH RIVER REPL\window files\LAYOUT.wnd			
Supervisor	Anderson, MW	REGION	STATE	FED. AID PROJ. NO.	SHEET NO.
Designed By	Sargent, S	10	WASH.		TOTAL SHEETS
Checked By	Martin, J	JOB NUMBER			
Detailed By	Hettle, J	12X303			
Bridge Projects Engr.		DATE	REVISION	BY	APPD
Prelim. Plan By					
Architect/Specialist					

BRIDGE AND STRUCTURES OFFICE



Washington State Department of Transportation

US 101
MIDDLE NEMAH RIVER BR.
REPLACE BRIDGE
MIDDLE NEMAH R BR. NO. 101/31 REPL.
LAYOUT

BRIDGE SHEET NO.	BR1
SHEET	50
OF	83
SHEETS	

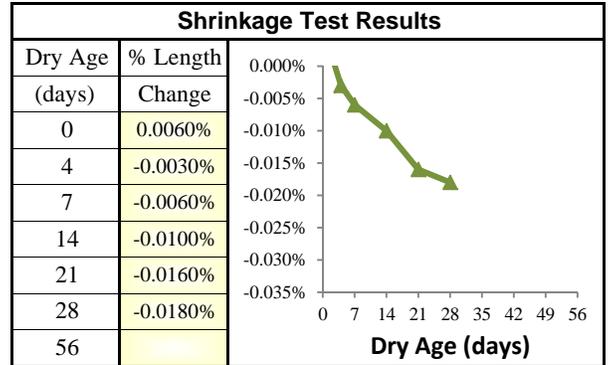
C. S. 2501 ~ PROJ. NO. XL3615 ~ SOUTHWEST REGION ~ US 101 ~ MP 33.80 TO MP 33.90 ~ MIDDLE NEMAH RIVER BRIDGE NO. 101/31 REPLACEMENT (NEW STRUCTURE)



Bridge #	101/31	Bridge Name	Middle Nemah River	Structure ID	0018464A
Contract #	8344	Region	SW	Project Engineer	Lori Figone
Contractor	SB Structures	Concrete Supplier	Bayview Redi Mix, Inc	Performance Deck Concrete?	YES
Bridge Description	Single-Span, 5-WF50G Girders (127' bridge length), 2-Lanes (36' wide roadway)				

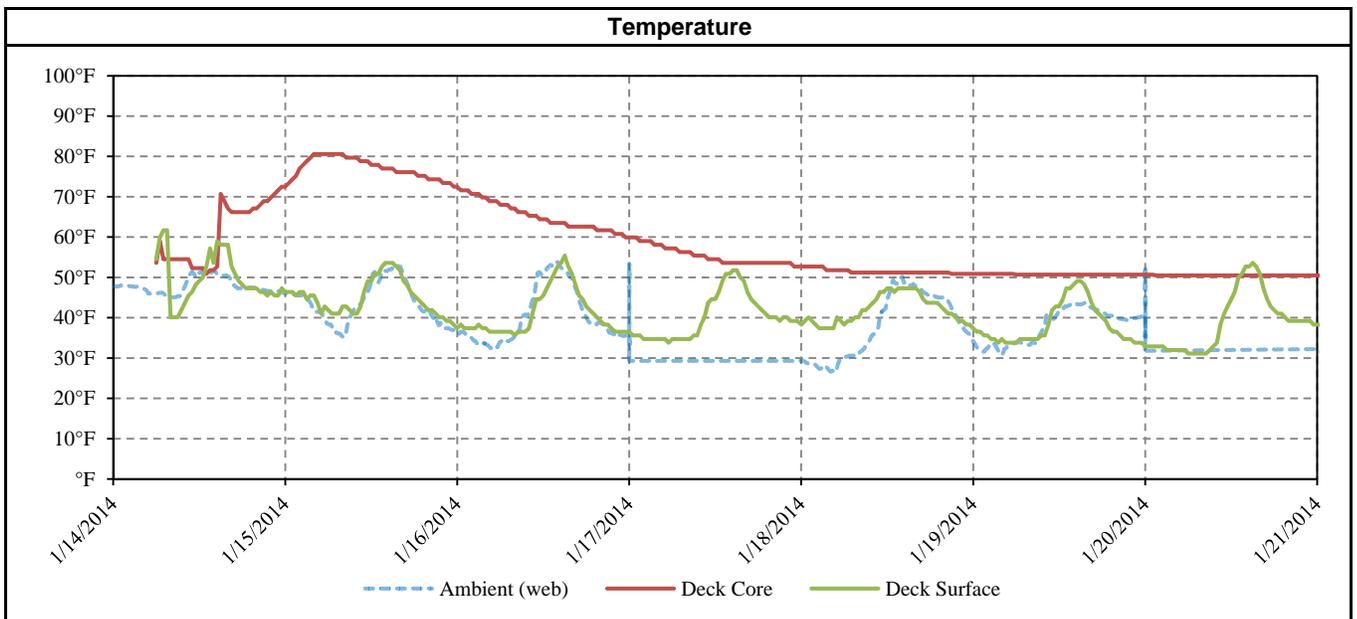
Mix Design (WSDOT Form 350-040)			
Water (max) =		230 lbs/cy	w/c = 0.38 max
Cementitious Materials	Lbs/cy	Source	Type, Class or Grade
cement	460	Ashgrove	Type I-II
fly ash	150	Lafarge	Type F
slag			
latex			
microsilica			
Concrete Admixtures	oz/cy	Manufacturer	Product
air entrainment	1-15	BASF	Micro Air
water reducer			
HR water reduce	20-30	BASF	Glenium 7500
set retarder			
shrink. reducer	120-140	BASF	Masterlife

Concrete Test Results		
compressive strength @ 28 days	5,691	psi
modulus of elasticity	4,012,122	psi
permeability @ 56 days	1,677	coulombs
mix design density	150.1	lb/cf



Aggregate					
	Comp. 1	Comp. 2	Comp. 3	Comp. 4	Comp. 5
WSDOT Pit #	PS-X-130	PS-X-130	PS-X-130		
Grading	#67	#4	Class II		
% Total	42.0%	20.0%	38.0%		
Lbs/cy	1350	650	1213		
ASR Mitigation	None Required				

Notes
Same Mix Design as:
* Bridge 6/8
* Bridge 101/44
* Bridge 105/4
* Bridge 105/3
if swell of concrete specimen is included, total change in length at 28 days drying is 240 microstrain (0.0060% + 0.0180%)



Concrete Mix Design

Contractor SB Structures		Submitted By Bayview Redi-Mix, Inc		Date 07/22/2013
Concrete Supplier Bayview Redi Mix, Inc			Plant Location Raymond 041, Aberdeen 011	
Contract Number 8344		Contract Name Middle Nemah River Bridge Replacement Bridge		

This mix is to be used in the following Bid Item No(s): _____

Concrete Class: **(check one only)**

- 3000
 4000
 4000^a
 4000^P
 4000W
 Concrete Overlay
 Cement Concrete Pavement^d
 Other Shrinkage

Remarks: _____

Mix Design No. WSDT4DS130 Plant No. 041, 011

Cementitious Materials	Source	Type, Class or Grade	Sp. Gr.	Lbs/cy
Cement	Ashgrove, Seattle, WA	Type I-II	3.15	460
Fly Ash ^a	Lafarge, Centralia, WA	Type F	2.58	150
GGBFS (Slag)				
Latex				
Microsilica				

Concrete Admixtures	Manufacturer	Product	Type	Est. Range (oz/cy)
Air Entrainment	BASF Cleveland, OH	Micro Air		1-15
Water Reducer				
High-Range Water Reducer	BASF Cleveland, OH	Glenium 7500	F	20-30
Set Retarder				
Other Shrinkage	BASF Cleveland, OH	Masterlife		120-140

Water (Maximum) 230 lbs/cy Is any of the water Recycled or Reclaimed? Yes^e No

Water Cementitious Ratio (Maximum) .38 Mix Design Density 150.1 lbs/cf^d

Design Performance	1	2	3	4	5	Average ^f
28 Day Compressive Strength (cylinders) psi	5,775	5,766	5,623	5,561	5,730	5,691
14 Day Flexural ^d Strength (beams) psi						

Agency Use Only (Check appropriate Box)

- This Mix Design **MEETS CONTRACT SPECIFICATIONS** and may be used on the bid items noted above
 This Mix Design **DOES NOT MEET CONTRACT SPECIFICATIONS** and is being returned for corrections

Reviewed By: Imi Tijme
PE Signature

7/24/13
Date

Aggregate Information

Concrete Aggregates	Component 1	Component 2	Component 3	Component 4	Component 5	Combined Gradation
WSDOT Pit No.	PS-X-130	PS-X130	PS-X-130			
WSDOT ASR 14-day Results (%) ^b	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No	
Grading ^c	AAASHTO #67	AAASHTO #4	Class II			
Percent of Total Aggregate	42	20	38			100%
Specific Gravity	2.825	2.825	2.747			
Lbs/cy (ssd)	1350	650	1213			

Percent Passing

	Component 1	Component 2	Component 3	Component 4	Component 5	Combined
2 inch	100	100	100			100
1-1/2 inch	100	100	100			100
1 inch	100	52	100			90
3/4 inch	93	1	100			77
1/2 inch	58	1	100			63
3/8 inch	30	1	100			51
No. 4	7	0	99			41
No. 8	0	0	78			30
No. 16	0	0	58			22
No. 30	0	0	35			13
No. 50	0	0	14			5
No. 100	0	0	3			1
No. 200	0	.1	1.1			0.5

90.4
77.3
62.6
50.8
40.6
29.6
✓
13.3
5.3
1.1
0.4

Fineness Modulus: 3.14 (Required for Class 2 Sand)

ASR Mitigation Method Proposed^b: Not Required for this Source

Notes:

- ^a Required for Class 4000D and 4000P mixes.
- ^b Alkali Silica Reactivity Mitigation is required for sources with expansions over 0.20% - Incidate method for ASR mitigation. For expansion of 0.21% - 0.45%, acceptable mitigation can be the use of low alkali cement or 25% type F fly ash. Any other proposed mitigation method or for pits with greater than 0.45% expansion, proof of mitigating measure, either ASTM C1260 / AASHTO T303 test results must be attached. If ASTM C 1293 testing has been submitted indicating 1-year expansion of 0.04% or less, mitigation is not required.
- ^c AASHTO No. 467, 57, 67, 7, 8; WSDOT Class 1, Class 2; or combined gradation. See Standard Specification 9-03.1.
- ^d Required for Cement Concrete Pavements.
- ^e Attach test results indicating conformance to Standard Specification 9-25.1.
- ^f Actual Average Strength as determined from testing or estimated from ACI 211.

SD-K. Slater #101
Received 7/23/13
(Page 3 of 4)



Lafarge North America Concrete Lab
5400 W Marginal Way SW
Seattle, WA. 98106

Report To: Bayview Ready Mix
Attention: Quality Control Personnel

Date: July 9, 2013

Subject: Bayview Ready Mix 4000D - WSDOT Performance Deck Mix

Project: 4000D Mix of Bayview Ready Mix

Date Sampled: June 11, 2013 by Bayview on site

Strength c-31

6x12 - 180000 lbs = 6370 psi

6x12 - 184560 lbs = 6530 psi

Modulus of Elasticity c-469

4,012,122 psi

SP 7.88
ASTM C 469

A handwritten signature in black ink that reads 'Rob Shogren'.

Rob Shogren, P.E, Ph.D.
Technical Service Engineer
Lafarge North America



Ash Grove Technical Center

11011 Cody Street, Suite 125

Overland Park, Kan. 66210

December 12, 2012

Report Number: R18439

Work Order Number: WO-120489

SUBJECT

On October 4, 2012 a request for technical service was issued on behalf of Marvin Prince of Bay View Redi-Mix in Aberdeen, Washington. Mr. Dave Burg requested that the Technical Center batch concrete with the submitted aggregates and cast specimens for rapid chloride penetrability (AASHTO T 277) and drying shrinkage (ASTM C 157) testing.

SAMPLE IDENTIFICATION

<u>Sample No.</u>	<u>Sample Description</u>	<u>Date Received</u>
S-120817	(1) 3.5-gal. bucket of Lafarge Centralia Plant Class F fly ash, Centralia, Oregon	03/26/2012
S-121541	(3) 5-gal. buckets of Ash Grove Cement Company Seattle Plant T I/II Portland Cement	07/17/2012
S-122202	(2) 5-gallon buckets of Bay View Redi-Mix fine aggregate, Pit # X-130	10/02/2012
S-122203	(2) 5-gallon buckets of Bay View Redi-Mix coarse aggregate, 3/4-in. to No. 4, Pit # X-130	10/02/2012
S-122204	(2) 5-gallon buckets of Bay View Redi-Mix coarse aggregate, 1.5-in. to 3/4-in., Pit # X-130	10/02/2012
S-122225	(1) 3.5-gal. bucket of BASF Master Life SRA 20	10/04/2012
S-122302	(1) 3.5-gal. bucket of BASF Glenium 7500	10/11/2012
S-122303	(1) 3.5-gal. bucket of BASF Micro-Air	10/11/2012

SUMMARY

Concrete mix proportions were provided by Mr. Burg. A concrete trial batch was performed with the submitted materials, and specimens were cast in accordance with applicable standards. Four cylinder specimens were cast for determination of chloride penetrability per AASHTO T 277 testing and three prisms were cast for determination of drying shrinkage per ASTM C 157.

One of the cylinder specimens was subjected to accelerated curing conditions and tested at 28-days of age. The remaining three specimens were cured in standard conditions. Of those, one was tested at 28-days of age and two were tested at 56-days of age.

The concrete drying shrinkage prisms were wet-cured for four weeks prior to their exposure to drying conditions (23°C and 50% RH). Their length change was monitored for an additional four weeks while stored in drying conditions.

TEST RESULTS

ASTM C 192 - Standard Practice for Making and Curing Concrete Test Specimens in the Laboratory

Concrete Mixture Proportions

4,000 PSI Mix

Trial Mix Results Calculated to 1yd³

D-101112-01

<u>S-Number</u>	<u>Description</u>	<u>SpG</u>	<u>Mass, lbs</u>	<u>Vol. Cuft</u>
S-121541	AG Seattle Type I/II	3.15	462	2.35
S-120817	Lafarge Centralia Class F	2.58	151	0.94
S-122202	Pit X-130 Fine Agg.	2.75	1,217	7.09
S-122204	Pit X-130 1.5 to 3/4 Agg.	2.83	652	3.69
S-122203	Pit X-130 3/4 to No. 4 Agg.	2.83	1,357	7.68
---	Overland Park Municipal	1.00	233	3.73
-	Air	-	5.6%	1.51
Totals:			4,072	27.00

Admixtures

<u>S-Number</u>	<u>Description</u>	<u>Dosage, oz/cwt</u>
S-122303	BASF Micro-Air	1.0
S-122302	BASF Glenium 7500	4.0
S-122225	BASF Master Life SRA 20	21.0

Plastic Properties

D-101112-01

Slump, in:	6.75
Unit Weight, lbs/cuft:	150.8
Air Content (Calculated), %:	5.6
w/cm ratio:	0.38
Concrete Temperature, F:	74°

AASHTO T 277 - Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration
Accelerated Cure

<u>Sample No.</u>	<u>Diameter, in.</u>	<u>Charge Passed, C</u>	<u>Corrected Charge, C</u>	<u>Qualitative Equivalent</u>	<u>Age, days</u>
D-101112-01	4.00	739	650	Very Low	28

AASHTO T 277 - Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration
Standard Cure

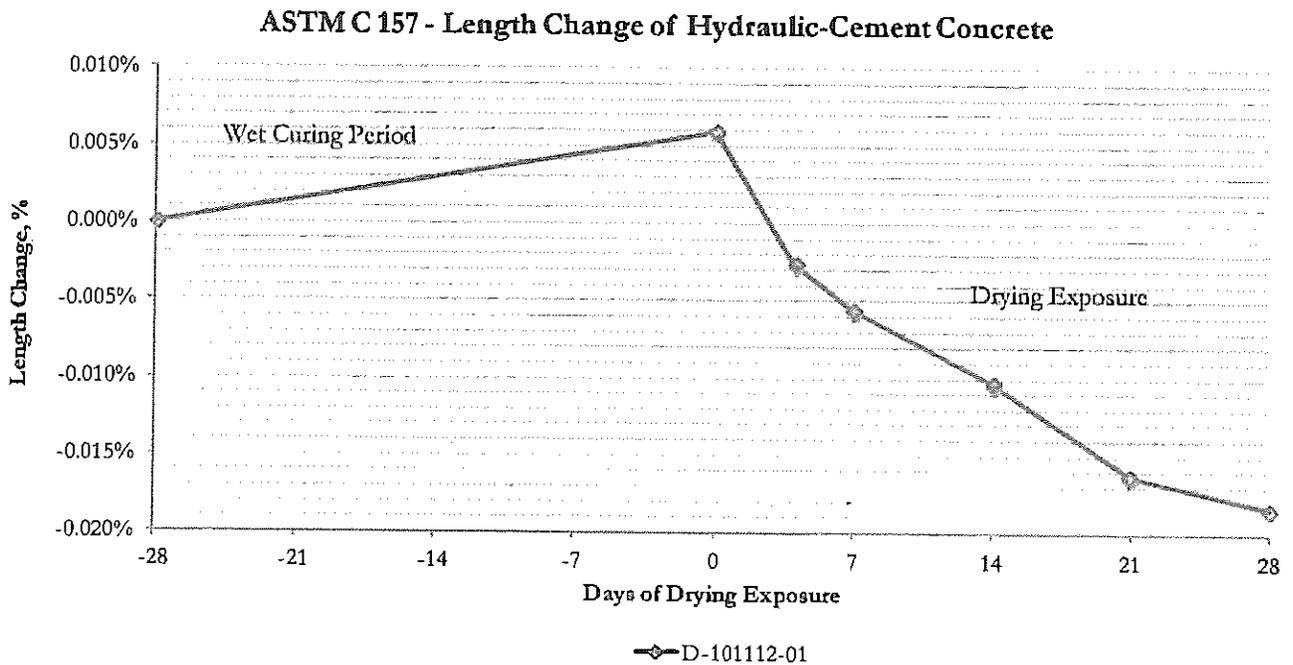
<u>Sample No.</u>	<u>Diameter, in.</u>	<u>Charge Passed, C</u>	<u>Corrected Charge, C</u>	<u>Qualitative Equivalent</u>	<u>Age, days</u>
D-101112-01	4.00	1,902	1,672	Low	28
	4.00	1,750	1,538	Low	56
	4.00	1,908	1,677	Low	56

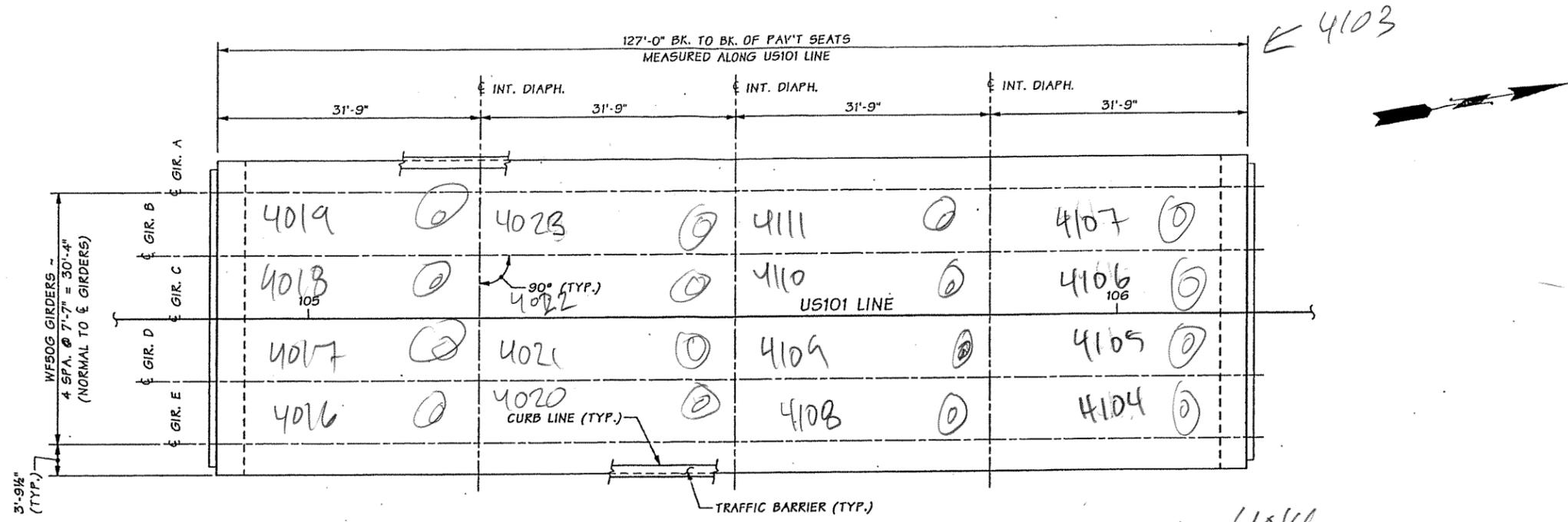
S. P. 88
Permeability < 2000 C
in 56 days

ASTM C 157 Standard Test Method for Length Change of Hardened Hydraulic-Cement Mortar and Concrete

Material:	Concrete
Number of Specimens per Mixture:	4
Size of Specimens, in:	Length: 10.0
	Width: 4.0
	Height: 4.0
Method of Consolidation:	4
Period of Moist Curing:	28-days
Drying Exposure Conditions:	23°C, 50% RH

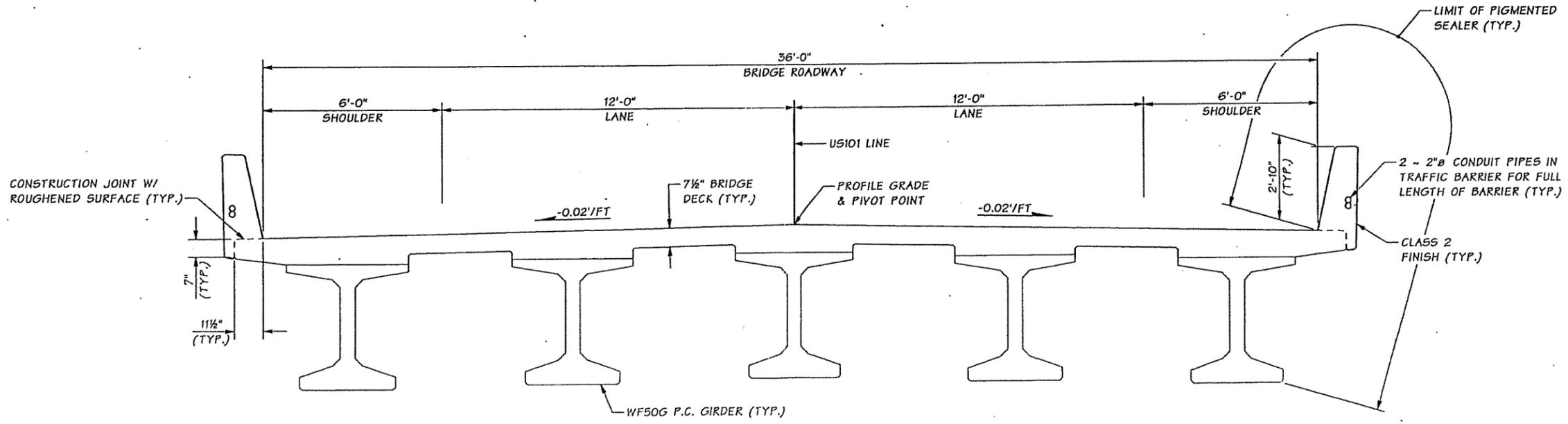
Length Change	Reading	D-101112-01
	Initial	0.000%
	0-days dry	0.006%
	4-days dry	-0.003%
	7-days dry	-0.006%
	14-days dry	-0.010%
	21-days dry	-0.016%
	28-days dry	-0.018%





FRAMING PLAN

BEARING OF ALL PIERS AND DIAPHRAGMS ARE: N 79°32'36" W



TYPICAL SECTION

SHOWN NEAR MID-SPAN

SR US101 FILE NO. 7061 SHEET BR10

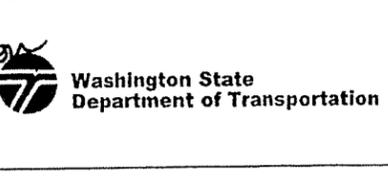
Bridge Design Engr.	Khaleghi, B	M:\Y-Team\US 101 - NEMAH RIVER REPL>window files\FRAMING PLAN.wnd
Supervisor	Anderson, MW	
Designed By	Sargent, S	08/11
Checked By	Martin, J	05/12
Detailed By	Nettle, J	08/11
Bridge Projects Engr.		
Prelim. Plan By		
Architect/Specialist		
DATE	REVISION	BY APPD

REGION	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
10	WASH.			
JOB NUMBER				
12X303				

BRIDGE AND STRUCTURES OFFICE

Professional Engineer Seal: WILLIAM SCOTT SARGENT, WASHINGTON STATE, LICENSE NO. 4290, 5/15/12

Professional Engineer Seal: WILLIAM ANDERSON, WASHINGTON STATE, LICENSE NO. 4290, 5/15/12



US 101
MIDDLE NEMAH RIVER BR.
REPLACE BRIDGE
MIDDLE NEMAH R BR. NO. 101/31 REPL.
FRAMING PLAN

BRIDGE SHEET NO.	BR10
SHEET OF SHEETS	59 OF 83

For May 15 08:40:22 2012



Bridge #	101/31	Bridge Name	Middle Nemah River			Structure ID	0018464A	
Contract #	8344	Region	SW	Project Engineer	Lori Figone	Performance Deck Concrete?	YES	
Contractor	SB Structures		Concrete Supplier	Bayview Redi Mix, Inc		Deck Placement	1/14/2014	
Bridge Description	Single-Span, 5-WF50G Girders (127' bridge length), 2-Lanes (36' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	0%
Min. =	0%
Max. =	0%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	31.75	7.58	0	16	0%
1	1	B	C	31.75	7.58	0	16	0%
1	1	C	D	31.75	7.58	0	16	0%
1	1	D	E	31.75	7.58	0	16	0%
1	2	A	B	31.75	7.58	0	16	0%
1	2	B	C	31.75	7.58	0	16	0%
1	2	C	D	31.75	7.58	0	16	0%
1	2	D	E	31.75	7.58	0	16	0%
1	3	A	B	31.75	7.58	0	16	0%
1	3	B	C	31.75	7.58	0	16	0%
1	3	C	D	31.75	7.58	0	16	0%
1	3	D	E	31.75	7.58	0	16	0%
1	4	A	B	31.75	7.58	0	16	0%
1	4	B	C	31.75	7.58	0	16	0%
1	4	C	D	31.75	7.58	0	16	0%
1	4	D	E	31.75	7.58	0	16	0%



	PIER 1		PIER 2	
GIR. A				
GIR. B	0%	0%	0%	0%
GIR. C	0%	0%	0%	0%
GIR. D	0%	0%	0%	0%
GIR. E	0%	0%	0%	0%

CRACKING INTENSITY ~ BRIDGE 101/31

100% = CRACK EVERY 2 FT.

LESS CRACKING

MORE CRACKING

BRIDGE NUMBER	101/31
BRIDGE NAME	MIDDLE NEMAH RIVER
INSPECTION DATE	5/7/2015
DECK CONCRETE	PERFORMANCE BASED

APPENDIX B

TWO-SPAN PRESTRESSED GIRDER BRIDGES

BRIDGE 16/7S-E (SOUTH SPRAGUE RAMP)

BRIDGE 195/117 (CHENEY-SPOKANE ROAD OVER US 195)

BRIDGE 395/442W (US 395 OVER US 2)

BRIDGE 16/3W (SR 16 OVER HOV)

BRIDGE 2/8.5N-W (BICKFORD AVE OVER US 2)

BRIDGE 395/441N-E (N-E RAMP OVER N-N RAMP)

BRIDGE 16/7S-E (SOUTH SPRAGUE RAMP)

Bridge #	16/7S-E	Bridge Name	South Sprague Ramp	Structure ID	0017594E		
Contract #	7594	Region	OR	Project Engineer	Jon Deffenbacher	Performance Deck Concrete?	No
Contractor	Guy F. Atkinson Const.	Concrete Supplier		Deck Placement	≈ 2010		
Bridge Description	2-Span (154' / 148'), 4-WF83G Girders (320' bridge length), 1-Lane (27' wide roadway)						

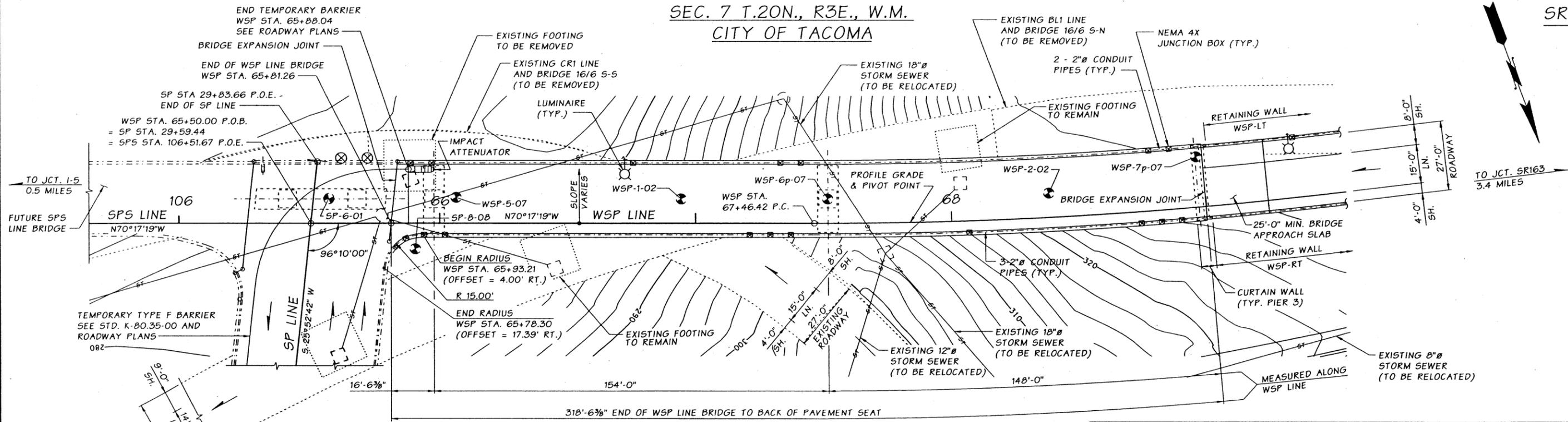


CONTENTS

1. Layout Plan Sheet
2. Field Notes
3. Crack Summary
4. Crack Intensity Diagram

SEC. 7 T.20N., R3E., W.M.
CITY OF TACOMA

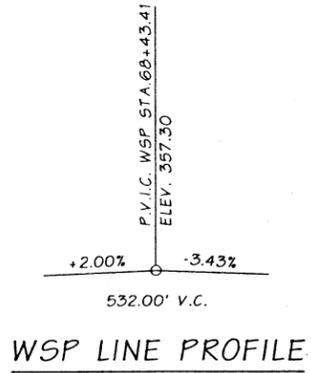
SR16



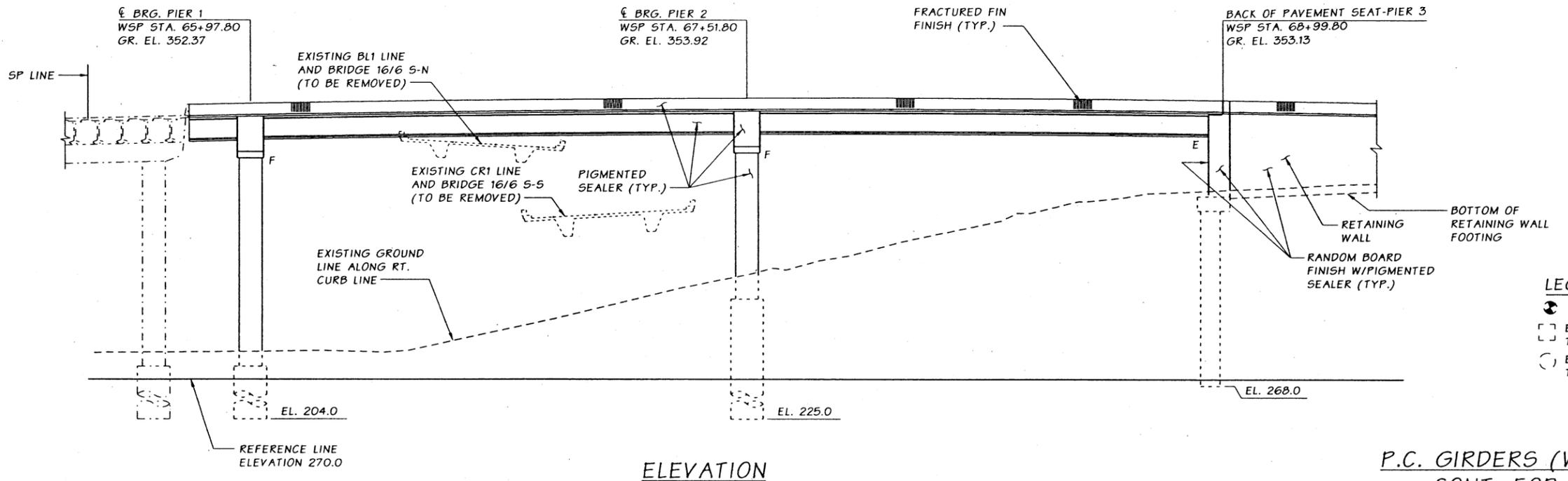
PLAN

BEARINGS OF ALL PIERS AND BACK OF PAVEMENT SEAT ARE NORMAL TO WSP LINE BACK OF PAVEMENT SEAT AT PIER 3 IS PARALLEL TO $\frac{1}{2}$ OF BEARING

WSP LINE CURVE DATA					
P.I. STATION	DELTA	RADIUS	TANGENT	LENGTH	BK. TANGENT BRG.
STA. 69+96.16	16°14'36" LT.	1750.00'	249.74'	496.13'	N 70°17'19" W



WSP LINE PROFILE



ELEVATION

GRADE ELEVATIONS SHOWN ARE FINISH GRADES AT TOP OF ROADWAY SLAB ON WSP LINE AND ARE EQUAL TO PROFILE GRADE.

- LEGEND**
- TEST BORING
 - EXISTING CATCH BASIN TO BE RELOCATED
 - EXISTING MANHOLE TO BE RELOCATED

P.C. GIRDERS (WF83G)
CONT. FOR L.L.
LOADING: HL-93

DATUM
N.A.V.D. OF 1988

Bridge Design Engr	C:\AAwork\PW.Work\Herzstein\ems02802\p3460.SH.BG.WSP.PP01.dgn		
Supervisor			
Designed By	E. HERZSTEIN	REGION NO.	10
Checked By	W. ELKEY	STATE	WASH
Detailed By	O. ROTH	FED. AID PROJ. NO.	
Bridge Proj. Engr		SHEET NO.	
Prelim Plan By		TOTAL SHEETS	
Architect/Specialist		DATE	
		REVISION	
		BY	APPD

PARSONS

BRIDGE AND STRUCTURES OFFICE



1-5 / SR16
WB NALLEY VALLEY I/C
WSP LINE BRIDGE

LAYOUT

BRIDGE SHEET NO. K-2
SHEET 754 OF 1360 SHEETS

6/16/2008 3:24:28 PM SR 16 JOB NO 7344 SHEET 2 OF 40



Bridge #	16/7S-E	Bridge Name	South Sprague Ramp			Structure ID	0017594E	
Contract #	7594	Region	OR	Project Engineer	Jon Deffenbacher	Performance Deck Concrete?	No	
Contractor	Guy F. Atkinson Const.		Concrete Supplier				Deck Placement	≈ 2010
Bridge Description	2-Span (154' / 148'), 4-WF83G Girders (320' bridge length), 1-Lane (27' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

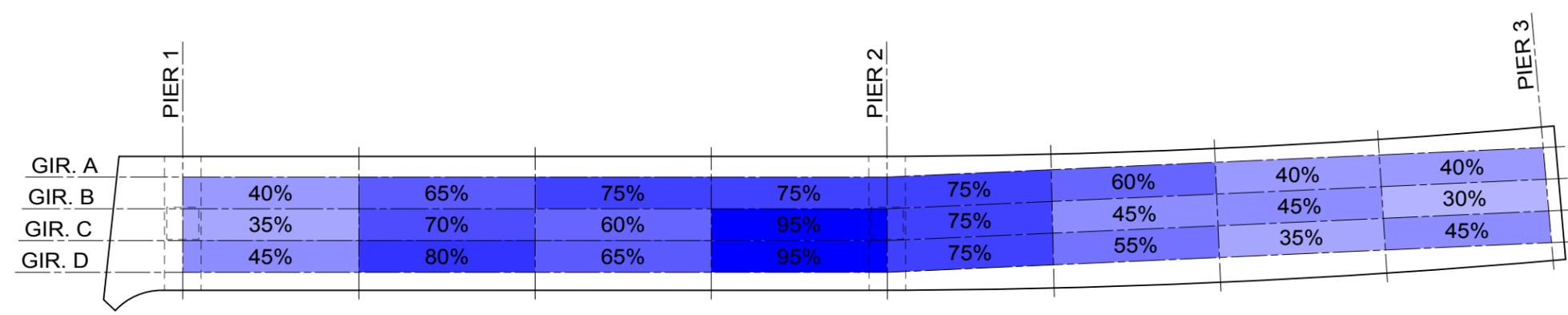
N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	59%
Min. =	30%
Max. =	95%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	38.50	6.92	8	19	40%
1	1	B	C	38.50	6.92	7	19	35%
1	1	C	D	38.50	6.92	9	19	45%
1	2	A	B	38.50	6.92	12	19	65%
1	2	B	C	38.50	6.92	13	19	70%
1	2	C	D	38.50	6.92	15	19	80%
1	3	A	B	38.50	6.92	14	19	75%
1	3	B	C	38.50	6.92	11	19	60%
1	3	C	D	38.50	6.92	12	19	65%
1	4	A	B	38.50	6.92	14	19	75%
1	4	B	C	38.50	6.92	18	19	95%
1	4	C	D	38.50	6.92	18	19	95%
2	1	A	B	37.00	6.92	14	19	75%
2	1	B	C	37.00	6.92	14	19	75%
2	1	C	D	37.00	6.92	14	19	75%
2	2	A	B	37.00	6.92	11	19	60%
2	2	B	C	37.00	6.92	9	19	45%
2	2	C	D	37.00	6.92	10	19	55%
2	3	A	B	37.00	6.92	8	19	40%
2	3	B	C	37.00	6.92	9	19	45%
2	3	C	D	37.00	6.92	7	19	35%
2	4	A	B	37.00	6.92	8	19	40%
2	4	B	C	37.00	6.92	6	19	30%
2	4	C	D	37.00	6.92	9	19	45%



CRACKING INTENSITY ~ BRIDGE 16/7S-E

100% = CRACK EVERY 2 FT.

LESS CRACKING

MORE CRACKING

BRIDGE NUMBER	16/7S-E
BRIDGE NAME	SOUTH SPRAGUE RAMP
INSPECTION DATE	5/29/2015
DECK CONCRETE	TRADITIONAL

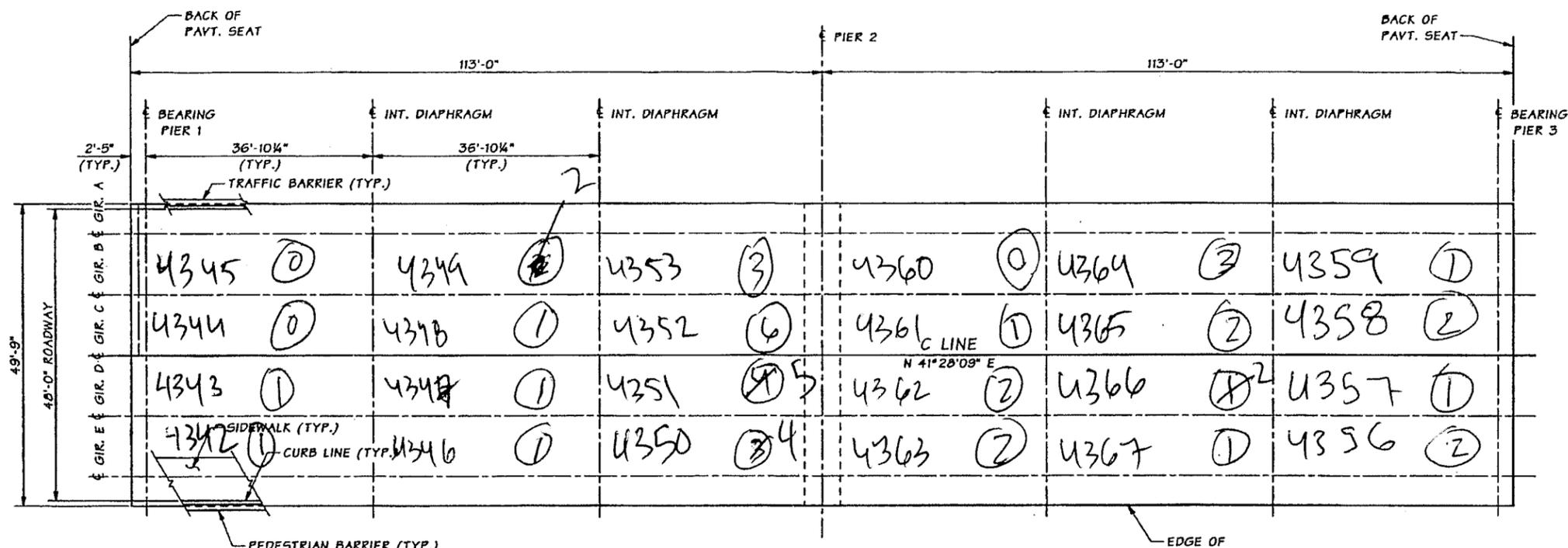
BRIDGE 195/117 (CHENEY-SPOKANE ROAD OVER US 195)

Bridge #	195/117	Bridge Name	Cheney-Spokane Road over US 195		Structure ID	0018378A	
Contract #	8378	Region	ER	Project Engineer	Chad Simonson	Performance Deck Concrete?	Yes
Contractor	Selland Construction		Concrete Supplier		Deck Placement	≈ 2014	
Bridge Description	2-Span (113' / 113"), 5-WF50G Girders (226' Bridge Length), 2-Lanes (48' wide roadway)						



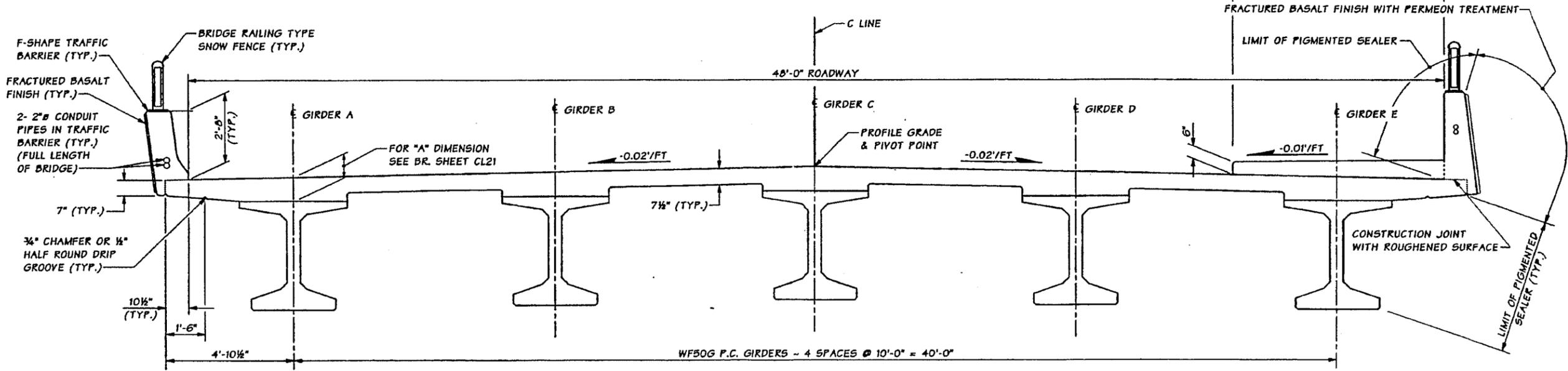
CONTENTS

1. Layout Plan Sheet
2. Mix Design Summary
3. Field Notes
4. Crack Summary
5. Crack Intensity Diagram



FRAMING PLAN

BEARING OF ALL GIRDERS IS N 41°28'09" E.
BEARING OF ALL PIERS AND DIAPHRAGMS IS NORMAL TO C-LINE.



TYPICAL SECTION

SR 195 FILE NO. 7006 SHEET CL21

Bridge Design Engr.	khaleghi, B	M:\Z-Team\US195 - Cheney Spokane I-C\US195 OXING\window files\FRAMING PLAN.WND			
Supervisor	zeldenrust, RP	REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.
Designed By	Hatch, H 05/10	10	WASH.		
Checked By	Gallagher, P 12/10	JOB NUMBER			
Detailed By	Lencke, DR 02/11				
Bridge Projects Engr.					
Prelim. Plan By					
Architect/Specialist		DATE	REVISION	BY	APPD.



BRIDGE AND STRUCTURES OFFICE



US 195 CHENEY-SPOKANE ROAD INTERCHANGE		BRIDGE SHEET NO.
C-LINE OVER US 195 BRIDGE		CL21
FRAMING PLAN AND TYPICAL SECTION		SHEET 155 OF 198

Wed Sep 12 07:50:28 2012



Bridge #	195/117	Bridge Name	Cheney-Spokane Road over US 195		Structure ID	0018378A	
Contract #	8378	Region	ER	Project Engineer	Chad Simonson	Performance Deck Concrete?	Yes
Contractor	Selland Construction		Concrete Supplier			Deck Placement	10/23/2013
Bridge Description	2-Span (113' / 113"), 5-WF50G Girders (226' Bridge Length), 2-Lanes (48' wide roadway)						

L = length between diaphragms (or length of "bay")

S = girder spacing

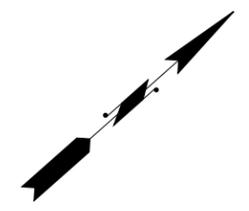
N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	10%
Min. =	0%
Max. =	35%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	36.85	10.00	0	18	0%
1	1	B	C	36.85	10.00	0	18	0%
1	1	C	D	36.85	10.00	1	18	5%
1	1	D	E	36.85	10.00	1	18	5%
1	2	A	B	36.85	10.00	2	18	10%
1	2	B	C	36.85	10.00	1	18	5%
1	2	C	D	36.85	10.00	1	18	5%
1	2	D	E	36.85	10.00	1	18	5%
1	3	A	B	36.85	10.00	3	18	15%
1	3	B	C	36.85	10.00	6	18	35%
1	3	C	D	36.85	10.00	5	18	30%
1	3	D	E	36.85	10.00	4	18	20%
2	1	A	B	36.85	10.00	0	18	0%
2	1	B	C	36.85	10.00	1	18	5%
2	1	C	D	36.85	10.00	2	18	10%
2	1	D	E	36.85	10.00	2	18	10%
2	2	A	B	36.85	10.00	3	18	15%
2	2	B	C	36.85	10.00	2	18	10%
2	2	C	D	36.85	10.00	2	18	10%
2	2	D	E	36.85	10.00	1	18	5%
2	3	A	B	36.85	10.00	1	18	5%
2	3	B	C	36.85	10.00	2	18	10%
2	3	C	D	36.85	10.00	1	18	5%
2	3	D	E	36.85	10.00	2	18	10%



	PIER 1			PIER 2			PIER 3
GIR. A							
GIR. B	0%	10%	15%	0%	15%	5%	
GIR. C	0%	5%	35%	5%	10%	10%	
GIR. D	5%	5%	30%	10%	10%	5%	
GIR. E	5%	5%	20%	10%	5%	10%	

CRACKING INTENSITY ~ BRIDGE 195/117

100% = CRACK EVERY 2 FT.



BRIDGE NUMBER	195/117
BRIDGE NAME	CHENEY-SPOKANE ROAD OVER US 195
INSPECTION DATE	5/20/2015
DECK CONCRETE	PERFORMANCE BASED

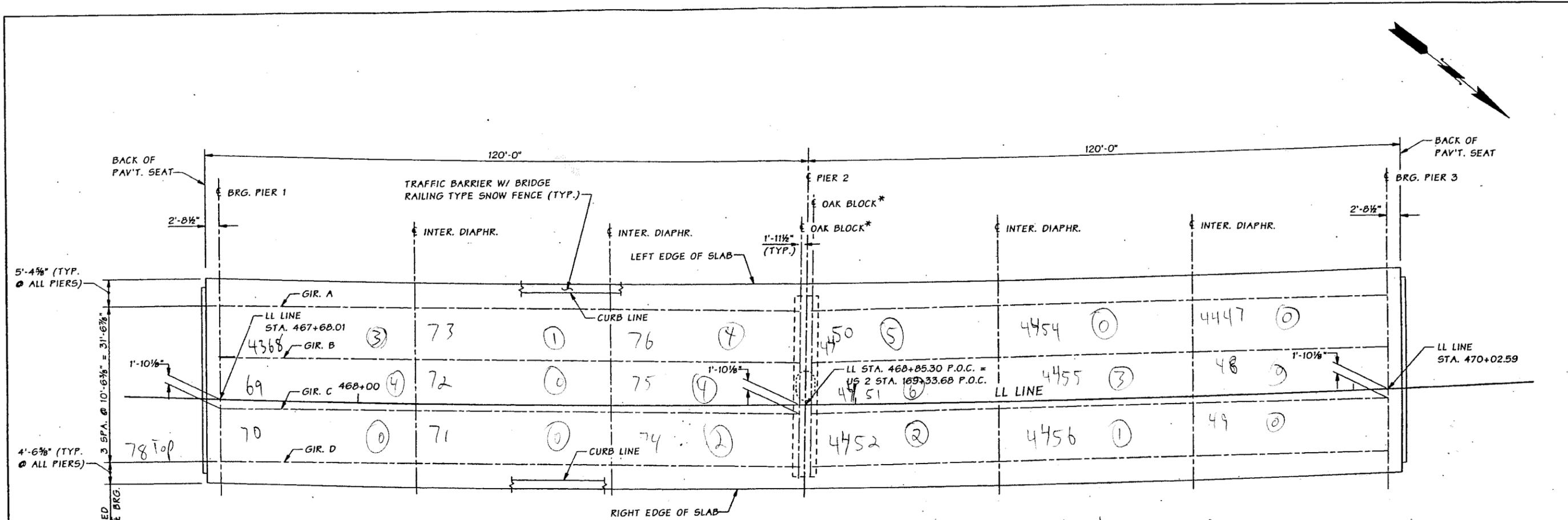
BRIDGE 395/442W (US 395 OVER US 2)

Bridge #	395/442W	Bridge Name	US 395 SB over US 2		Structure ID	0017610E	
Contract #	7610	Region	ER	Project Engineer	Bob Hilmes	Performance Deck Concrete?	No
Contractor	Graham Construction		Concrete Supplier		Deck Placement		≈ 2011
Bridge Description	2-Span (120' / 120"), 4-WF58G Girders (240' bridge length), 2-Lanes (38' wide roadway)						



CONTENTS

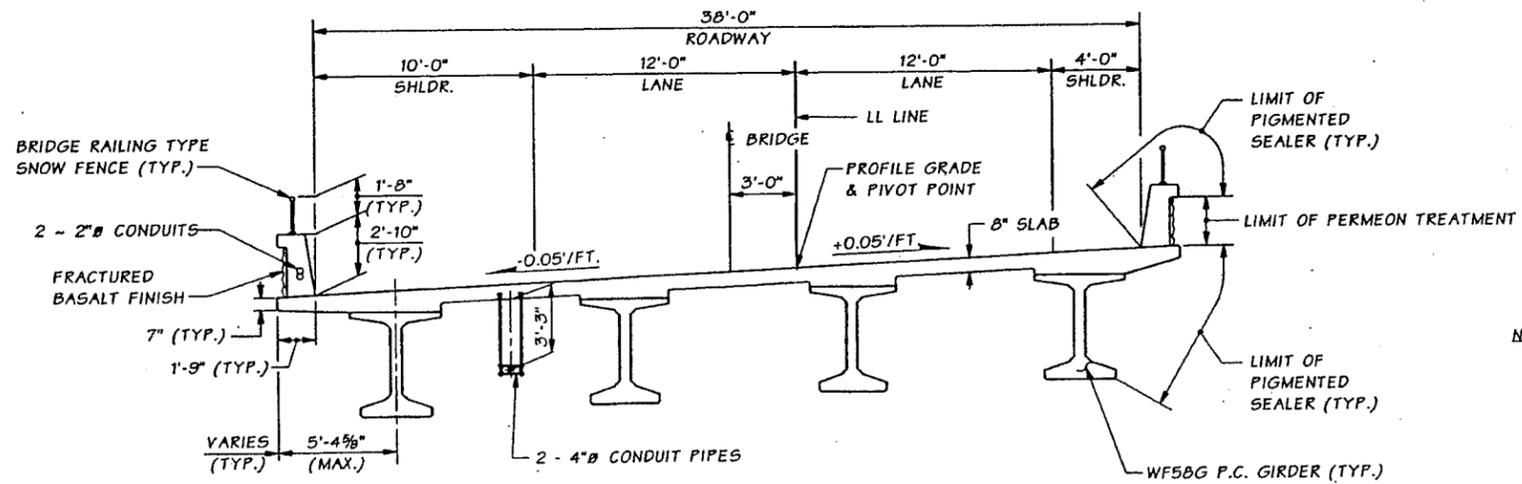
1. Layout Plan Sheet
2. Field Notes
3. Crack Summary
4. Crack Intensity Diagram



FRAMING PLAN

* SEE "OAK BLOCK DETAIL" BR. SHT. SB10

*Red bridge over farm
has asphalt settlement @ pavement seat.*



NOTE: LIMIT OF PIGMENTED SEALER ON CROSSBEAM COLUMN AND END PIERS TO 1'-0" BELOW FINISHED GROUND LINE.

JOB NO. SHEET SB22

Bridge Design Engr.	khaleghi, B	M:\2-Team\NSC - SR 395\PS&E\SB US2 XING\window files\FRAMING PLAN.WND			
Supervisor	Zeldenrust, RP	REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.
Designed By	Zhang, H 05/07	10	WASH.		TOTAL SHEETS
Checked By	Gallagher, P 07/08	JOB NUMBER			
Detalled By	Andreotti, L 07/08	082011			
Bridge Projects Engr.		DATE	REVISION	BY	APPD
Prefer. Plan By					
Architect/Specialet					



BRIDGE AND STRUCTURES OFFICE



US 395 NSC - US 2 LOWERING	BRIDGE SHEET NO. SB22
US 395 SB OVER US 2 BRIDGE	SHEET 298 OF 548 SHEETS
FRAMING PLAN	



Bridge #	395/442W	Bridge Name	US 395 SB over US 2			Structure ID	0017610E	
Contract #	7610	Region	ER	Project Engineer	Bob Hilmes	Performance Deck Concrete?	No	
Contractor	Graham Construction		Concrete Supplier				Deck Placement	≈ 2011
Bridge Description	2-Span (120' / 120"), 4-WF58G Girders (240' bridge length), 2-Lanes (38' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

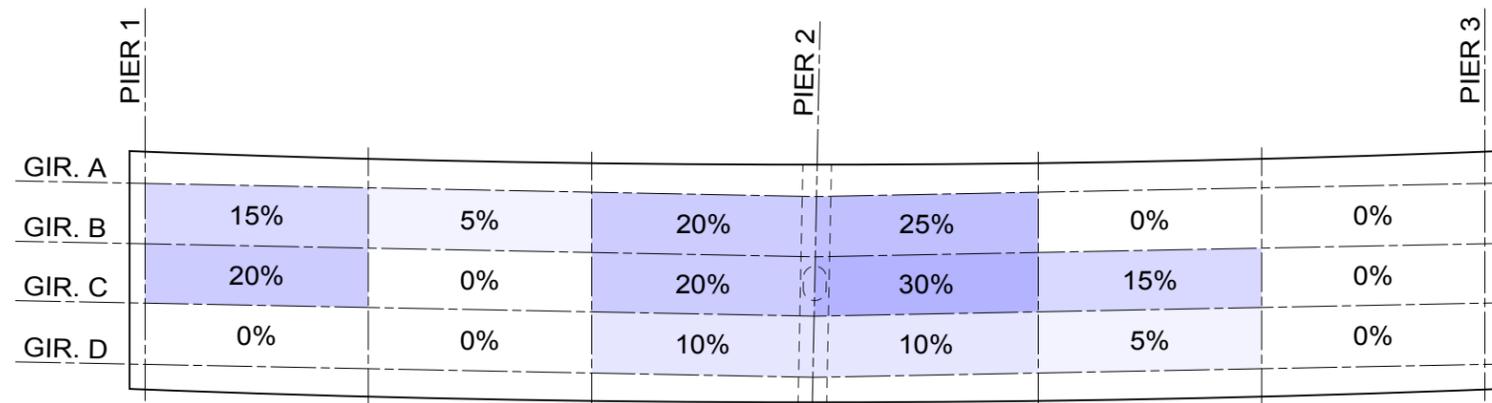
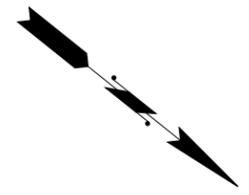
N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	10%
Min. =	0%
Max. =	30%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	40.00	10.53	3	20	15%
1	1	B	C	40.00	10.53	4	20	20%
1	1	C	D	40.00	10.53	0	20	0%
1	2	A	B	40.00	10.53	1	20	5%
1	2	B	C	40.00	10.53	0	20	0%
1	2	C	D	40.00	10.53	0	20	0%
1	3	A	B	40.00	10.53	4	20	20%
1	3	B	C	40.00	10.53	4	20	20%
1	3	C	D	40.00	10.53	2	20	10%
2	1	A	B	40.00	10.53	5	20	25%
2	1	B	C	40.00	10.53	6	20	30%
2	1	C	D	40.00	10.53	2	20	10%
2	2	A	B	40.00	10.53	0	20	0%
2	2	B	C	40.00	10.53	3	20	15%
2	2	C	D	40.00	10.53	1	20	5%
2	3	A	B	40.00	10.53	0	20	0%
2	3	B	C	40.00	10.53	0	20	0%
2	3	C	D	40.00	10.53	0	20	0%



CRACKING INTENSITY ~ BRIDGE 395/442W

100% = CRACK EVERY 2 FT.

LESS CRACKING

MORE CRACKING



BRIDGE NUMBER	395/442W
BRIDGE NAME	US 395 OVER US 2
INSPECTION DATE	5/21/2015
DECK CONCRETE	TRADITIONAL

BRIDGE 16/3W (SR 16 OVER HOV)

Bridge #	16/3W	Bridge Name	SR 16 Over HOV			Structure ID	0018189A
Contract #	8189	Region	OR	Project Engineer	Neal Uhlmeyer	Performance Deck Concrete?	Yes
Contractor	Mowat Construction		Concrete Supplier	Holroyd		Deck Placement	≈ 2014
Bridge Description	2-Span (141' / 141'), 6-WF59G Girders (282' bridge length), 3-Lanes (55' wide roadway)						



CONTENTS

1. Layout Plan Sheet
2. Mix Design Summary
3. Concrete Mix Design Form
4. Concrete Test Results
5. Field Notes
6. Crack Summary
7. Crack Intensity Diagram

SEC. 7, T. 20N., R. 3E., W.M.

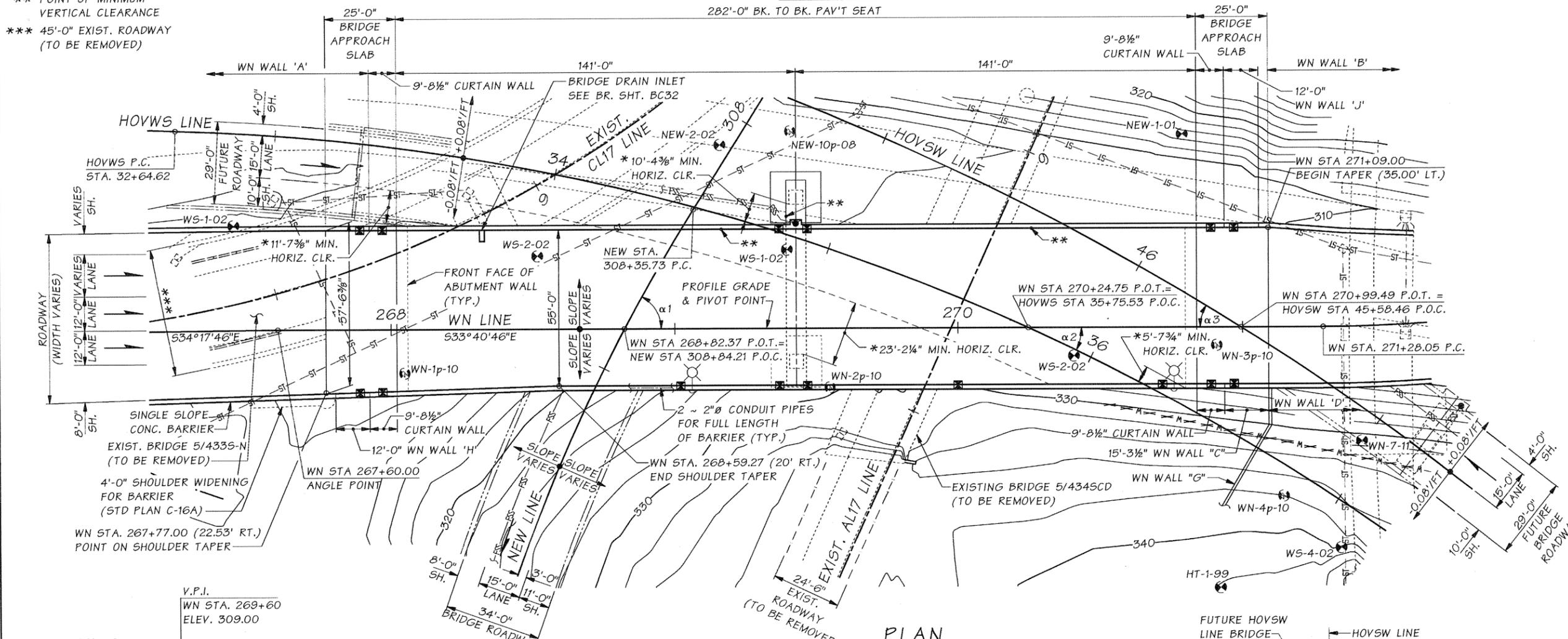
CITY OF TACOMA

282'-0" BK. TO BK. PAV'T SEAT

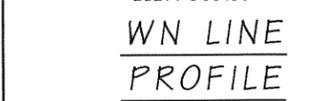
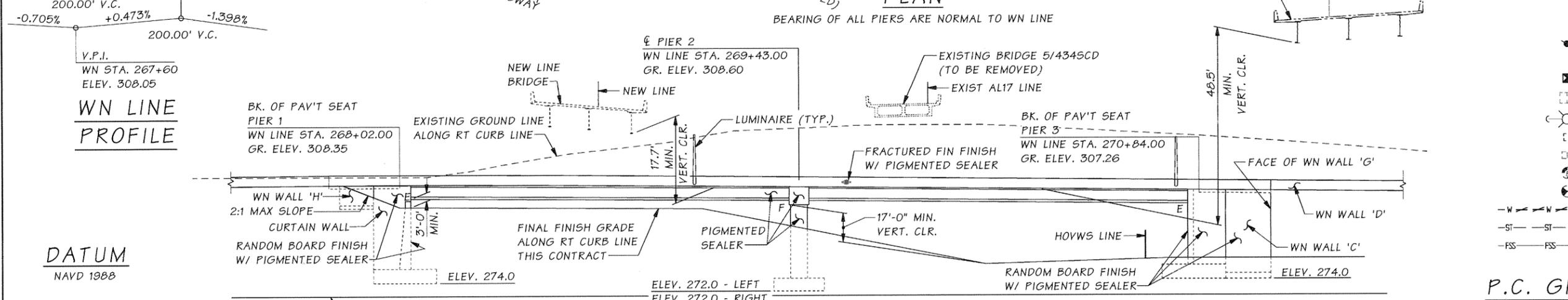
SR16



- * MIN. HORIZ. CLR. IS MEASURED TO EDGE OF TRAVELED LANE
- ** POINT OF MINIMUM VERTICAL CLEARANCE
- *** 45'-0" EXIST. ROADWAY (TO BE REMOVED)



INTERSECTING ANGLES
 $\alpha 1 = 62^{\circ}05'19''$
 $\alpha 2 = 24^{\circ}37'33''$
 $\alpha 3 = 32^{\circ}27'32''$



DATUM
NAVD 1988

ELEVATION

NOTE: GRADE ELEVATIONS SHOWN ARE FINISH GRADES AT TOP OF BRIDGE DECK ON WN LINE AND ARE EQUAL TO PROFILE GRADE. SEE STD. PLAN A-50.10-00 FOR EMBANKMENT DETAILS AT BRIDGE ENDS.

- LEGEND:
- FIRE SUPPRESSION SYSTEM HOSE OUTLET INCLUDING SIGN
 - JUNCTION BOX
 - EXIST. UNDERDECK LUMINAIRE
 - LUMINAIRE
 - EXIST. CATCH BASIN
 - EXIST. GRATE INLET
 - PIEZOMETER
 - TEST HOLE
 - DEACTIVE WATER LINE
 - EXIST. STORM SEWER LINE
 - FIRE SUPPRESSION SYSTEM

P.C. GIRDERS (WF58G)
 CONT. FOR L.L.
 LOADING: HL-93

Bridge Design Engr.	Khalighi, B	M:\Z-Team\SR16 EB NV\WN Line\window files\TEMP Layout_Add1.WND			
Supervisor	Zeldenrust, RP	REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.
Designed By	Young/Brown 01/10	10	WASH.		TOTAL SHEETS
Checked By	Brown/Rochon 04/11	JOB NUMBER			
Detailed By	Plesha, GM 02/11	09C519			
Bridge Projects Engr.	Lewis, RA				
Prelim. Plan By	CH2MHILL	7/14/11	REPLACEMENT SHEET	PG	RP2
Architect/Specialist	Kinderman, P	DATE	REVISION	BY	APPD

BRIDGE AND STRUCTURES OFFICE



I-5 / SR 16
 EB NALLEY VALLEY - HOV
 WN LINE BRIDGE
 LAYOUT

BRIDGE SHEET NO.
 BC2
 SHEET
 772
 OF
 1341
 SHEETS

SR 16 FILE NO. 2583 SHEET BC2

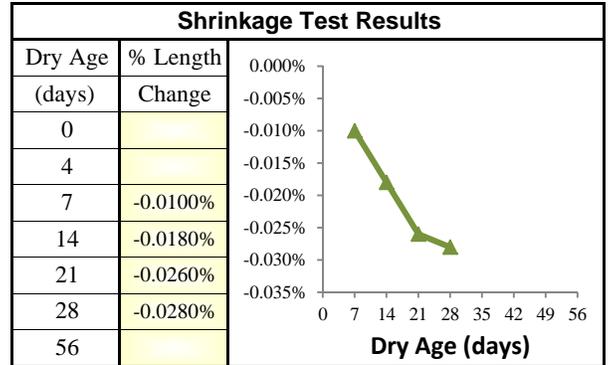
C.S. 270103 ~ PROJ. NO. XL3477 ~ OLYMPIC REGION ~ I-5 & SR16 INTERCHANGE ~ EASTBOUND NALLEY VALLEY ~ WN LINE BRIDGE



Bridge #	16/3W	Bridge Name	SR 16 Over HOV	Structure ID	0018189A
Contract #	8189	Region	OR	Project Engineer	Neal Uhlmeier
Contractor	Mowat Construction	Concrete Supplier	Holroyd	Performance Deck Concrete?	Yes
Bridge Description	2-Span (141' / 141'), 6-WF59G Girders (282' bridge length), 3-Lanes (55' wide roadway)				

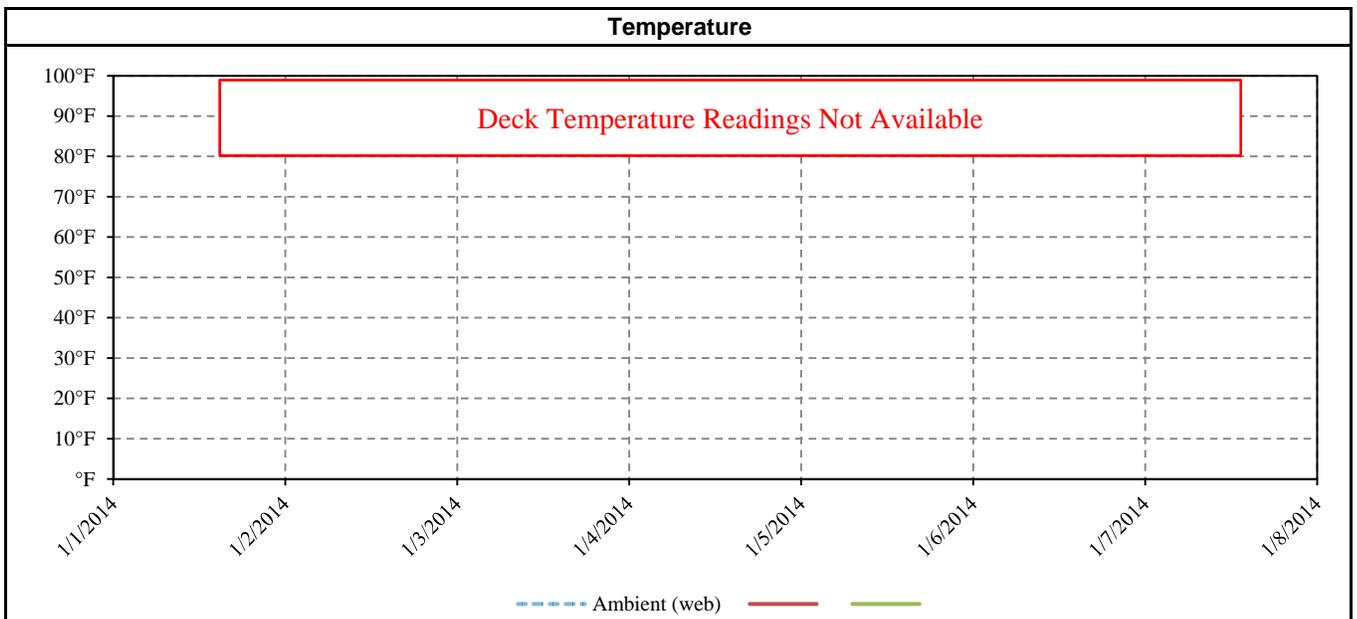
Mix Design (WSDOT Form 350-040)			
Water (max) =		217 lbs/cy	w/c = 0.38 max
Cementitious Materials	Lbs/cy	Source	Type, Class or Grade
cement	480	Lehigh Cement Co	Type I-II
fly ash	85	Lafarge	Type F
slag			
latex			
microsilica			
Concrete Admixtures	oz/cy	Manufacturer	Product
air entrainment	1 to 6	BASF	MB AE 90
water reducer			
HR water reduce	25 to 45	BASF	Glenium 3030 NS
set retarder			
shrink. reducer	30 to 45	BASF	Master Life SRA

Concrete Test Results		
compressive strength @ 28 days	6,458	psi
modulus of elasticity	5,461,245	psi
permeability @ 56 days	1,463	coulombs
mix design density	146.8	lb/cf



Aggregate					
	Comp. 1	Comp. 2	Comp. 3	Comp. 4	Comp. 5
WSDOT Pit #	J-9	J-9	J-9		
Grading	Class 1	#67	#4		
% Total	39.6%	45.1%	15.3%		
Lbs/cy	1265	1440	490		
ASR Mitigation	Use of low alkali cement				

Notes
This is the same mix that was used for Br. 5/434SCD



Contractor Mowat Construction Co		Submitted By Greg Smith	Date 12/15/2011
Concrete Supplier Holroyd Co., Inc.		Plant Location 3131 29th Ave Sw Tumwater, WA	
Contract Number 8189	Contract Name Nalley Valley Eastbound		

This mix is to be used in the following Bid Item No(s): 121, 122, 123, 124, 125, 126, 127

Concrete Class: (**check one only**)

- 3000
 4000
 4000^a
 4000P^a
 4000W
 Concrete Overlay
 Cement Concrete Pavement^d
 Other Shrinkage Reducer

Remarks: _____

Mix Design No. 6091FASD Plant No. Tacoma (3-4)

Cementitious Materials	Source	Type, Class or Grade	Sp. Gr.	Lbs/cy
Cement	Lehigh Cement Co	Type I-II	3.15	480
Fly Ash ^a	Lafarge	Type F	2.61	85
GGBFS (Slag)				
Latex				
Microsilica				

Concrete Admixtures	Manufacturer	Product	Type	Est. Range (oz/cy)
Air Entrainment	BASF Admixtures, Inc.	MB AE™ 90		1-6
Water Reducer				
High-Range Water Reducer	BASF Admixtures, Inc.	Glenium® 3030 NS	Type F	25-45
Set Retarder				
Other Shrinkage Reducer	BASF Admixtures, Inc.	MasterLIFE® SRA 20	Type S	30-45

Water (Maximum) 217 lbs/cy Is any of the water Recycled or Reclaimed? Yes^e No

Water Cementitious Ratio (Maximum) 0.38 Mix Design Density 146.8 lbs/cf^d

Design Performance	1	2	3	4	5	Average ^f
28 Day Compressive Strength (cylinders) psi	6,370	6,460	6,380	6,410	6,670	6,458
14 Day Flexural ^d Strength (beams) psi						

Agency Use Only (Check appropriate Box)

This Mix Design **MEETS CONTRACT SPECIFICATIONS** and may be used on the bid items noted above
 This Mix Design **DOES NOT MEET CONTRACT SPECIFICATIONS** and is being returned for corrections

Reviewed By: *Robert W. ...* 11 Apr 2013
 PE Signature Date

Aggregate Information

Concrete Aggregates	Component 1	Component 2	Component 3	Component 4	Component 5	Combined Gradation
WSDOT Pit No.	J-9	J-9	J-9			
WSDOT ASR 14-day Results (%) ^b	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No	
Grading ^c	Class 1	#67	#4			
Percent of Total Aggregate	39.6	45.1	15.3			100%
Specific Gravity	2.63	2.69	2.69			
Lbs/cy (ssd)	1265	1440	490			3195

Percent Passing

2 inch			100.0			100
1-1/2 inch			100.0			100
1 inch		100.0	52.0			93.4
3/4 inch		99.0	12.0			87.3
1/2 inch						66.9
3/8 inch	100.0	36.0	0			50.3
No. 4	97.0	3.0				39.4
No. 8	81.0	1.0				31.9
No. 16	62.0					23.2
No. 30	36.0					13.9
No. 50	13.0					5.2
No. 100	5.0					1.9
No. 200	2.5					1.0

Fineness Modulus: _____ (Required for Class 2 Sand)

ASR Mitigation Method Proposed^b: Pit No. J-9 has ASR of 0.43 and is mitigated by the use of low alkali cement.

Notes:

- a Required for Class 4000D and 4000P mixes.
- b Alkali Silica Reactivity Mitigation is required for sources with expansions over 0.20% - Incidate method for ASR mitigation. For expansion of 0.21% - 0.45%, acceptable mitigation can be the use of low alkali cement or 25% type F fly ash. Any other proposed mitigation method or for pits with greater than 0.45% expansion, proof of mitigating measure, either ASTM C1260 / AASHTO T303 test results must be attached. If ASTM C 1293 testing has been submitted indicating 1-year expansion of 0.04% or less, mitigation is not required.
- c AASHTO No. 467, 57, 67, 7, 8; WSDOT Class 1, Class 2; or combined gradation. See Standard Specification 9-03.1.
- d Required for Cement Concrete Pavements.
- e Attach test results indicating conformance to Standard Specification 9-25.1.
- f Actual Average Strength as determined from testing or estimated from ACI 211.



Modulus of Elasticity

5,461,245 psi

ASTM C-672 Scaling Resistance of Concrete Surfaces Exposed to Deicing Chemicals

Procedure: ASTM C-672

Result:	<u>Cycles</u>	<u>Rating</u>
	5	0
	10	0
	15	0
	25	0
	30	0

A handwritten signature in cursive script that reads 'Robt S. Shogren'.

Rob Shogren, P.E.
Technical Service Engineer
Lafarge North America



Lafarge North America Concrete Lab
5400 W Marginal Way SW
Seattle, WA. 98106

Report To: Holroyd
Attention: Quality Control Personnel

Date: September 30, 2011

Subject: Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration: ASTM C-1202

Tested Materials: Date Sampled: **August 2, 2011**
Mix Design: **Nalley Valley HPC**

Curing: ASTM C-1202 Standard Cure

Results:

Age
56 day

Coulombs
1463

*The ASTM C-1202 procedure was followed.

The test result is only valid if the aggregate(s) sample(s) is(are) representative of the current production and it is to be noted that Lafarge has no knowledge of the representatives of the sample received for testing. Also, material quality can vary with different locations in a quarry. It is recommended that testing be carried out on an annual basis or more frequently if a variation in stone quality is suspected.

Although the Lafarge North America Seattle Concrete Lab. applies state-of-the-art test methods, Lafarge North America. and its affiliates (Lafarge) can not guarantee the results shown above and shall assume no liability whatsoever for any errors in such results and for the consequence of such errors.

A handwritten signature in black ink that reads 'Robt S. Shogren'.

Rob Shogren, P.E.
Technical Service Engineer
Lafarge North America



Lafarge North America Concrete Lab
5400 W Marginal Way SW
Seattle, WA. 98106

Report To: Holroyd
Attention: Quality Control Personnel

Date: September 30, 2011

Subject: Length Change of Hardened Hydraulic-Cement Concrete Using Procedures of ASTM C-157

Tested Materials: Date Sampled: **August 2, 2011**
Source of Aggregates: Holroyd

Mix Design: WSDOT HPC

Results: Slump: 4.5"
Temp: 64^F Specimen Size: 4"x4"x10"
Consolidation: Rodding
Initial Cure: Lime water submersion (28 day initial cure)

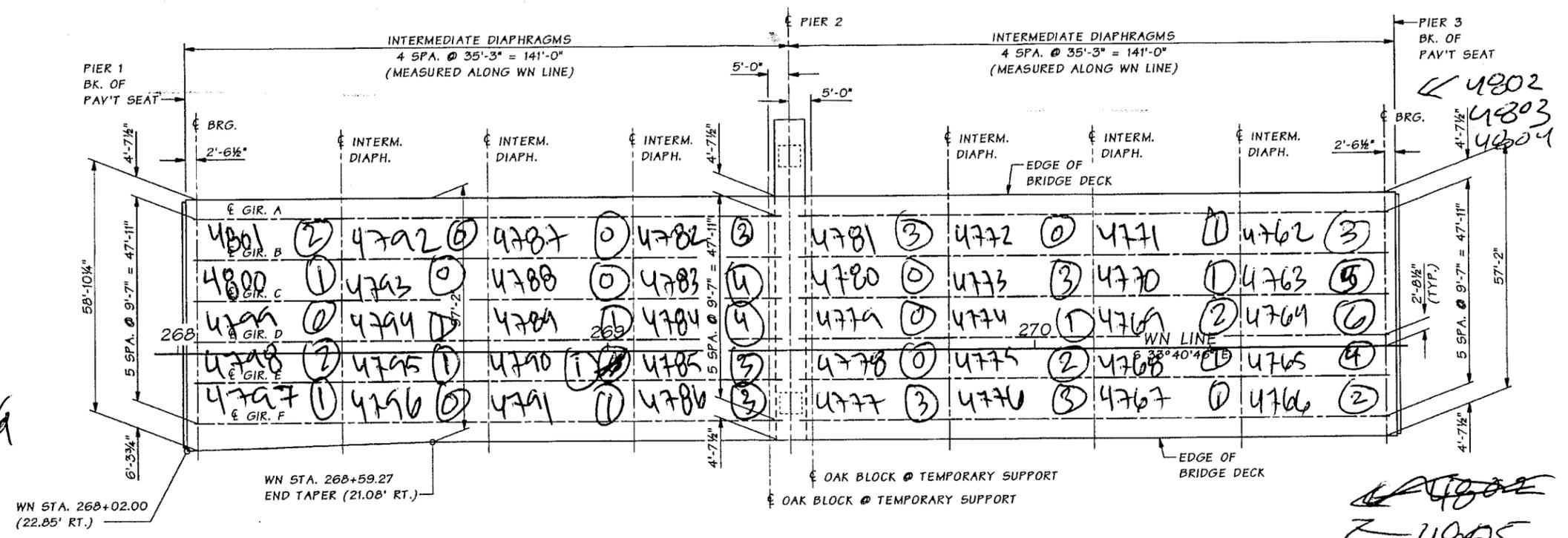
<u>Age (Days) After Initial Cure</u>	<u>Percent Length Change (Average of 3)</u>
7	0.010
14	0.018
21	0.026
28 (final)	0.028

*The ASTM C-157 procedure was followed.

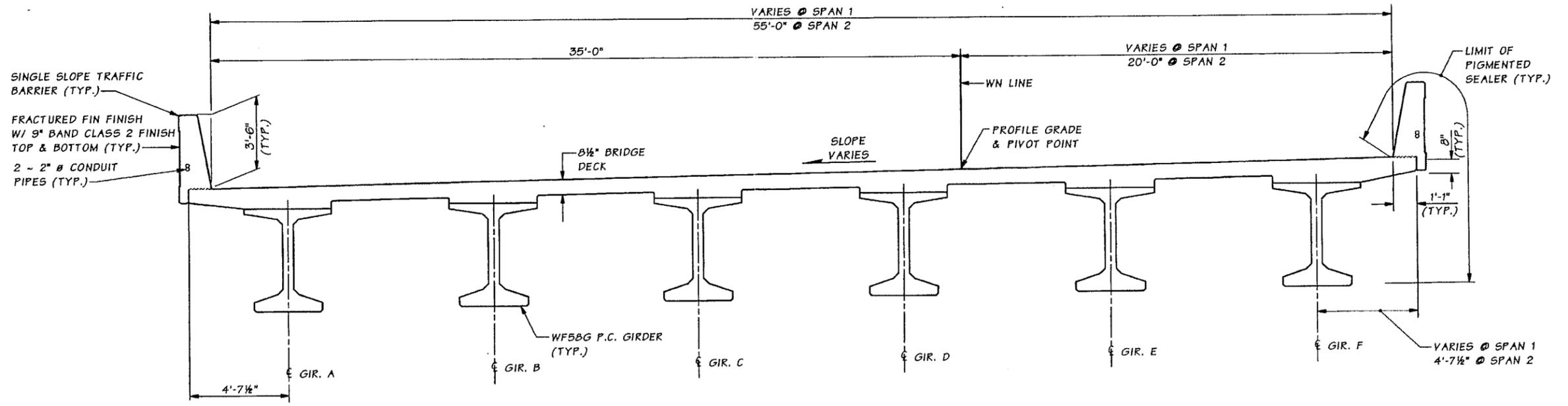
The test result is only valid if the aggregate(s) sample(s) is(are) representative of the current production and it is to be noted that Lafarge has no knowledge of the representatives of the sample received for testing. Also, material quality can vary with different locations in a quarry. It is recommended that testing be carried out on an annual basis or more frequently if a variation in stone quality is suspected.

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Rob Shogren, P.E.
Technical Service Engineer
Lafarge North America



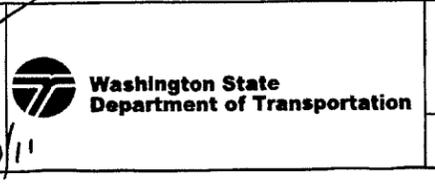
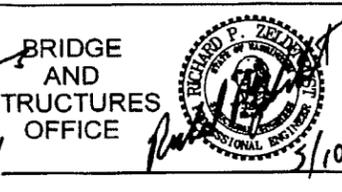
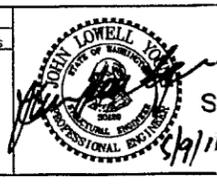
FRAMING PLAN



TYPICAL SECTION

SR 16 FILE NO. 2583 SHEET BC24

Bridge Design Engr.	Khaleghi, B	M:\Z-Team\SR16 EB NV\WN Line>window files\Framing Plan.WND
Supervisor	Zeldenrust, RP	
Designed By	Young, JL	02/10
Checked By	Brown, NS	04/11
Detailled By	Plesha, GM	03/10
Bridge Projects Engr.		
Prelim. Plan By		
Architect/Specialist		
DATE	REVISION	BY APPD



I-5 / SR 16 EB NALLEY VALLEY - HOV	
WN LINE BRIDGE	
FRAMING PLAN	
BRIDGE SHEET NO.	BC24
SHEET	794
OF	1341
SHEETS	

16/3W



Bridge #	16/3W	Bridge Name	SR 16 Over HOV			Structure ID	0018189A	
Contract #	8189	Region	OR	Project Engineer	Neal Uhlmeyer	Performance Deck Concrete?	Yes	
Contractor	Mowat Construction		Concrete Supplier	Holroyd		Deck Placement	≈ 2014	
Bridge Description	2-Span (141' / 141'), 6-WF59G Girders (282' bridge length), 3-Lanes (55' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

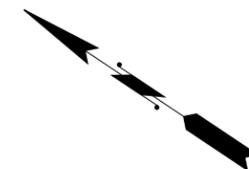
N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr} / N_{100} (rounded to the nearest 5%)

Avg. =	9%
Min. =	0%
Max. =	35%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	35.25	9.58	2	18	10%
1	1	B	C	35.25	9.58	1	18	5%
1	1	C	D	35.25	9.58	0	18	0%
1	1	D	E	35.25	9.58	2	18	10%
1	1	E	F	35.25	9.58	1	18	5%
1	2	A	B	35.25	9.58	0	18	0%
1	2	B	C	35.25	9.58	0	18	0%
1	2	C	D	35.25	9.58	1	18	5%
1	2	D	E	35.25	9.58	1	18	5%
1	2	E	F	35.25	9.58	0	18	0%
1	3	A	B	35.25	9.58	0	18	0%
1	3	B	C	35.25	9.58	0	18	0%
1	3	C	D	35.25	9.58	1	18	5%
1	3	D	E	35.25	9.58	1	18	5%
1	3	E	F	35.25	9.58	1	18	5%
1	4	A	B	35.25	9.58	3	18	15%
1	4	B	C	35.25	9.58	4	18	20%
1	4	C	D	35.25	9.58	4	18	20%
1	4	D	E	35.25	9.58	3	18	15%
1	4	E	F	35.25	9.58	3	18	15%
2	1	A	B	35.25	9.58	3	18	15%
2	1	B	C	35.25	9.58	0	18	0%
2	1	C	D	35.25	9.58	0	18	0%
2	1	D	E	35.25	9.58	0	18	0%
2	1	E	F	35.25	9.58	3	18	15%
2	2	A	B	35.25	9.58	0	18	0%
2	2	B	C	35.25	9.58	3	18	15%
2	2	C	D	35.25	9.58	1	18	5%
2	2	D	E	35.25	9.58	2	18	10%
2	2	E	F	35.25	9.58	3	18	15%
2	3	A	B	35.25	9.58	1	18	5%
2	3	B	C	35.25	9.58	1	18	5%
2	3	C	D	35.25	9.58	2	18	10%
2	3	D	E	35.25	9.58	1	18	5%
2	3	E	F	35.25	9.58	1	18	5%
2	4	A	B	35.25	9.58	3	18	15%
2	4	B	C	35.25	9.58	5	18	30%
2	4	C	D	35.25	9.58	6	18	35%
2	4	D	E	35.25	9.58	4	18	20%
2	4	E	F	35.25	9.58	2	18	10%



	PIER 1				PIER 2				PIER 3
GIR. A									
GIR. B	10%	0%	0%	15%	15%	0%	5%	15%	
GIR. C	5%	0%	0%	20%	0%	15%	5%	30%	
GIR. D	0%	5%	5%	20%	0%	5%	10%	35%	
GIR. E	10%	5%	5%	15%	0%	10%	5%	20%	
GIR. F	5%	0%	5%	15%	15%	15%	5%	10%	

CRACKING INTENSITY ~ BRIDGE 16/3W

100% = CRACK EVERY 2 FT.

LESS CRACKING

MORE CRACKING

BRIDGE NUMBER	16/3W
BRIDGE NAME	SR 16 OVER HOV
INSPECTION DATE	5/29/2015
DECK CONCRETE	PERFORMANCE BASED

BRIDGE 2/8.5N-W (BICKFORD AVE OVER US 2)

Bridge #	2/8.5N-W	Bridge Name	N-W Ramp (Bickford Ave) over US 2		Structure ID	0018286A
Contract #	8286	Region	NW	Project Engineer	Mark Sawyer	Performance Deck Concrete? Yes
Contractor	Granite Construction		Concrete Supplier	Concrete Nor'West	Deck Placement	4/3/2013
Bridge Description	2-Span (145' / 145'), 4-WF66G Girders (290' bridge length), 1-Lane (32' wide roadway)					



CONTENTS

1. Layout Plan Sheet
2. Mix Design Summary
3. Concrete Mix Design Form
4. Concrete Test Results
5. Field Notes
6. Crack Summary
7. Crack Intensity Diagram



Concrete Mix Design

Contractor Granite Construction		Submitted By Concrete Nor'West		Date 11/29/2012
Concrete Supplier Concrete Nor'West		Plant Location 15415 84th St NE, Lake Stevens WA		
Contract Number 8206	Contract Name Bickford Ave & US 2 Improvements			

This mix is to be used in the following Bid Item No(s): _____ Class 4000D 68.18

Concrete Class: (check one only)

- 3000
 4000
 4000D^a
 4000P^a
 4000W
 Concrete Overlay
 Cement Concrete Pavement^d
 Other

Remarks: Class 4000D with high range water reducer and shrink reducing admixture. Needs to be less than 2000 coulombs at 56 days per AASHTO 277

Mix Design No. 15BICK1 REV 1 Plant No. Getchell

Cementitious Materials	Source	Type, Class or Grade	Sp. Gr.	Lbs/cy
Cement	Ash Grove - Seattle	Type I/II Low Alkali	3.15	480
Fly Ash ^a	Lafarge	Type F	2.60	90
GGBFS (Slag)				
Latex				
Microsilica	BASF	SF 100	2.20	10

Concrete Admixtures	Manufacturer	Product	Type	Est. Range (oz/cy)
Air Entrainment	BASF	AE-90		1-10
Water Reducer				
High-Range Water Reducer	BASF	Glenium 7500	F	23
Set Retarder				
Other	BASF	MasterLIFE SRA 20	SRA	64

Water (Maximum) 230 lbs/cy

Is any of the water Recycled or Reclaimed? Yes^e No

Water Cementitious Ratio (Maximum) .40

Mix Design Density 147.0 lbs/cf^d

Design Performance	1	2	3	4	5	Average ^f
28 Day Compressive Strength (cylinders) psi						SEE
14 Day Flexural ^d Strength (beams) psi						Attached

Agency Use Only (Check appropriate Box)

- This Mix Design MEETS CONTRACT SPECIFICATIONS and may be used on the bid items noted above
 This Mix Design DOES NOT MEET CONTRACT SPECIFICATIONS and is being returned for corrections

Reviewed By: _____

PE Signature

3/19/2013
Date

Mix Design No. 15BICK1 REV 1

Plant No. Getchell

Aggregate Information

Concrete Aggregates	Component 1	Component 2	Component 3	Component 4	Component 5	Combined Gradation
WSDOT Pit No.	D - 306	D - 306	D - 306			
WSDOT ASR 14-day Results (%) ^b	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No	
Grading ^c	# 57	Class 2 Sand	#8			
Percent of Total Aggregate	48.5	39	9.5			100%
Specific Gravity	2.71	2.67	2.69			
Lbs/cy (ssd)	1620	1238	300			

Percent Passing

Size	Component 1	Component 2	Component 3	Component 4	Component 5	Combined
2 inch	100					
1-1/2 inch	100					100
1 inch	98					
3/4 inch	69					84
1/2 inch	38		100			
3/8 inch	11	100	99			54.1
No. 4	1	98.9	27			41.8
No. 8	1	85.8	1			34.1
No. 16		63.4	0			24.7
No. 30		43.1				16.8
No. 50		21.3				8.3
No. 100		5				2
No. 200		.8				.3

Fineness Modulus: 2.83 (Required for Class 2 Sand)

ASR Mitigation Method Proposed^b: The use of low Alkali cement will mitigate the .44 ASR value at D - 306

Notes:

- a Required for Class 4000D and 4000P mixes.
- b Alkali Silica Reactivity Mitigation is required for sources with expansions over 0.20% - Incidate method for ASR mitigation. For expansion of 0.21% - 0.45%, acceptable mitigation can be the use of low alkali cement or 25% type F fly ash. Any other proposed mitigation method or for pits with greater than 0.45% expansion, proof of mitigating measure, either ASTM C1260 / AASHTO T303 test results must be attached. If ASTM C 1293 testing has been submitted indicating 1-year expansion of 0.04% or less, mitigation is not required.
- c AASHTO No. 467, 57, 67, 7, 8; WSDOT Class 1, Class 2; or combined gradation. See Standard Specification 9-03.1.
- d Required for Cement Concrete Pavements.
- e Attach test results indicating conformance to Standard Specification 9-25.1.
- f Actual Average Strength as determined from testing or estimated from ACI 211.



Ash Grove Technical Center

11011 Cody Street, Suite 125
Overland Park, Kan. 66210

January 3, 2013 – Preliminary Report
January 24, 2013 – Final Report

Report Number: R18459
Work Order Number: WO-120607

SUBJECT

On December 10, 2012 a request for technical service was issued on behalf of Dave Enders of Concrete Nor' West in Burlington, Washington. Mr. Dave Burg requested that the Technical Center conduct AASHTO T 277 testing on the submitted concrete cylinders at specified ages.

SAMPLE IDENTIFICATION

<u>Sample No.</u>	<u>Sample Description</u>	<u>Date Received</u>
S-122885	(4) 4 x 8 Concrete Cylinders, Cast 11-29-2012 Mix15 Bick1 (WSDOT 4000D)	12/05/2012

TEST RESULTS

AASHTO T 277 - Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration
Accelerated Cure

<u>Sample No.</u>	<u>Diameter, in.</u>	<u>Charge Passed, C</u>	<u>Corrected Charge, C</u>	<u>Qualitative Equivalent</u>	<u>Age, days</u>
S-122885	4.00	1422	1,250	Low	28

AASHTO T 277 - Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration
Standard Cure

<u>Sample No.</u>	<u>Diameter, in.</u>	<u>Charge Passed, C</u>	<u>Corrected Charge, C</u>	<u>Qualitative Equivalent</u>	<u>Age, days</u>
S-122885	4.00	2,882	2,533	Moderate	28
S-122885	4.00	1,762	1,548	Low	56
S-122885 *	4.00	---	---	---	56

* This sample's cell lost continuity midway through the test so the results are not reported.

Table 1. Chloride Ion Penetrability Based on Charge Passed (Excerpted from AASHTO T 277)

<u>Charge Passed (coulombs)</u>	<u>Chloride Ion Penetrability</u>
> 4,000	High
2,000 – 4,000	Moderate
1,000 – 2,000	Low
100 – 1,000	Very Low
< 100	Negligible

Materials Testing & Consulting, Inc.

Geotechnical Engineering • Special Inspection • Materials Testing • Environmental Consulting



AASHTO T-160, Length Change of Hardened Hydraulic-Cement Mortar and Concrete

Client: Concrete Nor'West
 Project: Q.C. - Getchell Pit
 Project #: 12B006-06

Mix Data

Supplier: <u>Concrete Nor'West</u>	Mix #: <u>15BICK1</u>
Date/Time Batched: <u>Nov 29, 12 8:55 AM</u>	Cement, lbs.: <u>490</u>
Date/Time Cast: <u>Nov 29, 12 10:35 AM</u>	Flyash, lbs.: <u>90</u>
Slump: <u>3.75"</u>	Water, gals.: <u>19.6</u>
Air Content: <u>6.50%</u>	Fine Agg., lbs.: <u>1241</u>
Concrete Temp: <u>58</u>	Coarse Agg., lbs.: <u>1605 (7/8")</u>
Ambient Temp: <u>63</u>	Coarse Agg., lbs.: <u>312 (3/8")</u>
W/C Ratio: <u>0.36</u>	Admixture, oz./cwt <u>21.3 (Glenium)</u>
Unit Weight: <u>NT</u>	Admixture, oz./cwt <u>1.0 (MBAE-90)</u>
Yield: _____	Admixture, oz./cwt <u>64.0 (BASF Masterlife SRA)</u>
Storage Method: <u>Air Storage</u>	Admixture, oz./cwt _____

Sample I.D. #	Reference Bar Reading	Sample Reading	Date & Time	Age of Concrete	Gauge Length	% Change In Length
B5927	0.1635	0.0899	Nov 30, 12 10:19 AM	24 Hours	10	
B5928	0.1635	0.0783	Nov 30, 12 10:19 AM		10	
B5929	0.1635	0.1117	Nov 30, 12 10:19 AM		10	
						Average: -0.0030 %
B5927	0.1636	0.0896	Dec 27, 12 9:31 AM	28 day initial wet cure	10	-0.0040 %
B5928	0.1636	0.0777	Dec 27, 12 9:31 AM		10	-0.0070 %
B5929	0.1636	0.1120	Dec 27, 12 9:31 AM		10	0.0020 %
						Average: -0.0030 %
B5927	0.1631	0.0875	Dec 31, 12 9:10 AM	4 day air cure	10	-0.0200 %
B5928	0.1631	0.0762	Dec 31, 12 9:10 AM		10	-0.0170 %
B5929	0.1631	0.1096	Dec 31, 12 9:10 AM		10	-0.0170 %
						Average: -0.0180 %
B5927	0.1650	0.0890	Jan 3, 13 9:19 AM	7 day air cure	10	-0.0240 %
B5928	0.1650	0.0777	Jan 3, 13 9:19 AM		10	-0.0210 %
B5929	0.1650	0.1111	Jan 3, 13 9:19 AM		10	-0.0210 %
						Average: -0.0220 %
B5927	0.1651	0.0885	Jan 10, 13 9:00 AM	14 day air cure	10	-0.0300 %
B5928	0.1651	0.0774	Jan 10, 13 9:00 AM		10	-0.0250 %
B5929	0.1651	0.1107	Jan 10, 13 9:00 AM		10	-0.0260 %
						Average: -0.0270 %
B5927	0.1653	0.0882	Jan 24, 13 2:45 PM	28 day air cure	10	-0.0350 %
B5928	0.1653	0.0771	Jan 24, 13 2:45 PM		10	-0.0300 %
B5929	0.1653	0.1105	Jan 24, 13 2:45 PM		10	-0.0300 %
						Average: -0.0317 %

Remarks: 10 lbs. of Silica Fume added to mix. Average 28 compressive strength for this concrete was 6630 psi.

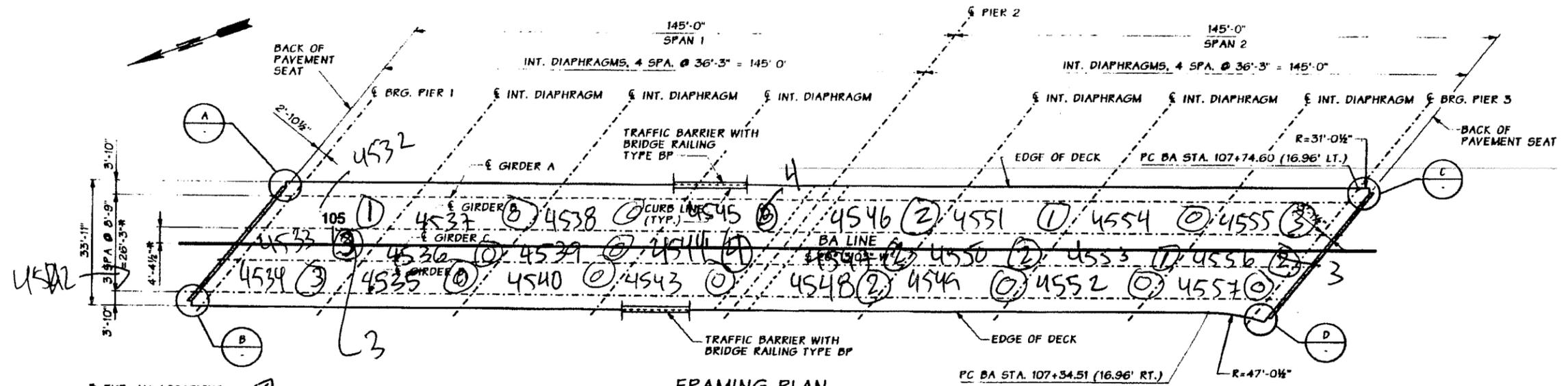
Reviewed By: C. Z

Corporate ~ 777 Chrysler Drive • Burlington, WA 98233 • Phone (360) 755-1990 • Fax (360) 755-1980
 NW Region ~ 2126 East Bakerview Rd., Suite #101 • Bellingham, WA 98226 • Phone (360) 647-6061 • Fax (360) 647-8111
 SW Region ~ 2118 Black Lake Blvd. • Olympia, WA 98512 • Phone (360) 534-9777 • Fax (360) 534-9779

Visit our website: www.mtc-inc.net

9/24/11 AM

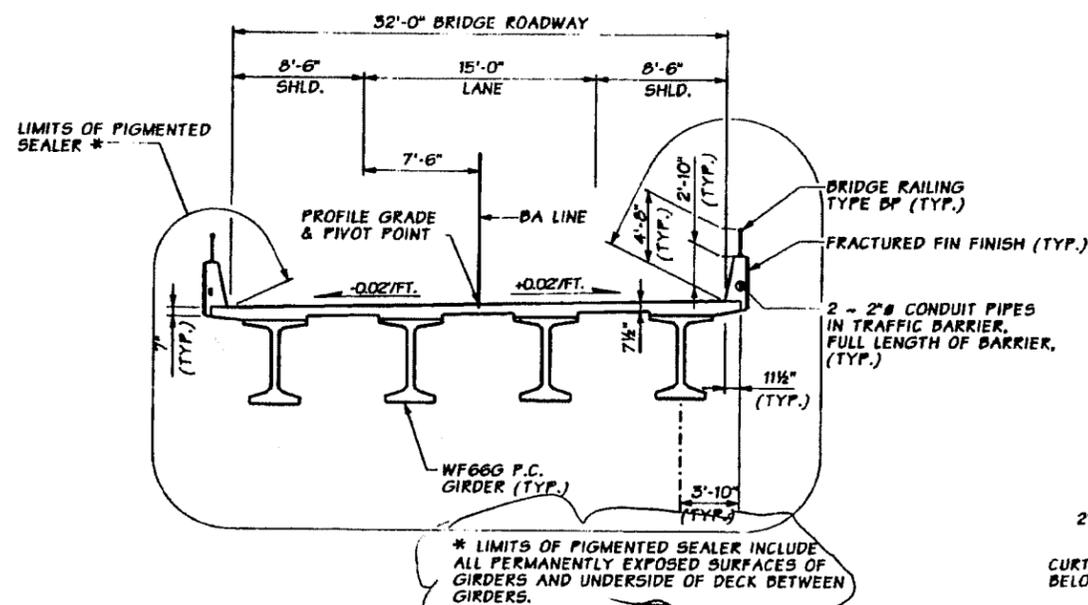
3/21/2012



FRAMING PLAN

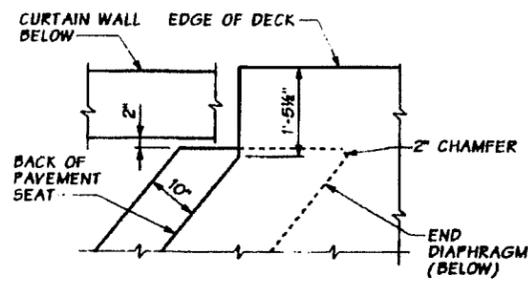
BEARING OF ALL PIERS IS N 31°00'35\"

* TYP. ALL LOCATIONS
4541

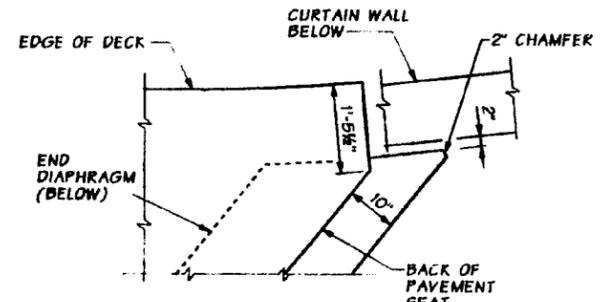


TYPICAL SECTION

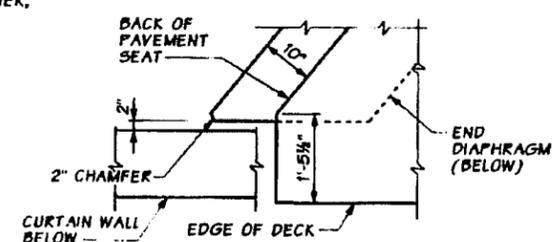
* LIMITS OF PIGMENTED SEALER INCLUDE ALL PERMANENTLY EXPOSED SURFACES OF GIRDERS AND UNDERSIDE OF DECK BETWEEN GIRDERS.



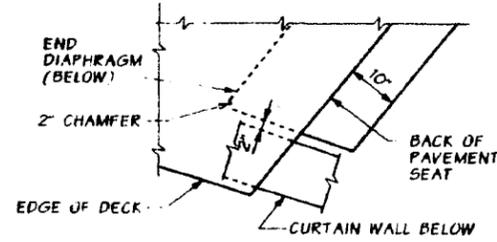
DETAIL A



DETAIL C



DETAIL B



DETAIL D

Bridge Design Engr	Khalighi, B	P:\W3X59501\700CADD\709STRW3X59501_P5_BG_01B.dgn			
Supervisor	Schattler, JG	REG. NO.	STATE	FED. AID PROJ. NO.	SHEET NO.
Designed By	Lu, M	8-11			
Checked By	Dusenberry, KT	8-11	10	WASH	
Detected By	Proffar, DL	8-11			
Bridge Projects Engr					
Prof'n Plan By					
Architect/Specialist					
	DATE	REVISION	BY	APP'D	



US 2
BICKFORD AVENUE I/C
SAFETY AND CULVERT REPLACEMENT
BICKFORD AVENUE OVER US 2 BRIDGE

FRAMING PLAN AND TYPICAL SECTION

SHEET NO.
BG18
296
OF
358
SHEETS



Bridge #	2/8.5N-W	Bridge Name	N-W Ramp (Bickford Ave) over US 2			Structure ID	0018286A	
Contract #	8286	Region	NW	Project Engineer	Mark Sawyer	Performance Deck Concrete?	Yes	
Contractor	Granite Construction		Concrete Supplier	Concrete Nor'West		Deck Placement	4/3/2013	
Bridge Description	2-Span (145' / 145'), 4-WF66G Girders (290' bridge length), 1-Lane (32' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

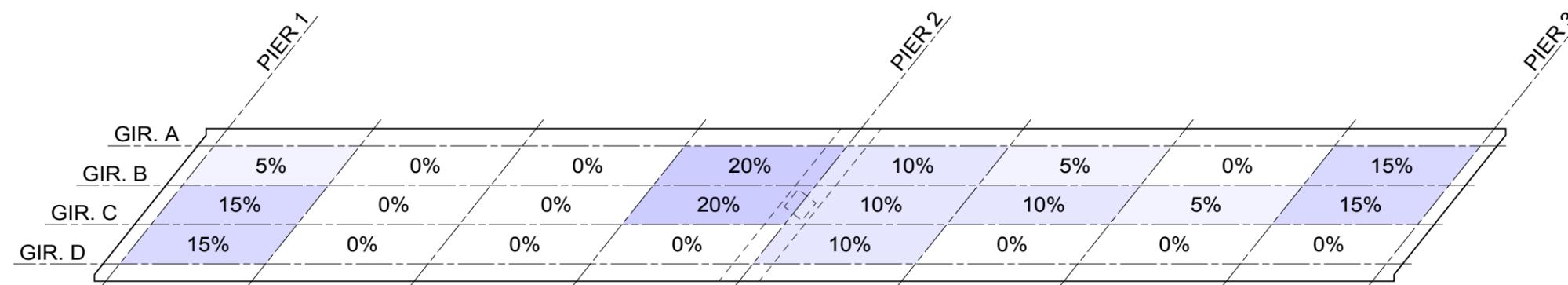
N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	6%
Min. =	0%
Max. =	20%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	36.25	8.75	1	18	5%
1	1	B	C	36.25	8.75	3	18	15%
1	1	C	D	36.25	8.75	3	18	15%
1	2	A	B	36.25	8.75	0	18	0%
1	2	B	C	36.25	8.75	0	18	0%
1	2	C	D	36.25	8.75	0	18	0%
1	3	A	B	36.25	8.75	0	18	0%
1	3	B	C	36.25	8.75	0	18	0%
1	3	C	D	36.25	8.75	0	18	0%
1	4	A	B	36.25	8.75	4	18	20%
1	4	B	C	36.25	8.75	4	18	20%
1	4	C	D	36.25	8.75	0	18	0%
2	1	A	B	36.25	8.75	2	18	10%
2	1	B	C	36.25	8.75	2	18	10%
2	1	C	D	36.25	8.75	2	18	10%
2	2	A	B	36.25	8.75	1	18	5%
2	2	B	C	36.25	8.75	2	18	10%
2	2	C	D	36.25	8.75	0	18	0%
2	3	A	B	36.25	8.75	0	18	0%
2	3	B	C	36.25	8.75	1	18	5%
2	3	C	D	36.25	8.75	0	18	0%
2	4	A	B	36.25	8.75	3	18	15%
2	4	B	C	36.25	8.75	3	18	15%
2	4	C	D	36.25	8.75	0	18	0%



CRACKING INTENSITY ~ BRIDGE 2/8.5N-W

100% = CRACK EVERY 2 FT.

LESS CRACKING

MORE CRACKING

BRIDGE NUMBER	2/8.5N-W
BRIDGE NAME	N-W RAMP (BICKFORD AVE) OVER US 2
INSPECTION DATE	5/21/2015
DECK CONCRETE	PERFORMANCE BASED

BRIDGE 395/441N-E (N-E RAMP OVER N-N RAMP)

Bridge #	395/441N-E	Bridge Name	N-E Ramp Over N-N Ramp		Structure ID	0017610E	
Contract #	7610	Region	ER	Project Engineer	Bob Hilmes	Performance Deck Concrete?	Yes
Contractor	Graham Construction		Concrete Supplier	Central Pre-Mix Conc.	Deck Placement	7/29/2010	
Bridge Description	2-Span (110' / 110"), 4-WF58G Girders (220' bridge length), 2-Lanes (37' wide roadway)						



CONTENTS

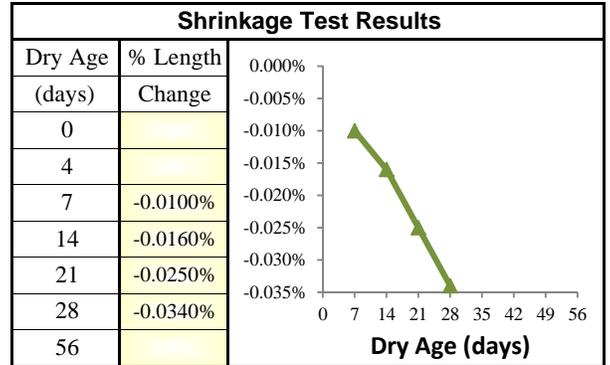
1. Layout Plan Sheet
2. Mix Design Summary
3. Concrete Mix Design Form
4. Concrete Test Results
5. Field Notes
6. Crack Summary
7. Crack Intensity Diagram



Bridge #	395/441N-E	Bridge Name	N-E Ramp Over N-N Ramp		Structure ID	0017610E	
Contract #	7610	Region	ER	Project Engineer	Bob Hilmes	Performance Deck Concrete?	Yes
Contractor	Graham Construction		Concrete Supplier	Central Pre-Mix Conc.		Deck Placement	7/29/2010
Bridge Description							2-Span (110' / 110"), 4-WF58G Girders (220' bridge length), 2-Lanes (37' wide roadway)

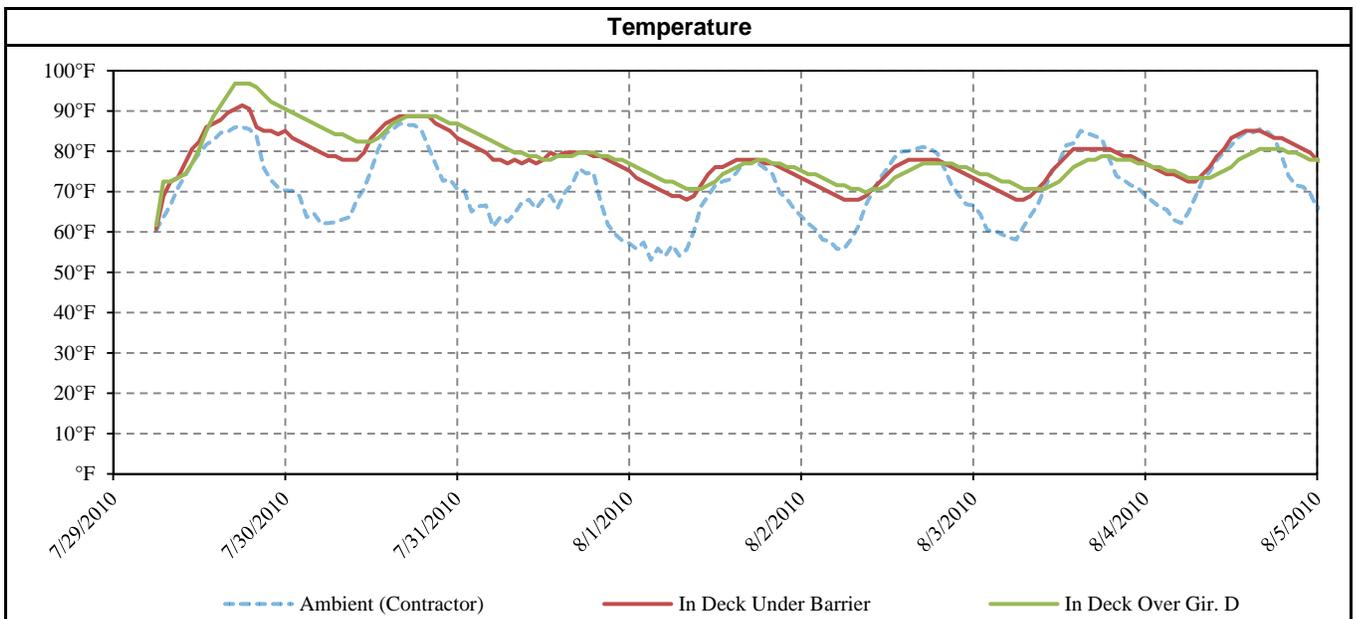
Mix Design (WSDOT Form 350-040)			
Water (max) =		220 lbs/cy	w/c = 0.39 max
Cementitious Materials	Lbs/cy	Source	Type, Class or Grade
cement	435	Lafarge	Type I
fly ash	130	Wabamun/Sundance	Type F
slag			
latex			
microsilica			
Concrete Admixtures	oz/cy	Manufacturer	Product
air entrainment	15 to 45	WR Grace	Daravair 1000
water reducer	15 to 40	WR Grace	WRDA 64
HR water reduce	11 to 25	WR Grace	Adva 190 or 195
set retarder			
shrink. reducer	128	WR Grace	Eclipse Plus

Concrete Test Results		
compressive strength @ 28 days	5,660	psi
modulus of elasticity		psi
permeability @ 56 days	1,452	coulombs
mix design density	140.6	lb/cf



Aggregate					
	Comp. 1	Comp. 2	Comp. 3	Comp. 4	Comp. 5
WSDOT Pit #	PS C-173 PS C-107	PS C-173 PS C-108	PS C-173 PS C-109	PS C-173 PS C-110	PS C-297 PS C-120
Grading	1½ Round	¾ Round	¾ Round	Course Sand	Blend Sand
% Total	16.0%	36.0%	10.0%	24.0%	1400.0%
Lbs/cy	490	1090	300	710	420
ASR Mitigation Low Alkali Cement and Flyash					

Notes
This was pilot bridge for performance based mix design
Original contract called for a different bridge to use the performance based specification, but schedule conflicts necessitated changing to this bridge.





Contractor Graham Construction & Management, Inc.		Submitted By Craig L. Matteson Central Pre-Mix Concrete Co.	Date 2/6/2009
Concrete Supplier Central Pre-Mix Concrete Co.		Plant Location 1901 N. Sullivan Rd. 302 N. Park Rd. or Crestline & Magnesium	
Contract Number 7610	Contract Name US 395 / NSC - US 2 Lowering		

This mix is to be used in the following Bid Item No(s): 4000D Bridge Deck Project Specific Performance Mix

Concrete Class: (check one only)

Item # 74

- 3000
 4000
 4000^a
 4000^aP
 4000W
 Concrete Overlay
 Cement Concrete Pavement^d
 Other Eclipse Plus

Remarks: Bridge Deck Concrete for US 395 SB Over US 2 Bridge. The Total Paste Volume is 6.75 cf or 25.0%

Mix Design No. 320292 Plant No. 1, 3 or 4

Cementitious Materials	Source	Type, Class or Grade	Sp. Gr.	Lbs/cy
Cement	Lafarge Richmond, BC	AASHTO Type I	3.15	435
Fly Ash ^a	Wabamun or Sundance	Type F	2.01	130 ^v
GGBFS (Slag)				
Latex				
Microsilica				

Concrete Admixtures	Manufacturer	Product	Type	Est. Range (oz/cy)
Air Entrainment	WR Grace	Daravair 1000		15 to 45
Water Reducer	WR Grace	WRDA 64	A & D	15-40
High-Range Water Reducer	WR Grace	Adva 190 or 195	HRWRA	11-25
Set Retarder				
Other Eclipse Plus	WR Grace	Shrinkage Reducing	S	128

Water (Maximum) 220 lbs/cy Is any of the water Recycled or Reclaimed? Yes^e No

Water Cementitious Ratio (Maximum) .39 Mix Design Density 140.6 +/- lbs/cf^d

Design Performance	1	2	3	4	5	Average ^f
28 Day Compressive Strength (cylinders) psi	5,680	5,670	5,640	RECEIVED		5,660
14 Day Flexural ^d Strength (beams) psi				FEB 06 2009		

Agency Use Only (Check appropriate Box) HILMES P.E.O.

This Mix Design MEETS CONTRACT SPECIFICATIONS and may be used on the bid items noted above
 This Mix Design DOES NOT MEET CONTRACT SPECIFICATIONS and is being returned for corrections

Reviewed By: _____ Date: _____

PE Signature Date

Mix Design No. 320292 Plant No. 1, 3 or 4

Aggregate Information

Concrete Aggregates	Component 1	Component 2	Component 3	Component 4	Component 5	Combined Gradation
WSDOT Pit No.	PS C-173 or PS C-107	PS C-297 & PS C-120				
WSDOT ASR 14-day Results (%) ^b	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No					
Grading ^c	1 1/2" Round Combined	3/4" Round Combined	3/8" Round Combined	Course Sand Combined	Blend Sand Combined	
Percent of Total Aggregate	16	36	10	24	14	100%
Specific Gravity	2.69	2.68	2.67	2.64	2.64	
Lbs/cy (ssd)	490	1090	300	710	420	1 1/2" NMA Specification

Percent Passing

2 inch						
1-1/2 inch	100					100 100
1 inch	42.9	100				91.0
3/4 inch	4.7	92.2				82.0 62-88
1/2 inch	1.0	55.1	100			67.9
3/8 inch	.7	30.7	99.0	100	100	59.0 43-64
No. 4		2.6	32.9	96.2	99.4	41.2 ✓ 29-47
No. 8		.8	4.9	58.1	97.1	28.3 ✓ 19-34
No. 16		.5	1.2	18.9	87.9	17.1 ✓ 12-25
No. 30		.4	.7	6.5	60.6	10.3 ✓ 7-18
No. 50		.3	.6	2.8	26.4	4.5 ✓ 3-14
No. 100		.3	.5	1.4	8.0	1.6 ✓ 0-10
No. 200	.5	.3	.4	1.0	3.7	1.0 ✓ 0-2.0

Fineness Modulus: N/A (Required for Class 2 Sand)

ASR Mitigation Method Proposed^b: Using Low Alkali Cement and Flyash ✓

Notes:

- ^a Required for Class 4000D and 4000P mixes.
- ^b Alkali Silica Reactivity Mitigation is required for sources with expansions over 0.20% - Incidate method for ASR mitigation. For expansion of 0.21% - 0.45%, acceptable mitigation can be the use of low alkali cement or 25% type F fly ash. Any other proposed mitigation method or for pits with greater than 0.45% expansion, proof of mitigating measure, either ASTM C1260 / AASHTO T303 test results must be attached. If ASTM C 1293 testing has been submitted indicating 1-year expansion of 0.04% or less, mitigation is not required.
- ^c AASHTO No. 467, 57, 67, 7, 8; WSDOT Class 1, Class 2; or combined gradation. See Standard Specification 9-03.1.
- ^d Required for Cement Concrete Pavements.
- ^e Attach test results indicating conformance to Standard Specification 9-25.1.
- ^f Actual Average Strength as determined from testing or estimated from ACI 211.



Should be test
HASATO T 277

Lafarge North America Concrete Lab
5400 W Marginal Way SW
Seattle, WA. 98106

Report To: Central Pre-Mix Concrete Co.
Attention: Quality Control Personnel

Date: November 22, 2008

Subject: Rapid Chloride Ion Penetration ASTM C-1202

Date Sampled: September 2008

Mix Design: HPC #2

Results:

Age (Days)
56

Coulombs
1452

The test result is only valid if the aggregate(s) sample(s) is(are) representative of the current production and it is to be noted that Lafarge has no knowledge of the representatives of the sample received for testing. Also, material quality can vary with different locations in a quarry. It is recommended that testing be carried out on an annual basis or more frequently if a variation in stone quality is suspected.

Although the Lafarge North America Seattle Concrete Lab. applies state-of-the-art test methods, Lafarge North America, and its affiliates (Lafarge) can not guarantee the results shown above and shall assume no liability whatsoever for any errors in such results and for the consequence of such errors.

Sincerely,

Rob Shogren, P.E.
Technical Service Engineer
Lafarge North America

RECEIVED

FEB 06 2009

HILMES P.E.O.



Lafarge North America Concrete Lab
5400 W Marginal Way SW
Seattle, WA. 98106

Report To: CPM Spokane
Attention: Quality Control Personnel

Date: October 30, 2008

Subject: ASTM C-157 Standard Method for Length Change of Hardened Hydraulic-Cement Mortar and Concrete

Tested Materials: Date Sampled: Sept 2008
Mix Design ID: Mix #2

ASTM C-157 Expansion: Three (3) test bars were prepared from each concrete mixture. Results are an average of the three (3) bars.

Age (Days)	Percent Length Change
7	#1 0.010%
14	0.016%
21	0.025%
28 (final)	0.034%

* The test result is only valid if the aggregate(s) sample(s) is(are) representative of the current production and it is to be noted that Lafarge has no knowledge of the representatives of the sample received for testing. Also, material quality can vary with different locations in a quarry. It is recommended that testing be carried out on an annual basis or more frequently if a variation in stone quality is suspected.

Although the Lafarge North America Seattle Concrete Lab. applies state-of-the-art test methods, Lafarge North America, and its affiliates (Lafarge) can not guarantee the results shown above and shall assume no liability whatsoever for any errors in such results and for the consequence of such errors.

Rob Shogren, P.E.
Technical Service Engineer
Lafarge North America

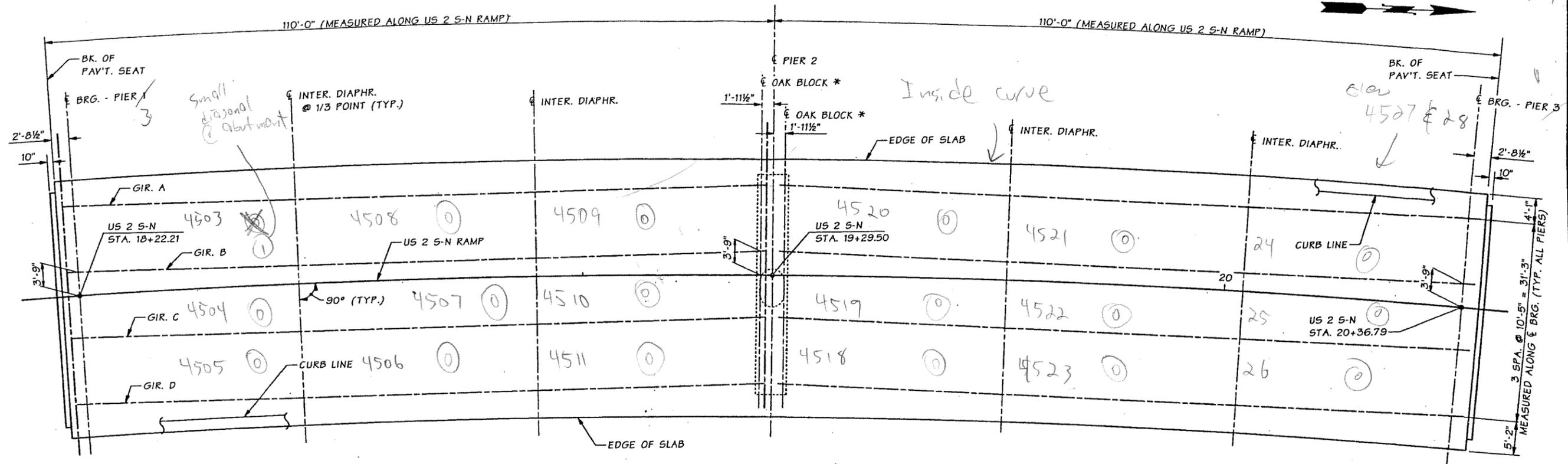
RECEIVED

FEB 06 2009

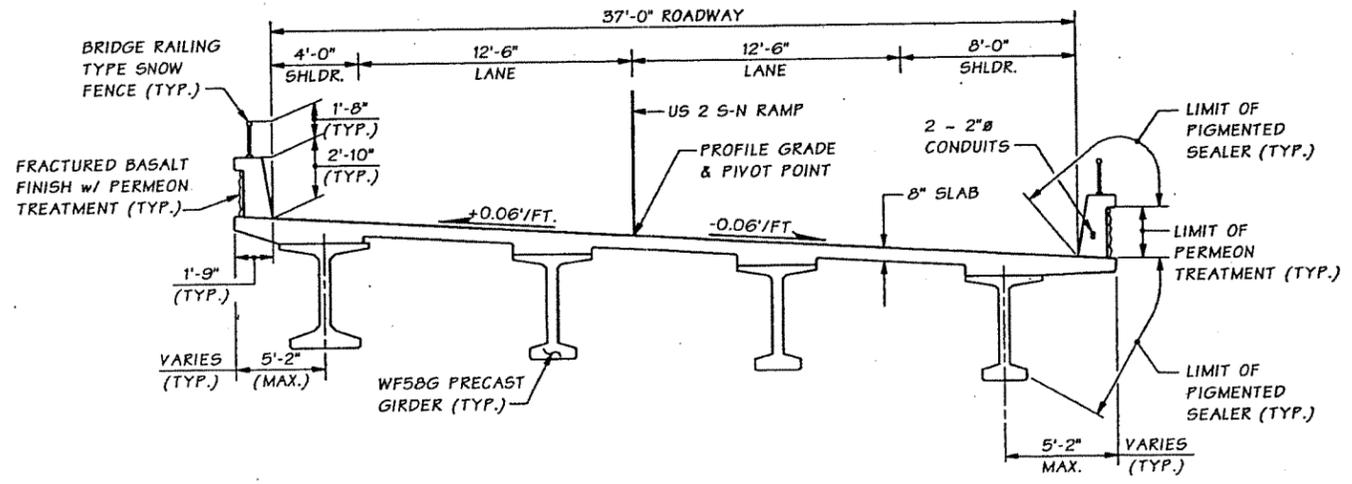
HILMES P.E.O.

Should be test
ASSHTD T/60

Doc 29, 30, 31



FRAMING PLAN
* SEE "OAK BLOCK DETAIL" BR. SHT. SN10



TYPICAL SECTION

SR 395 FILE NO. SHEET SN22

Bridge Design Engr.	khaleghi, B	M:\Z-Team\NSC - SR 395\PS&E\NB S-N OXING\window files\FRAMING PLAN.WND			
Supervisor	Zeldenrust, RP	REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO. TOTAL SHEETS
Designed By	Bedi, G 05/07	10	WASH.		
Checked By	Rosa, M 03/08	JOB NUMBER 082011			
Detailed By	Andreotti, L 05/07				
Bridge Projects Engr.					
Prelim. Plan By		DATE	REVISION	BY	APP'D
Architect/Specialist					



BRIDGE AND STRUCTURES OFFICE



US 395 NSC - US 2 LOWERING		BRIDGE SHEET NO. SN22
S - N RAMP OVER EW - N RAMP BRIDGE		SHEET 448 OF 548 SHEETS
FRAMING PLAN		

395/441 N-E



Bridge #	395/441N-E	Bridge Name	N-E Ramp Over N-N Ramp			Structure ID	0017610E	
Contract #	7610	Region	ER	Project Engineer	Bob Hilmes	Performance Deck Concrete?	Yes	
Contractor	Graham Construction		Concrete Supplier	Central Pre-Mix Conc.		Deck Placement	7/29/2010	
Bridge Description	2-Span (110' / 110"), 4-WF58G Girders (220' bridge length), 2-Lanes (37' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

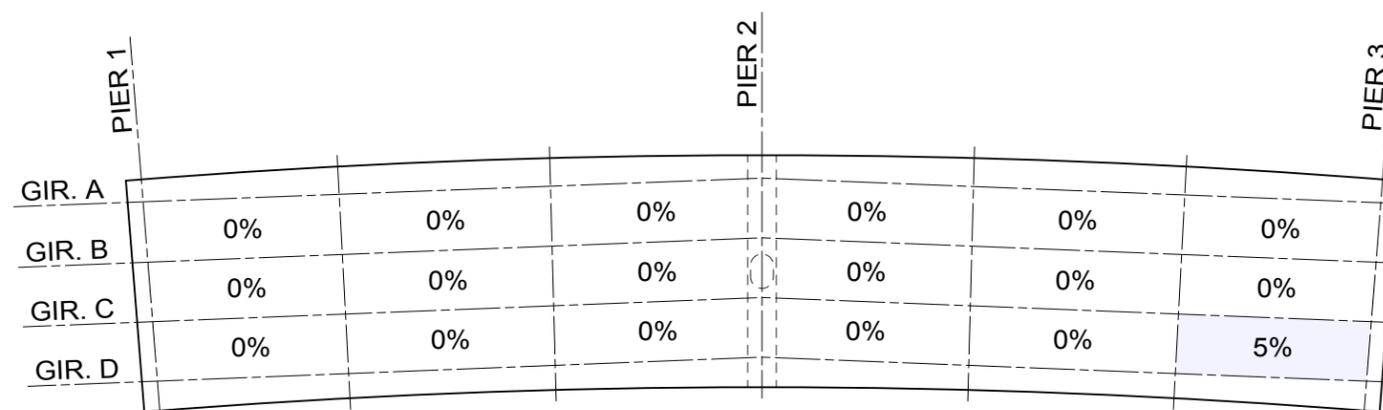
N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	0%
Min. =	0%
Max. =	5%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	36.67	10.42	0	18	0%
1	1	B	C	36.67	10.42	0	18	0%
1	1	C	D	36.67	10.42	0	18	0%
1	2	A	B	36.67	10.42	0	18	0%
1	2	B	C	36.67	10.42	0	18	0%
1	2	C	D	36.67	10.42	0	18	0%
1	3	A	B	36.67	10.42	0	18	0%
1	3	B	C	36.67	10.42	0	18	0%
1	3	C	D	36.67	10.42	0	18	0%
2	1	A	B	36.67	10.42	0	18	0%
2	1	B	C	36.67	10.42	0	18	0%
2	1	C	D	36.67	10.42	0	18	0%
2	2	A	B	36.67	10.42	0	18	0%
2	2	B	C	36.67	10.42	0	18	0%
2	2	C	D	36.67	10.42	0	18	0%
2	3	A	B	36.67	10.42	0	18	0%
2	3	B	C	36.67	10.42	0	18	0%
2	3	C	D	36.67	10.42	1	18	5%



CRACKING INTENSITY ~ BRIDGE 395/441N-E

100% = CRACK EVERY 2 FT.

LESS CRACKING

MORE CRACKING



BRIDGE NUMBER	395/441N-E
BRIDGE NAME	N-E RAMP OVER N-N RAMP
INSPECTION DATE	5/21/2015
DECK CONCRETE	PERFORMANCE BASED

APPENDIX C

MULTI-SPAN PRESTRESSED GIRDER BRIDGES

BRIDGE 3034A (MANETTE BRIDGE)

BRIDGE 90/106N (Gold CREEK WB)

6/115 (SOUTH FORK CHEHALIS RIVER)

BRIDGE 5/234W (I-5 OVER BLAKESLEE JUNCTION RAILROAD)

BRIDGE 105/4 (NORTH RIVER)

BRIDGE 105/3 (SMITH CREEK)

BRIDGE 6/8 (WILLAPA RIVER)

BRIDGE 5/232NCD (SKOOKUMCHUCK RIVER NBCD)

BRIDGE 5/232SCD (SKOOKUMCHUCK RIVER SBCD)

BRIDGE 101/44 (BONE RIVER)

BRIDGE 3034A (MANETTE BRIDGE)

Bridge #	303/4A	Bridge Name	Manette Bridge		Structure ID	0017926A	
Contract #	7926	Region	OR	Project Engineer	Michele Britton	Performance Deck Concrete?	No
Contractor	Manson-Mowat, A J.V.		Concrete Supplier		Deck Placement	≈ 2011	
Bridge Description	7-Span (160' / 250' / 250' / 250' / 250' / 140'), 4-P.C./P.T. Girders (1550' bridge length), 2-Lanes (44' wide)						



CONTENTS

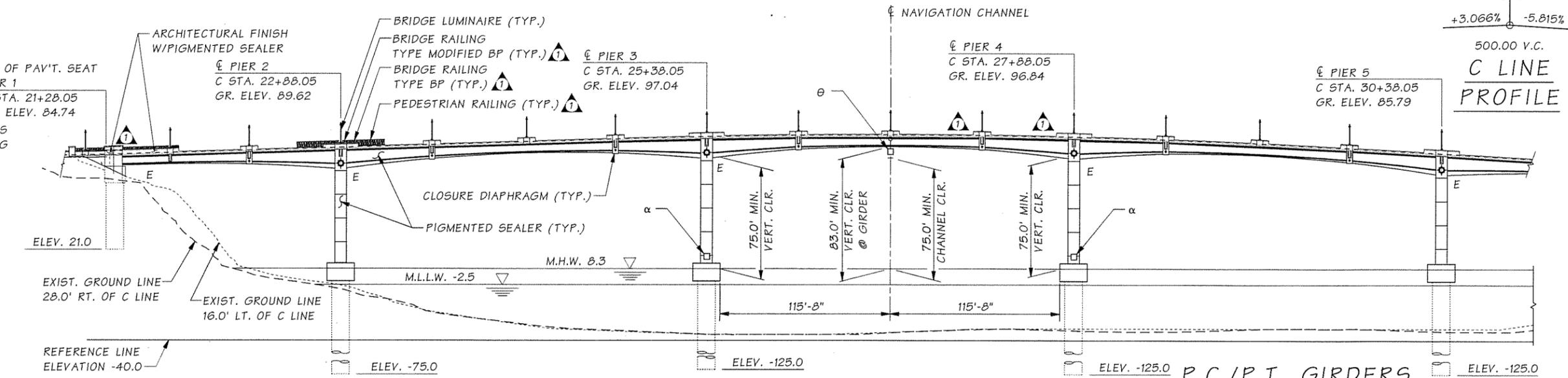
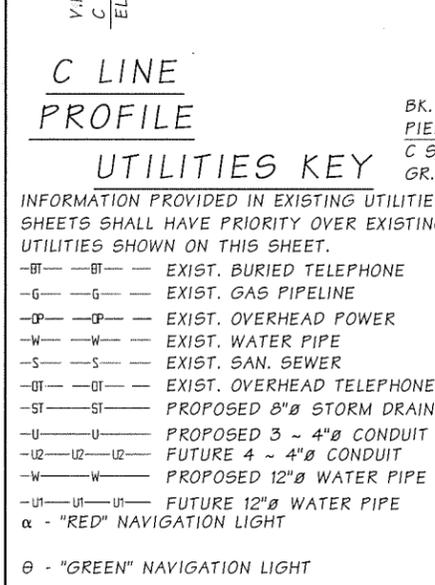
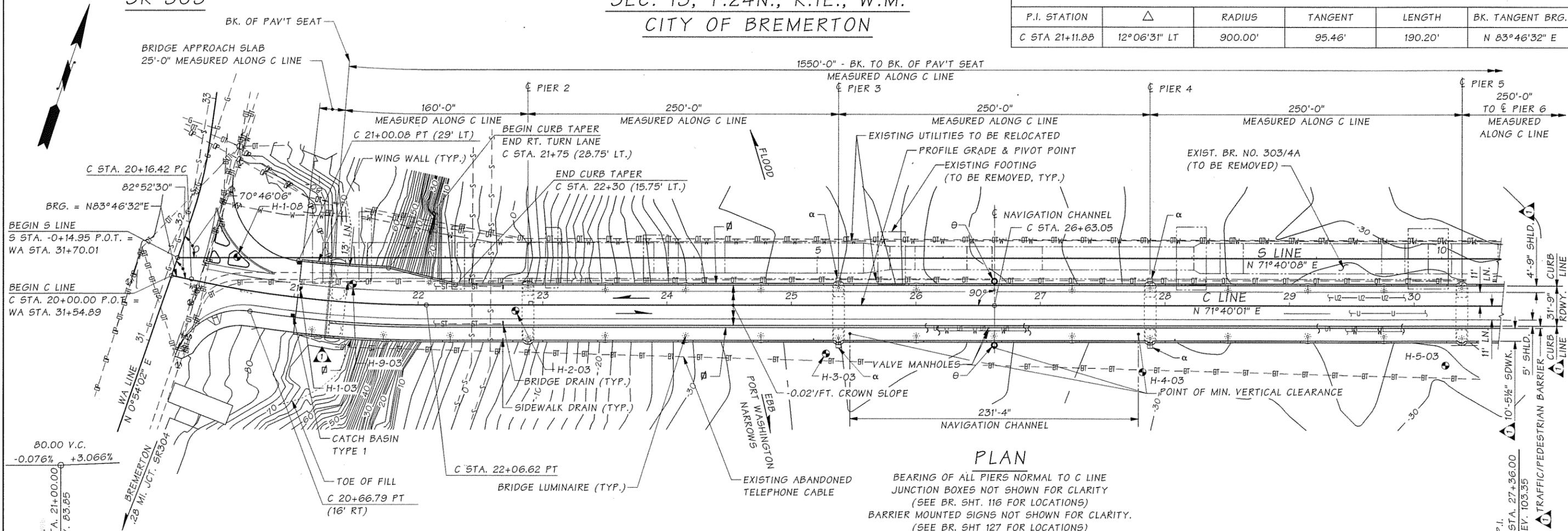
1. Layout Plan Sheet
2. Field Notes
3. Crack Summary
4. Crack Intensity Diagram

SR 303

SEC. 13, T.24N., R.1E., W.M.
CITY OF BREMERTON

CURVE DATA

P.I. STATION	Δ	RADIUS	TANGENT	LENGTH	BK. TANGENT BRG.
C STA 21+11.88	12°06'31" LT	900.00'	95.46'	190.20'	N 83°46'32" E



- UTILITIES KEY
- INFORMATION PROVIDED IN EXISTING UTILITIES SHEETS SHALL HAVE PRIORITY OVER EXISTING UTILITIES SHOWN ON THIS SHEET.
- BT - EXIST. BURIED TELEPHONE
 - G - EXIST. GAS PIPELINE
 - OP - EXIST. OVERHEAD POWER
 - W - EXIST. WATER PIPE
 - S - EXIST. SAN. SEWER
 - OT - EXIST. OVERHEAD TELEPHONE
 - ST - PROPOSED 8" STORM DRAIN
 - U - PROPOSED 3 - 4" CONDUIT
 - U2 - FUTURE 4 - 4" CONDUIT
 - W - PROPOSED 12" WATER PIPE
 - U1 - FUTURE 12" WATER PIPE
 - R - "RED" NAVIGATION LIGHT
 - θ - "GREEN" NAVIGATION LIGHT
 - ∅ - CONDUIT PIPES IN TRAFFIC, TRAFFIC/PEDESTRIAN, & PEDESTRIAN BARRIERS NUMBER & SIZE VARY ALONG LENGTH OF BRIDGE.

DATUM
N.A.V.D. OF 1988

Bridge Design Engr.	khaleghi, B	M:\w-Team\MANETTE SR303>window files\NB-LAYOUT1.wnd	REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
Supervisor	Clarke, PT		10	WASH.			
Designed By	ADM, EJF	03/10					
Checked By	EJF, ADM						
Detailed By	Puryear, D	03/10					
Bridge Projects Engr.	Lewis, RA	06/2011					
Prelim. Plan By	Messmer, A	04/10					
Architect/Specialist	Kinderman, P						

Washington State Department of Transportation

BRIDGE AND STRUCTURES OFFICE

6/9/11

MANETTE BRIDGE 303/4A
BRIDGE REPLACEMENT

LAYOUT
1 OF 2

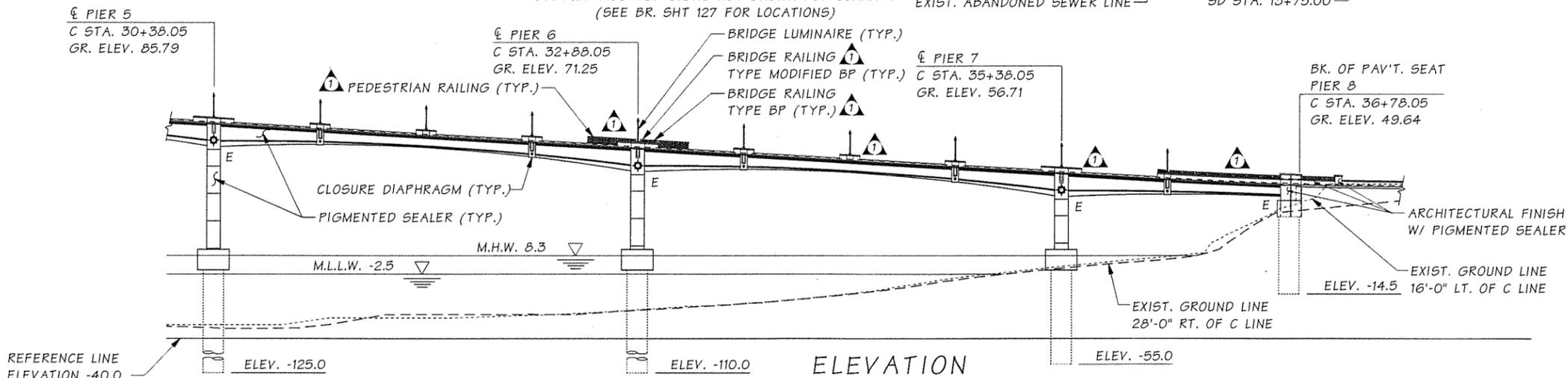
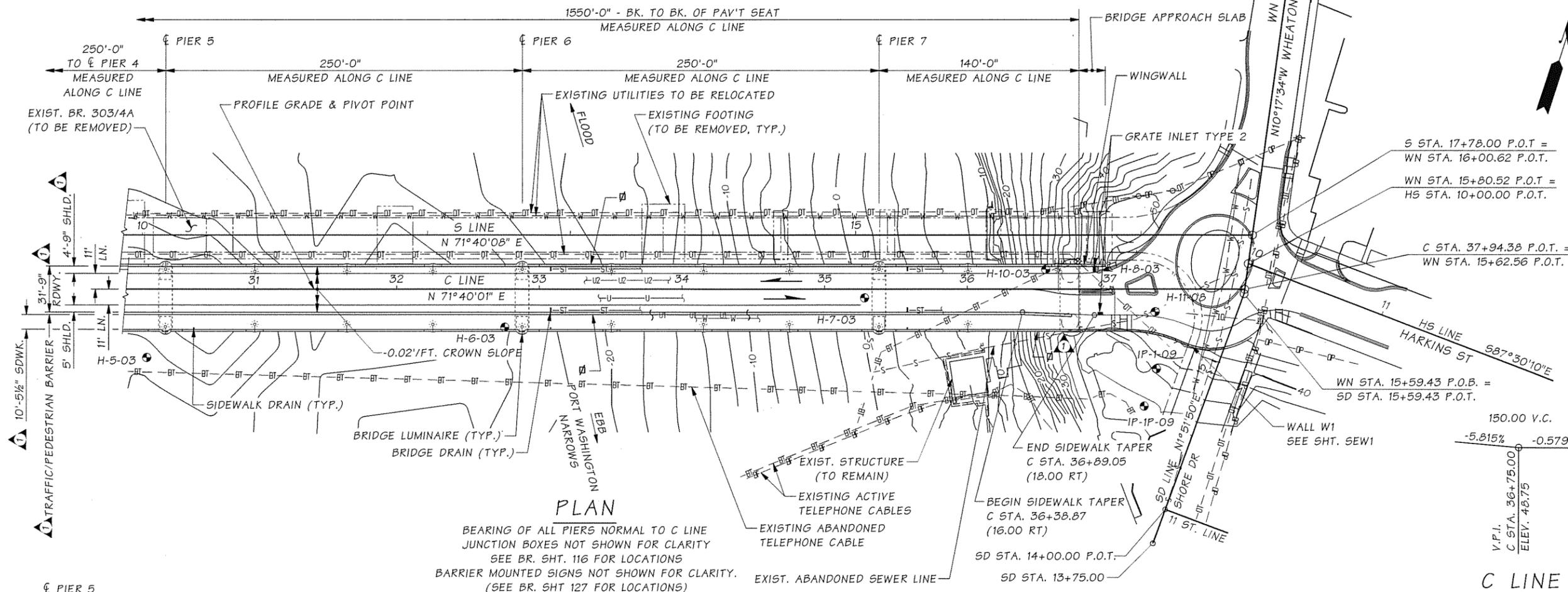
BRIDGE SHEET NO. 1
SHEET 161 OF 303 SHEETS

SR 303 FILE NO. 7004 SHEET 1

PROJ. NO. 0L2829 ~ OLYMPIC REGION ~ MANETTE BR. BREMERTON VIC BR. REPLACEMENT ~ SR 303 SPUR

SEC. 13, T.24N., R.1E., W.M.
CITY OF BREMERTON

SR 303



UTILITIES KEY

INFORMATION PROVIDED IN EXISTING UTILITIES SHEETS SHALL HAVE PRIORITY OVER EXISTING UTILITIES SHOWN ON THIS SHEET.

- BT--BT-- EXIST. BURIED TELEPHONE
- G--G-- EXIST. GAS PIPELINE
- OP--OP-- EXIST. OVERHEAD POWER
- W--W-- EXIST. WATER PIPE
- S--S-- EXIST. SAN. SEWER
- OT--OT-- EXIST. OVERHEAD TELEPHONE
- ST--ST-- PROPOSED 8" STORM DRAIN
- U--U-- PROPOSED 3 - 4" CONDUIT
- U2--U2-- FUTURE 4 - 4" CONDUIT
- W--W-- PROPOSED 12" WATER PIPE
- U1--U1-- FUTURE 12" WATER PIPE

Ø - CONDUIT PIPES IN TRAFFIC, TRAFFIC/PEDESTRIAN, & PEDESTRIAN BARRIERS NUMBER & SIZE VARY ALONG LENGTH OF BRIDGE.

Bridge Design Engr.	Khaleghi, B	M:\W-Team\MANETTE SR303>window files\NB-LAYOUT2.wnd
Supervisor	Clarke, PT	
Designed By	ADM, EJF	03/10
Checked By	EJF, ADM	
Detailed By	Puryear, D	03/10
Bridge Projects Engr.	Lewis, RA	06/2011
Prelim. Plan By	Messmer, A	03/10
Architect/Specialist	Kinderman, P	

REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
10	WASH.			
JOB NUMBER				
09C526				
DATE	REVISION	BY	APP'D	



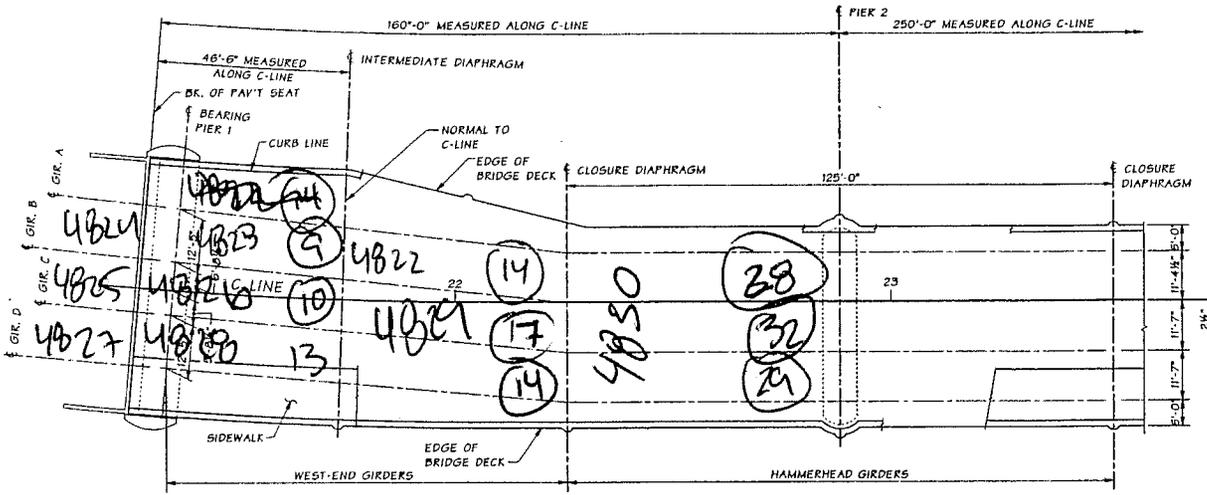
Washington State
Department of Transportation
BRIDGE AND STRUCTURES OFFICE

MANETTE BRIDGE 303/4A
BRIDGE REPLACEMENT

LAYOUT
2 OF 2

C.S. 1841 ~ PROJ. NO. 012829 ~ OLYMPIC REGION ~ MP 2.98 TO 3.27 ~ SR 303 SPUR ~ MANETTE BR. NO. 303/4A REPL.

SR FILE NO. SHEET 2



FRAMING PLAN
 BEARING PIER 1 IS PARALLEL TO BACK OF PAV'T SEAT.

SR. FILE NO. SHEET 50

Bridge Design Engr.	khaleghi, B								
Supervisor	Clarke, PT								
Designed By	Hessner, A	03/10							
Checked By	Spitznas, P								
Detailed By	Puryear, D	03/10							
Bridge Projects Engr.									
Prepn. Plan By									
Architect/Specalist									
DATE		REVISION		BY	APPT				

WASH STATE	FED. AID PROJ. NO.	PERM NO.	TOTAL SHEETS
10 WASH			
JOB NUMBER	09C526		

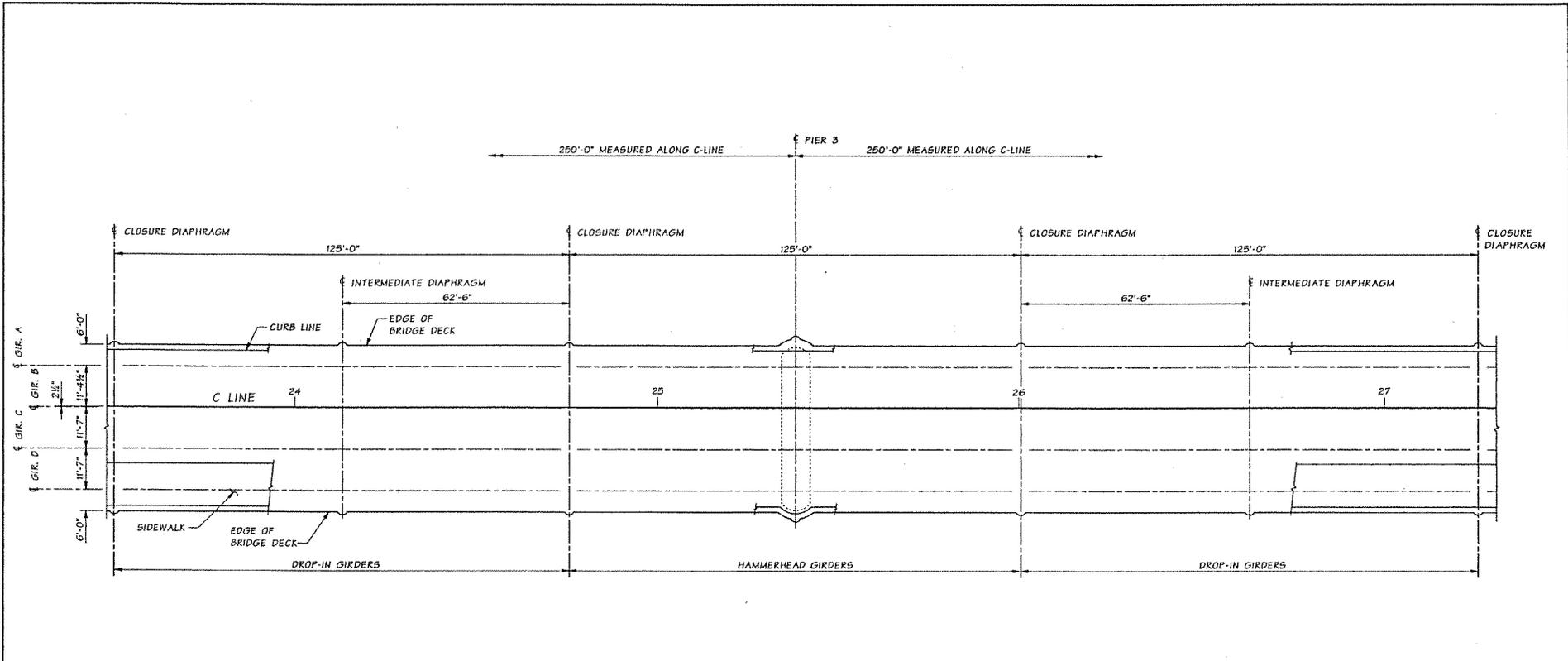
3/17/10

Washington State Department of Transportation
 BRIDGE AND STRUCTURES OFFICE

**MANETTE BRIDGE 303/4A
 BRIDGE REPLACEMENT**

FRAMING PLAN
 1 OF 5

SHEET NO.	60
TOTAL	220
OF	303
SHEET	303



FRAMING PLAN

SR FILE NO. SHEET 61

Bridge Design Eng.	Khalighi, B	M:\w-team\MANETTE SR303\window files\42-FRAMING PLAN2.WND
Supervisor	Clarke, PT	
Designed By	Messner, A	03/10
Checked By	Spitznas, P	
Detaild By	Gunn's, E	03/10
Bridge Projects Eng.		
Drawn Plan By		
Project Specialist		
DATE	REVISION	BY APPD

BRIDGE NO. STATE FED. AID PROJ. NO. WAY NO. TOTAL SECTS.

10 WASH.

JOB NUMBER 09C526

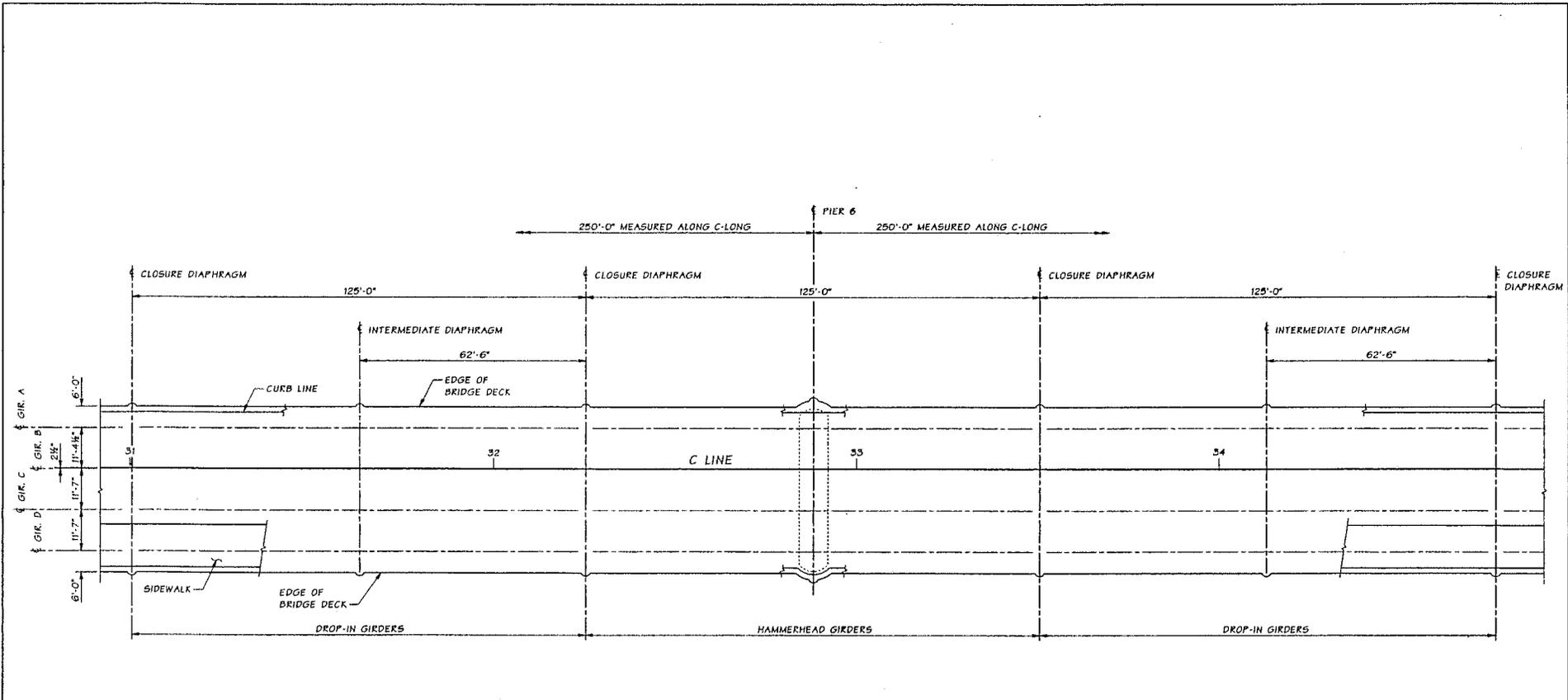
3/17/10



Washington State Department of Transportation

BRIDGE AND STRUCTURES OFFICE

MANETTE BRIDGE 303/4A BRIDGE REPLACEMENT	61
FRAMING PLAN 2 OF 5	221 OF 303 31423



FRAMING PLAN

SR FILE NO. SHEET 63

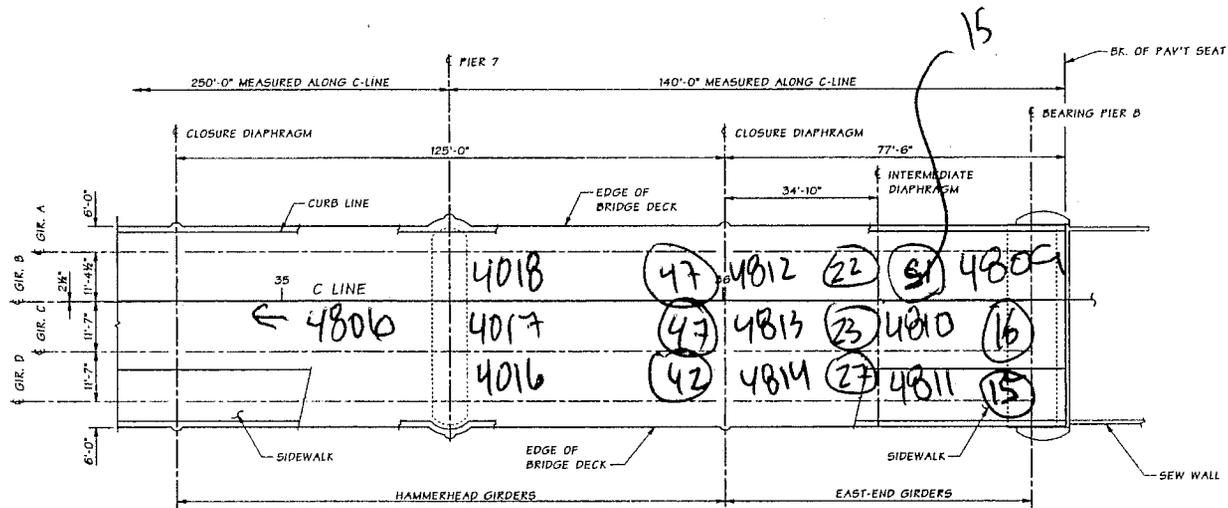
Bridge Design Engr	khaleghi, B	M:\w-Team\MANETTE SR303\window files\44-FRAMING PLAN.dwg
Supervisor	Clarke, PI	
Designed By	Ferluga, E	03/10
Checked By	Spiczmas, P	
Detailled By	Gunn, E	03/10
Bridge Projects Engr		
Prepn. Plan By		
Architect/Specifier		
DATE	REVISION	BY APPD

REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
30	WASH.			
JOB NUMBER		09C526		

3/17/10



MANETTE BRIDGE 303/4A BRIDGE REPLACEMENT	63 of 223 303
FRAMING PLAN 4 OF 5	



FRAMING PLAN

SR FILE NO. SHEET 64

Bridge Design Engr.	Khalighi, B	M:\W-Team\MANETTE SR303\window files\45-FRAMING PLANS.WPD
Supervisor	Clarke, PT	
Designed By	Hessmer, A	03/10
Checked By	Spitznas, P	
Detailled By	Guthis, E	03/10
Bridge Projects Engr.		
Prefer. Plan By		
Architect/Speciaist		
DATE	REVISION	BY APPD

REG#	STATE	FED. AID PROJ. NO.	FBI	TOTAL
10	WASH			
JOB NUMBER CUC326				

Professional Engineer Seal: Gregory D. Vetter, License No. 10000, State of Washington, expires 12/31/10. Date: 4/17/10.

Professional Surveyor Seal: License No. 10000, State of Washington, expires 12/31/10. Date: 4/17/10.

Washington State Department of Transportation
BRIDGE AND STRUCTURES OFFICE

MANETTE BRIDGE 303/4A
BRIDGE REPLACEMENT

FRAMING PLAN
5 OF 5

SHEET NO.	64
SHEET	224
OF	303
DATE	2010

WSP Mar 17 15:35:33 2010



Bridge #	303/4A	Bridge Name	Manette Bridge			Structure ID	0017926A	
Contract #	7926	Region	OR	Project Engineer	Michele Britton	Performance Deck Concrete?	No	
Contractor	Manson-Mowat, A J.V.		Concrete Supplier			Deck Placement	≈ 2011	
Bridge Description	7-Span (160' / 250' / 250' / 250' / 250' / 250' / 140'), 4-P.C./P.T. Girders (1550' bridge length), 2-Lanes (44' wide)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr} / N_{100} (rounded to the nearest 5%)

Avg. =	73%
Min. =	45%
Max. =	100%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	38.67	12.24	9	19	45%
1	1	B	C	38.67	12.24	10	19	55%
1	1	C	D	38.67	12.24	13	19	70%
1	2	A	B	51.00	11.82	14	26	55%
1	2	B	C	51.00	11.82	17	26	65%
1	2	C	D	51.00	11.82	14	26	55%
1	3	A	B	62.50	11.58	28	31	90%
1	3	B	C	62.50	11.58	32	31	100%
1	3	C	D	62.50	11.58	29	31	95%
2	1	A	B	62.50	11.58	#N/A	31	#N/A
2	1	B	C	62.50	11.58	#N/A	31	#N/A
2	1	C	D	62.50	11.58	#N/A	31	#N/A
2	2	A	B	62.50	11.58	#N/A	31	#N/A
2	2	B	C	62.50	11.58	#N/A	31	#N/A
2	2	C	D	62.50	11.58	#N/A	31	#N/A
2	3	A	B	62.50	11.58	#N/A	31	#N/A
2	3	B	C	62.50	11.58	#N/A	31	#N/A
2	3	C	D	62.50	11.58	#N/A	31	#N/A
2	4	A	B	62.50	11.58	#N/A	31	#N/A
2	4	B	C	62.50	11.58	#N/A	31	#N/A
2	4	C	D	62.50	11.58	#N/A	31	#N/A
3	1	A	B	62.50	11.58	#N/A	31	#N/A
3	1	B	C	62.50	11.58	#N/A	31	#N/A
3	1	C	D	62.50	11.58	#N/A	31	#N/A
3	2	A	B	62.50	11.58	#N/A	31	#N/A
3	2	B	C	62.50	11.58	#N/A	31	#N/A
3	2	C	D	62.50	11.58	#N/A	31	#N/A
3	3	A	B	62.50	11.58	#N/A	31	#N/A
3	3	B	C	62.50	11.58	#N/A	31	#N/A
3	3	C	D	62.50	11.58	#N/A	31	#N/A
3	4	A	B	62.50	11.58	#N/A	31	#N/A
3	4	B	C	62.50	11.58	#N/A	31	#N/A
3	4	C	D	62.50	11.58	#N/A	31	#N/A
4	1	A	B	62.50	11.58	#N/A	31	#N/A
4	1	B	C	62.50	11.58	#N/A	31	#N/A
4	1	C	D	62.50	11.58	#N/A	31	#N/A
4	2	A	B	62.50	11.58	#N/A	31	#N/A
4	2	B	C	62.50	11.58	#N/A	31	#N/A
4	2	C	D	62.50	11.58	#N/A	31	#N/A
4	3	A	B	62.50	11.58	#N/A	31	#N/A
4	3	B	C	62.50	11.58	#N/A	31	#N/A



Bridge #	303/4A	Bridge Name	Manette Bridge			Structure ID	0017926A	
Contract #	7926	Region	OR	Project Engineer	Michele Britton	Performance Deck Concrete?	No	
Contractor	Manson-Mowat, A J.V.		Concrete Supplier			Deck Placement	≈ 2011	
Bridge Description	7-Span (160' / 250' / 250' / 250' / 250' / 250' / 140'), 4-P.C./P.T. Girders (1550' bridge length), 2-Lanes (44' wide)							

L = length between diaphragms (or length of "bay")

S = girder spacing

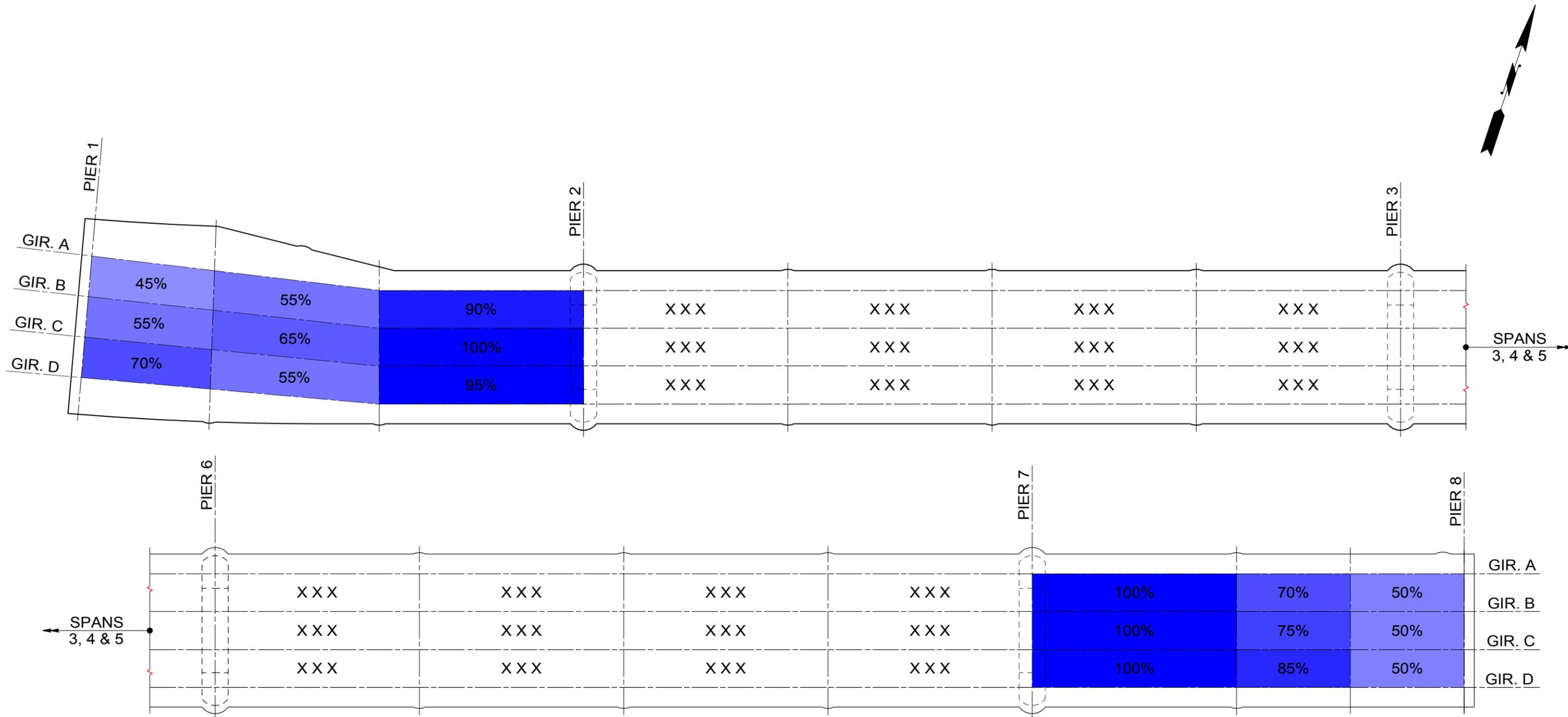
N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	73%
Min. =	45%
Max. =	100%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
4	3	C	D	62.50	11.58	#N/A	31	#N/A
4	4	A	B	62.50	11.58	#N/A	31	#N/A
4	4	B	C	62.50	11.58	#N/A	31	#N/A
4	4	C	D	62.50	11.58	#N/A	31	#N/A
5	1	A	B	62.50	11.58	#N/A	31	#N/A
5	1	B	C	62.50	11.58	#N/A	31	#N/A
5	1	C	D	62.50	11.58	#N/A	31	#N/A
5	2	A	B	62.50	11.58	#N/A	31	#N/A
5	2	B	C	62.50	11.58	#N/A	31	#N/A
5	2	C	D	62.50	11.58	#N/A	31	#N/A
5	3	A	B	62.50	11.58	#N/A	31	#N/A
5	3	B	C	62.50	11.58	#N/A	31	#N/A
5	3	C	D	62.50	11.58	#N/A	31	#N/A
5	4	A	B	62.50	11.58	#N/A	31	#N/A
5	4	B	C	62.50	11.58	#N/A	31	#N/A
5	4	C	D	62.50	11.58	#N/A	31	#N/A
6	1	A	B	62.50	11.58	#N/A	31	#N/A
6	1	B	C	62.50	11.58	#N/A	31	#N/A
6	1	C	D	62.50	11.58	#N/A	31	#N/A
6	2	A	B	62.50	11.58	#N/A	31	#N/A
6	2	B	C	62.50	11.58	#N/A	31	#N/A
6	2	C	D	62.50	11.58	#N/A	31	#N/A
6	3	A	B	62.50	11.58	#N/A	31	#N/A
6	3	B	C	62.50	11.58	#N/A	31	#N/A
6	3	C	D	62.50	11.58	#N/A	31	#N/A
6	4	A	B	62.50	11.58	#N/A	31	#N/A
6	4	B	C	62.50	11.58	#N/A	31	#N/A
6	4	C	D	62.50	11.58	#N/A	31	#N/A
7	1	A	B	62.50	11.58	47	31	100%
7	1	B	C	62.50	11.58	47	31	100%
7	1	C	D	62.50	11.58	42	31	100%
7	2	A	B	62.50	34.83	22	31	70%
7	2	B	C	62.50	34.83	23	31	75%
7	2	C	D	62.50	34.83	27	31	85%
7	3	A	B	62.50	34.83	15	31	50%
7	3	B	C	62.50	34.83	16	31	50%
7	3	C	D	62.50	34.83	15	31	50%



CRACKING INTENSITY ~ BRIDGE 16/7S-E

100% = CRACK EVERY 2 FT.

XXX = CRACKS NOT COUNTED DUE TO LIMITED ACCESS

SPANS 3, 4 AND 5 NOT SHOWN FOR CLARITY

LESS CRACKING

MORE CRACKING

BRIDGE NUMBER	303/4A
BRIDGE NAME	MANETTE BRIDGE
INSPECTION DATE	5/29/2015
DECK CONCRETE	TRADITIONAL

BRIDGE 90/106N (GOLD CREEK WB)

Bridge #	90/106N	Bridge Name	Gold Creek WB		Structure ID	0017852D	
Contract #	7852	Region	SC	Project Engineer	Will Smith	Performance Deck Concrete?	No
Contractor	Max J. Kuney Company		Concrete Supplier		Deck Placement		≈ 2012
Bridge Description	6-Span (155' / 155' / 155' / 155' / 155' / 155'), 7-WF74G Girders (930' bridge length), 3-Lanes (56' wide roadway)						



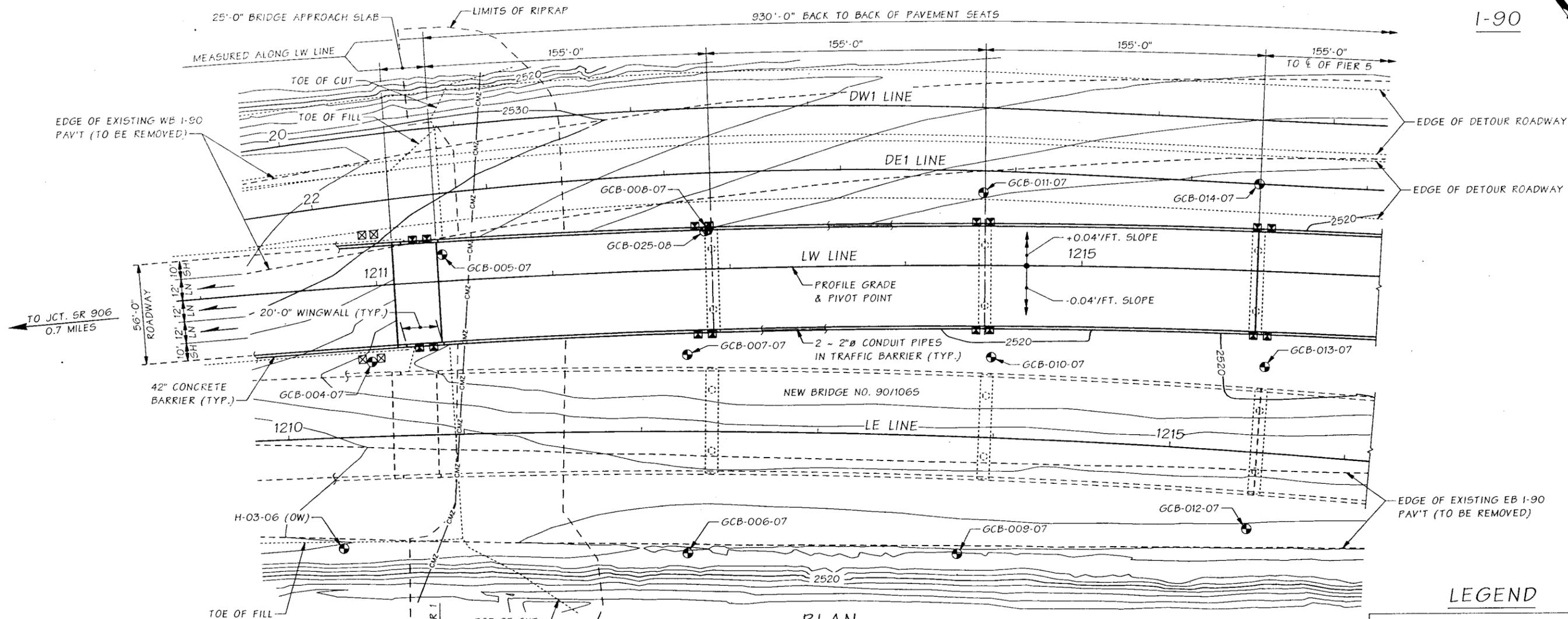
CONTENTS

1. Layout Plan Sheet
2. Field Notes
3. Crack Summary
4. Crack Intensity Diagram

SEC. 15, T.22N., R.11E., W.M.
KITTITAS COUNTY

I-90

LW LINE CURVE DATA					
P.I. STA.	Δ	RADIUS	TANGENT	LENGTH	BACK TANGENT BEARING
1214+45.27	16°38'51" RT.	4665.00'	769.19'	1524.76'	S 61°50'12" E

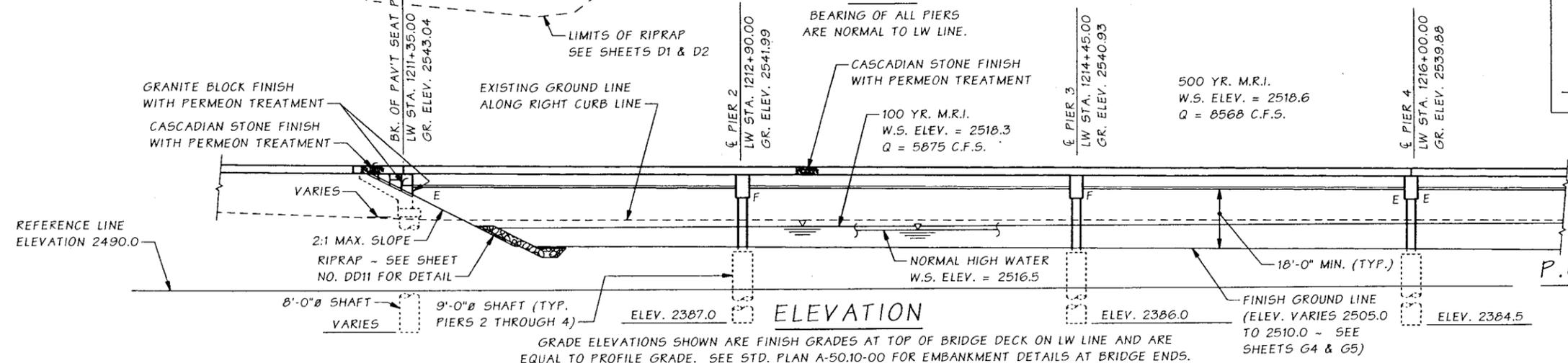


PLAN

BEARING OF ALL PIERS ARE NORMAL TO LW LINE.

LEGEND

- ⊕ SOIL BORING LOCATIONS
- ⊠ JUNCTION BOX NEMA 4X 5.5.
- ⊞ JUNCTION BOX (TYP.)
- CMZ- LIMIT OF CHANNEL MIGRATION ZONE



ELEVATION

GRADE ELEVATIONS SHOWN ARE FINISH GRADES AT TOP OF BRIDGE DECK ON LW LINE AND ARE EQUAL TO PROFILE GRADE. SEE STD. PLAN A-50.10-00 FOR EMBANKMENT DETAILS AT BRIDGE ENDS.

DATUM
NAVD 88

P.C. GIRDERS (WF74G)
CONT. FOR L.L.
LOADING: HL-93

SR 90 FILE NO. 7258 SHEET 801

Bridge Design Engr.	Khaileghi, B	M:\X-Team\I-90 HYAK - SS VIC\BR 90-106N\window files\001 LAYOUT 1.WND
Supervisor	Stoddard, RB	
Designed By	Chu, A	11/08
Checked By	JB/RC/PRG/PMN	10/09
Detailed By	McCarthy, DJ	09/09
Bridge Projects Engr.	Lewis, RA	08/08
Prelim. Plan By	Wei, J	06/08
Architect/Specialist	PDK, BSA, GAW	08/08
DATE	REVISION	BY APP'D

REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
10	WASH.			
JOB NUMBER				
C9Y019				

BRIDGE AND STRUCTURES OFFICE

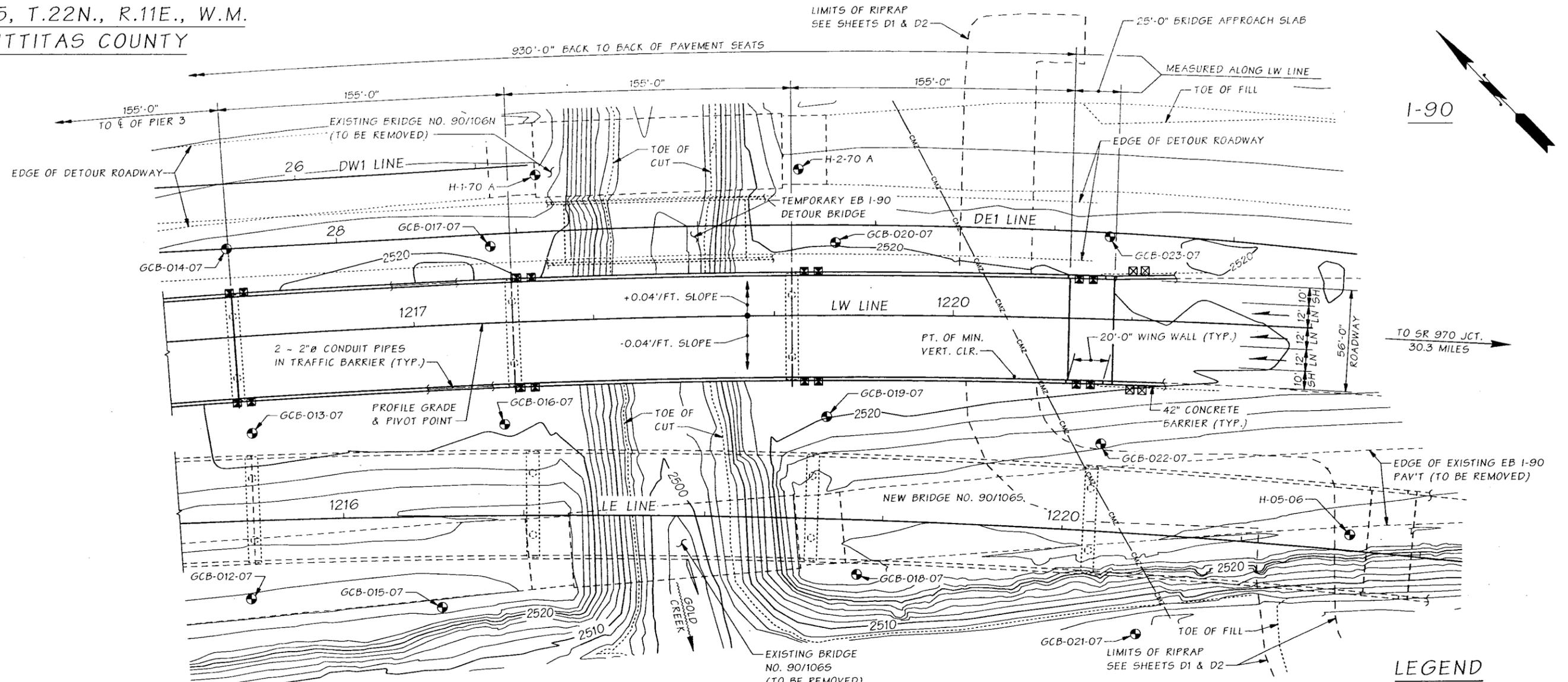


I-90
HYAK TO SNOWSHED VICINITY PHASE 1B -
ADD LANES AND BRIDGES
GOLD CR BR. NO. 90/106N REPLACEMENT
LAYOUT 1 OF 2

BRIDGE SHEET NO.	BD1
SHEET	622
OF	808
SHEETS	

C.S. 190115 ~ PROJ. NO. XL2779F ~ SOUTH CENTRAL REGION ~ I-90 ~ MP 55.37 TO MP 55.55 ~ GOLD CR BR. NO. 90/106N REPLACEMENT

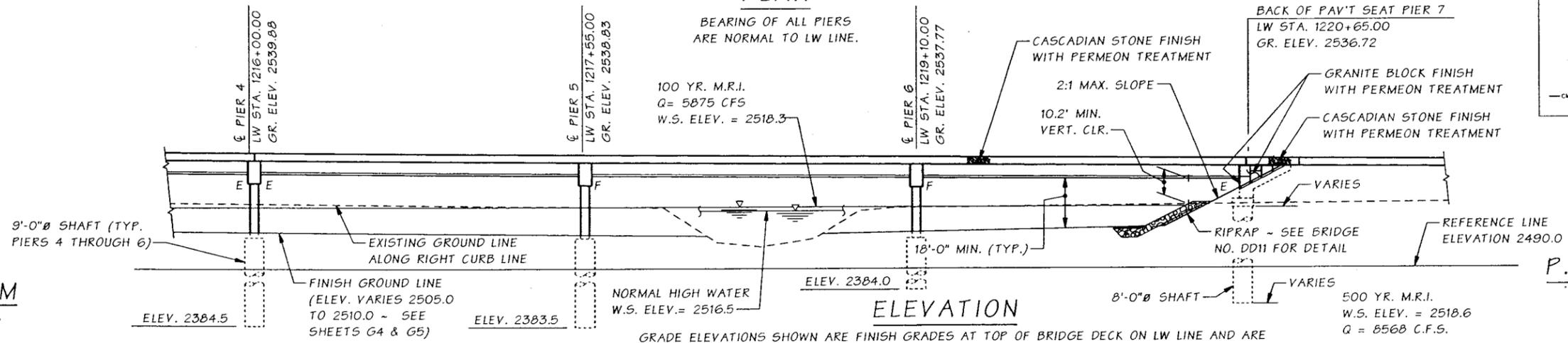
SEC. 15, T.22N., R.11E., W.M.
KITTITAS COUNTY



PLAN

BEARING OF ALL PIERS ARE NORMAL TO LW LINE.

100 YR. M.R.I.
Q = 5875 CFS
W.S. ELEV. = 2518.3



ELEVATION

GRADE ELEVATIONS SHOWN ARE FINISH GRADES AT TOP OF BRIDGE DECK ON LW LINE AND ARE EQUAL TO PROFILE GRADE. SEE STD. PLAN A-50.10-00 FOR EMBANKMENT DETAILS AT BRIDGE ENDS.

LEGEND

- SOIL BORING LOCATIONS
- ⊠ JUNCTION BOX NEMA 4X S.S.
- ⊠ JUNCTION BOX (TYP.)
- CMZ — LIMIT OF CHANNEL MIGRATION ZONE

DATUM
NAVD 88

P.C. GIRDERS (WF74G)
CONT. FOR L.L.
LOADING: HL-93

SR 90 FILE NO. 7258 SHEET 802

Bridge Design Engr.	khaleghi, B	M:\X-Team\I-90 HYAK - SS VIC\BR 90-106N\window files\002 LAYOUT 2.WND
Supervisor	Stoddard, RB	
Designed By	Chu, A	11/08
Checked By	JB/RC/PRG/PMN	10/09
Detailed By	McCarthy, DJ	09/09
Bridge Projects Engr.	Lewis, RA	06/08
Prelim. Plan By	Wei, J	08/08
Architect/Specialist	PDK, BSA, GAW	08/08
DATE	REVISION	BY APP'D

BRIDGE AND STRUCTURES OFFICE

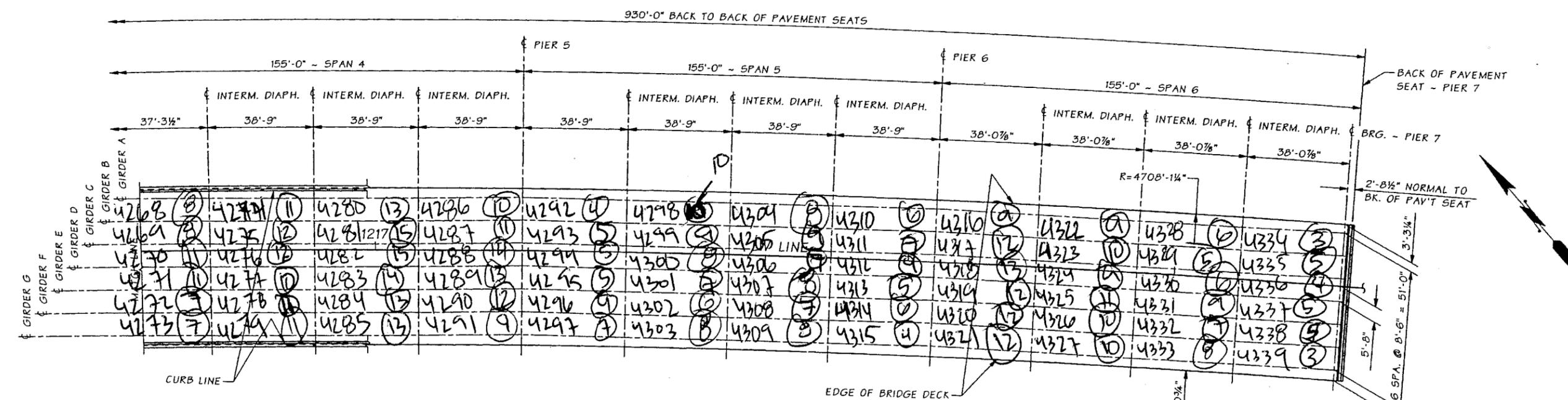
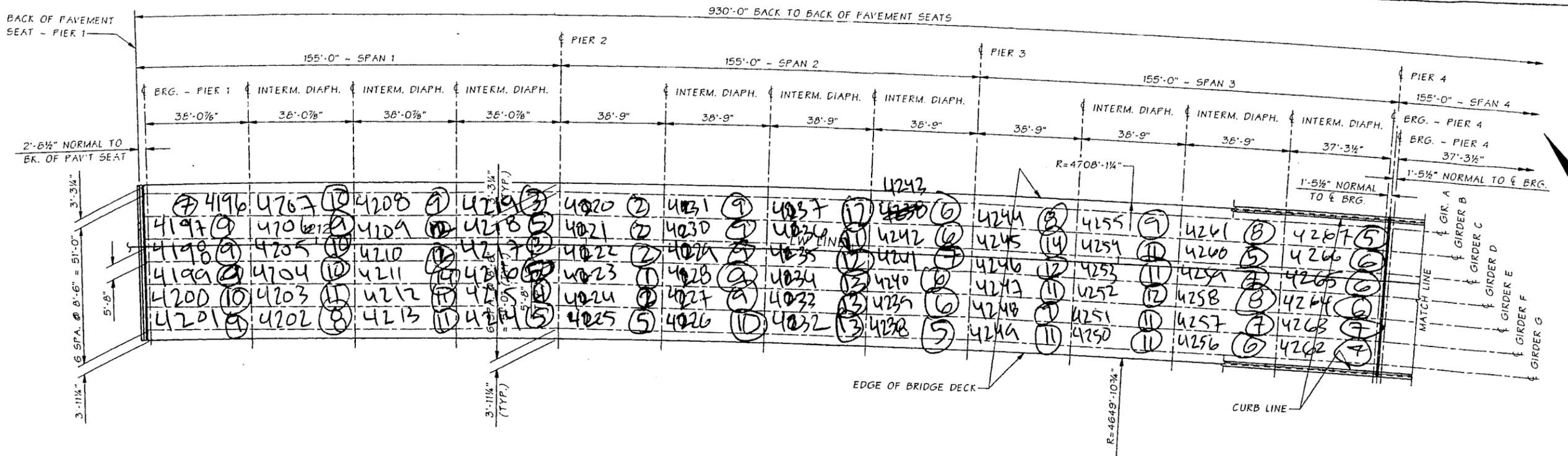
10/19/09

BRILLIAN KHALEGI
PROFESSIONAL ENGINEER



I-90	BRIDGE SHEET NO.
HYAK TO SNOWSHED VICINITY PHASE 1B - ADD LANES AND BRIDGES	BD2
GOLD CR BR. NO. 90/106N REPLACEMENT	SHEET 623
LAYOUT 2 OF 2	OF 808
	SHEETS

PROJ. NO. XL2779F ~ SOUTH CENTRAL REGION ~ I-90 ~ MP 55.37 TO MP 55.55 ~ GOLD CR BR. NO. 90/106N REPLACEMENT



FRAMING PLAN

ALL LONGITUDINAL DIMENSIONS ARE ALONG LW LINE UNLESS OTHERWISE SHOWN.

SR 90 FILE NO. 7258 SHEET 8028

Bridge Design Engr.	Khaleghi, B	M:\X-Team\I-90 HYAK - SS VZ\BR 90-106\Window files\FRAMING PLAN.WND
Supervisor	Stoddard, RB	
Designed By	Chu, A	11/08
Checked By	PMN/PRG	10/09
Detailed By	McCarthy, DJ	09/09
Bridge Projects Engr.		
Preim. Plan By		
Architect/Specialist		
DATE	REVISION	BY APPD



BRIDGE AND STRUCTURES OFFICE



I-90
HYAK TO SNOWSHED VICINITY PHASE 1B -
ADD LANES AND BRIDGES
GOLD CR BR. NO. 90/106N REPLACEMENT

BRIDGE SHEET NO.
BD28
SHEET
649
OF
808
SHEETS

FRAMING PLAN



Bridge #	90/106N	Bridge Name	Gold Creek WB			Structure ID	0017852D	
Contract #	7852	Region	SC	Project Engineer	Will Smith	Performance Deck Concrete?	No	
Contractor	Max J. Kuney Company		Concrete Supplier			Deck Placement	≈ 2012	
Bridge Description	6-Span (155' / 155' / 155' / 155' / 155' / 155'), 7-WF74G Girders (930' bridge length), 3-Lanes (56' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr} / N_{100} (rounded to the nearest 5%)

Avg. =	44%
Min. =	5%
Max. =	80%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	38.07	8.50	7	19	35%
1	1	B	C	38.07	8.50	9	19	45%
1	1	C	D	38.07	8.50	9	19	45%
1	1	D	E	38.07	8.50	9	19	45%
1	1	E	F	38.07	8.50	10	19	55%
1	1	F	G	38.07	8.50	9	19	45%
1	2	A	B	38.07	8.50	10	19	55%
1	2	B	C	38.07	8.50	9	19	45%
1	2	C	D	38.07	8.50	10	19	55%
1	2	D	E	38.07	8.50	10	19	55%
1	2	E	F	38.07	8.50	11	19	60%
1	2	F	G	38.07	8.50	8	19	40%
1	3	A	B	38.07	8.50	9	19	45%
1	3	B	C	38.07	8.50	12	19	65%
1	3	C	D	38.07	8.50	12	19	65%
1	3	D	E	38.07	8.50	14	19	75%
1	3	E	F	38.07	8.50	11	19	60%
1	3	F	G	38.07	8.50	11	19	60%
1	4	A	B	38.07	8.50	3	19	15%
1	4	B	C	38.07	8.50	5	19	25%
1	4	C	D	38.07	8.50	3	19	15%
1	4	D	E	38.07	8.50	5	19	25%
1	4	E	F	38.07	8.50	4	19	20%
1	4	F	G	38.07	8.50	5	19	25%
2	1	A	B	38.75	8.50	2	19	10%
2	1	B	C	38.75	8.50	2	19	10%
2	1	C	D	38.75	8.50	2	19	10%
2	1	D	E	38.75	8.50	1	19	5%
2	1	E	F	38.75	8.50	2	19	10%
2	1	F	G	38.75	8.50	5	19	25%
2	2	A	B	38.75	8.50	9	19	45%
2	2	B	C	38.75	8.50	9	19	45%
2	2	C	D	38.75	8.50	9	19	45%
2	2	D	E	38.75	8.50	9	19	45%
2	2	E	F	38.75	8.50	9	19	45%
2	2	F	G	38.75	8.50	10	19	55%
2	3	A	B	38.75	8.50	12	19	65%
2	3	B	C	38.75	8.50	11	19	60%
2	3	C	D	38.75	8.50	12	19	65%
2	3	D	E	38.75	8.50	13	19	70%
2	3	E	F	38.75	8.50	13	19	70%



Bridge #	90/106N	Bridge Name	Gold Creek WB			Structure ID	0017852D	
Contract #	7852	Region	SC	Project Engineer	Will Smith	Performance Deck Concrete?	No	
Contractor	Max J. Kuney Company		Concrete Supplier			Deck Placement	≈ 2012	
Bridge Description	6-Span (155' / 155' / 155' / 155' / 155' / 155'), 7-WF74G Girders (930' bridge length), 3-Lanes (56' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr} / N_{100} (rounded to the nearest 5%)

Avg. =	44%
Min. =	5%
Max. =	80%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
2	3	F	G	38.75	8.50	13	19	70%
2	4	A	B	38.75	8.50	6	19	30%
2	4	B	C	38.75	8.50	6	19	30%
2	4	C	D	38.75	8.50	7	19	35%
2	4	D	E	38.75	8.50	6	19	30%
2	4	E	F	38.75	8.50	6	19	30%
2	4	F	G	38.75	8.50	5	19	25%
3	1	A	B	38.75	8.50	8	19	40%
3	1	B	C	38.75	8.50	14	19	75%
3	1	C	D	38.75	8.50	12	19	65%
3	1	D	E	38.75	8.50	11	19	60%
3	1	E	F	38.75	8.50	9	19	45%
3	1	F	G	38.75	8.50	11	19	60%
3	2	A	B	38.75	8.50	9	19	45%
3	2	B	C	38.75	8.50	11	19	60%
3	2	C	D	38.75	8.50	11	19	60%
3	2	D	E	38.75	8.50	12	19	65%
3	2	E	F	38.75	8.50	11	19	60%
3	2	F	G	38.75	8.50	11	19	60%
3	3	A	B	38.75	8.50	8	19	40%
3	3	B	C	38.75	8.50	5	19	25%
3	3	C	D	38.75	8.50	7	19	35%
3	3	D	E	38.75	8.50	8	19	40%
3	3	E	F	38.75	8.50	7	19	35%
3	3	F	G	38.75	8.50	6	19	30%
3	4	A	B	38.75	8.50	5	19	25%
3	4	B	C	38.75	8.50	6	19	30%
3	4	C	D	38.75	8.50	6	19	30%
3	4	D	E	38.75	8.50	6	19	30%
3	4	E	F	38.75	8.50	7	19	35%
3	4	F	G	38.75	8.50	7	19	35%
4	1	A	B	38.75	8.50	8	19	40%
4	1	B	C	38.75	8.50	8	19	40%
4	1	C	D	38.75	8.50	11	19	60%
4	1	D	E	38.75	8.50	11	19	60%
4	1	E	F	38.75	8.50	7	19	35%
4	1	F	G	38.75	8.50	7	19	35%
4	2	A	B	38.75	8.50	11	19	60%
4	2	B	C	38.75	8.50	12	19	65%
4	2	C	D	38.75	8.50	12	19	65%
4	2	D	E	38.75	8.50	10	19	55%



Bridge #	90/106N	Bridge Name	Gold Creek WB			Structure ID	0017852D	
Contract #	7852	Region	SC	Project Engineer	Will Smith	Performance Deck Concrete?	No	
Contractor	Max J. Kuney Company		Concrete Supplier			Deck Placement	≈ 2012	
Bridge Description	6-Span (155' / 155' / 155' / 155' / 155' / 155'), 7-WF74G Girders (930' bridge length), 3-Lanes (56' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	44%
Min. =	5%
Max. =	80%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
4	2	E	F	38.75	8.50	11	19	60%
4	2	F	G	38.75	8.50	11	19	60%
4	3	A	B	38.75	8.50	13	19	70%
4	3	B	C	38.75	8.50	15	19	80%
4	3	C	D	38.75	8.50	15	19	80%
4	3	D	E	38.75	8.50	14	19	75%
4	3	E	F	38.75	8.50	13	19	70%
4	3	F	G	38.75	8.50	13	19	70%
4	4	A	B	38.75	8.50	10	19	55%
4	4	B	C	38.75	8.50	11	19	60%
4	4	C	D	38.75	8.50	14	19	75%
4	4	D	E	38.75	8.50	13	19	70%
4	4	E	F	38.75	8.50	12	19	65%
4	4	F	G	38.75	8.50	9	19	45%
5	1	A	B	38.75	8.50	4	19	20%
5	1	B	C	38.75	8.50	5	19	25%
5	1	C	D	38.75	8.50	5	19	25%
5	1	D	E	38.75	8.50	5	19	25%
5	1	E	F	38.75	8.50	4	19	20%
5	1	F	G	38.75	8.50	7	19	35%
5	2	A	B	38.75	8.50	10	19	55%
5	2	B	C	38.75	8.50	9	19	45%
5	2	C	D	38.75	8.50	8	19	40%
5	2	D	E	38.75	8.50	7	19	35%
5	2	E	F	38.75	8.50	6	19	30%
5	2	F	G	38.75	8.50	8	19	40%
5	3	A	B	38.75	8.50	8	19	40%
5	3	B	C	38.75	8.50	9	19	45%
5	3	C	D	38.75	8.50	7	19	35%
5	3	D	E	38.75	8.50	8	19	40%
5	3	E	F	38.75	8.50	7	19	35%
5	3	F	G	38.75	8.50	8	19	40%
5	4	A	B	38.75	8.50	6	19	30%
5	4	B	C	38.75	8.50	7	19	35%
5	4	C	D	38.75	8.50	9	19	45%
5	4	D	E	38.75	8.50	5	19	25%
5	4	E	F	38.75	8.50	6	19	30%
5	4	F	G	38.75	8.50	4	19	20%
6	1	A	B	38.07	8.50	9	19	45%
6	1	B	C	38.07	8.50	12	19	65%
6	1	C	D	38.07	8.50	13	19	70%



Bridge #	90/106N	Bridge Name	Gold Creek WB			Structure ID	0017852D	
Contract #	7852	Region	SC	Project Engineer	Will Smith	Performance Deck Concrete?	No	
Contractor	Max J. Kuney Company		Concrete Supplier				Deck Placement	≈ 2012
Bridge Description	6-Span (155' / 155' / 155' / 155' / 155' / 155'), 7-WF74G Girders (930' bridge length), 3-Lanes (56' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

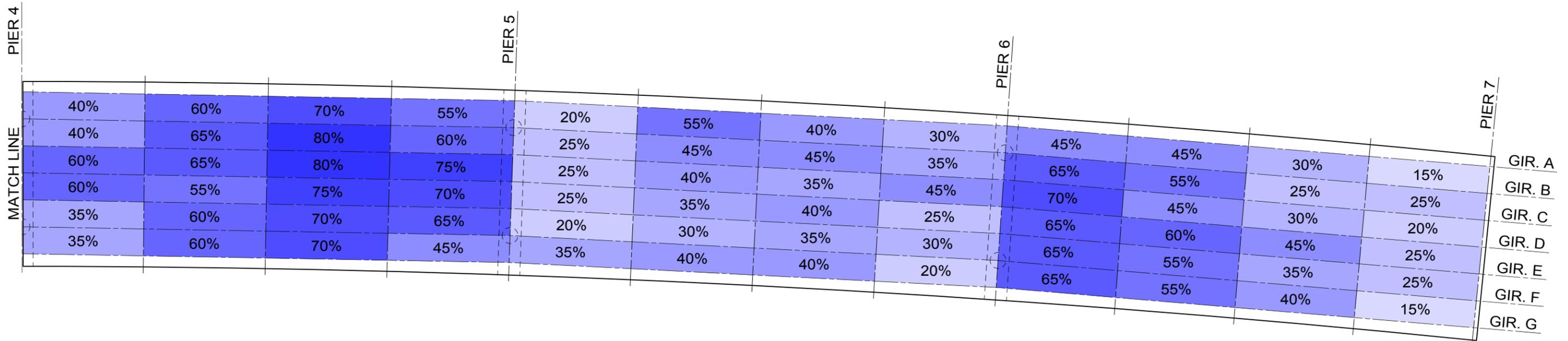
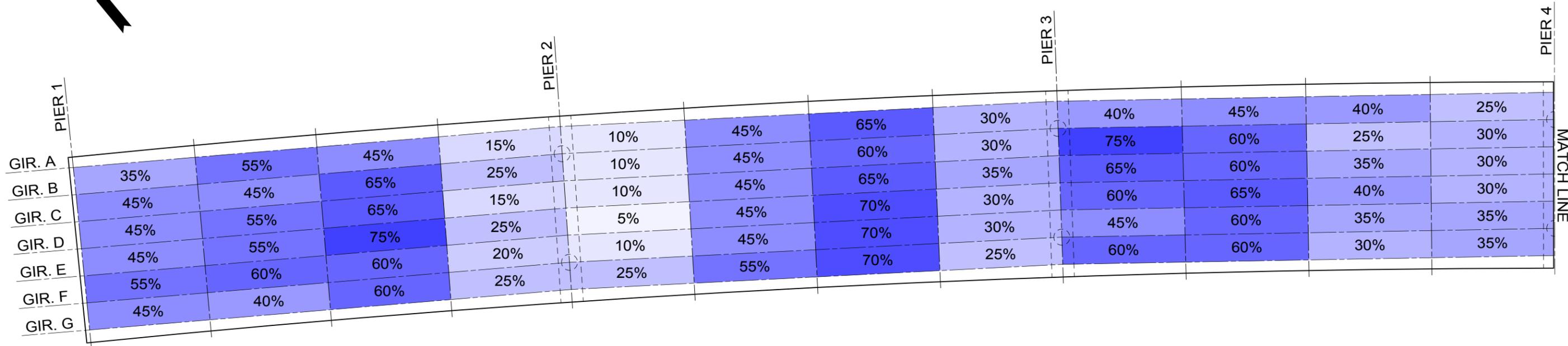
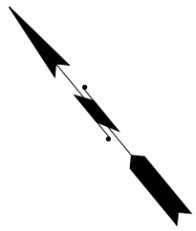
N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	44%
Min. =	5%
Max. =	80%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
6	1	D	E	38.07	8.50	12	19	65%
6	1	E	F	38.07	8.50	12	19	65%
6	1	F	G	38.07	8.50	12	19	65%
6	2	A	B	38.07	8.50	9	19	45%
6	2	B	C	38.07	8.50	10	19	55%
6	2	C	D	38.07	8.50	9	19	45%
6	2	D	E	38.07	8.50	11	19	60%
6	2	E	F	38.07	8.50	10	19	55%
6	2	F	G	38.07	8.50	10	19	55%
6	3	A	B	38.07	8.50	6	19	30%
6	3	B	C	38.07	8.50	5	19	25%
6	3	C	D	38.07	8.50	6	19	30%
6	3	D	E	38.07	8.50	9	19	45%
6	3	E	F	38.07	8.50	7	19	35%
6	3	F	G	38.07	8.50	8	19	40%
6	4	A	B	38.07	8.50	3	19	15%
6	4	B	C	38.07	8.50	5	19	25%
6	4	C	D	38.07	8.50	4	19	20%
6	4	D	E	38.07	8.50	5	19	25%
6	4	E	F	38.07	8.50	5	19	25%
6	4	F	G	38.07	8.50	3	19	15%



CRACKING INTENSITY ~ BRIDGE 90/106N

100% = CRACK EVERY 2 FT.

LESS CRACKING

MORE CRACKING



BRIDGE NUMBER	90/106N
BRIDGE NAME	GOLD CREEK WB
INSPECTION DATE	5/20/2015
DECK CONCRETE	TRADITIONAL

6/115 (SOUTH FORK CHEHALIS RIVER)

Bridge #	6/115	Bridge Name	South Fork Chehalis River		Structure ID	0017587A	
Contract #	7587	Region	SW	Project Engineer	Collin Newell	Performance Deck Concrete?	No
Contractor	Scarsella Bros.		Concrete Supplier	Unknown		Deck Placement	≈ 2009
Bridge Description	5-Span (160' / 160' / 160' / 142.5' / 142.5'), 5-WF74G Girders (765' bridge length), 2-Lanes (40' wide roadway)						



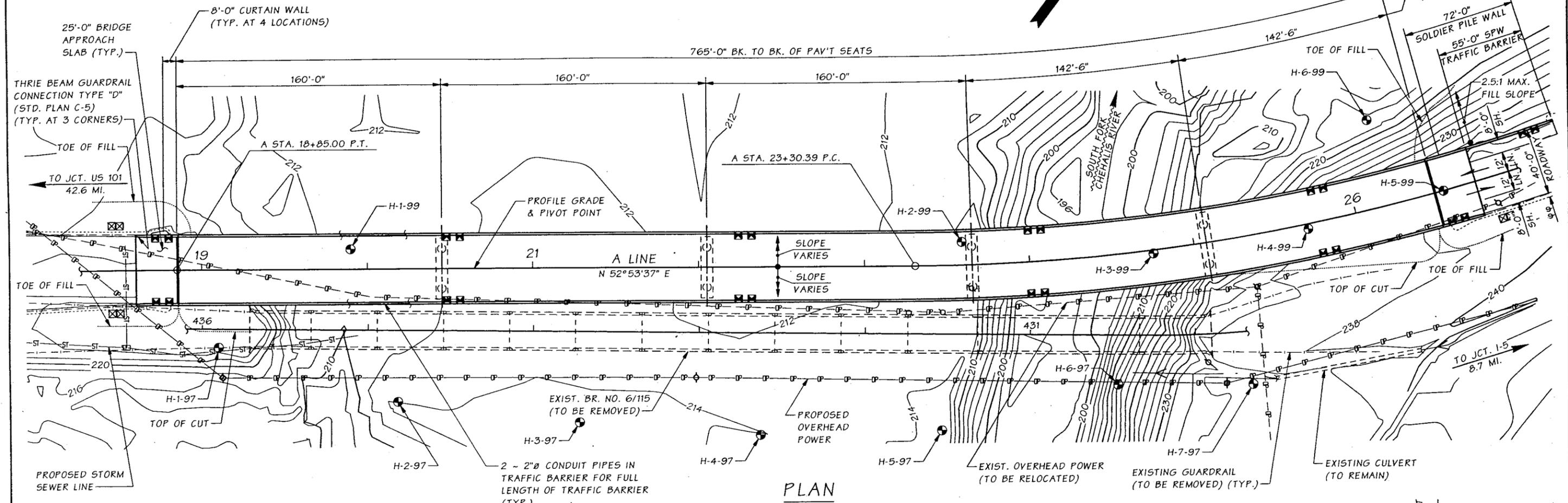
CONTENTS

1. Layout Plan Sheet
2. Field Notes
3. Crack Summary
4. Crack Intensity Diagram

A LINE CURVE DATA					
P.I. STATION	Δ	RADIUS	TANGENT	LENGTH	BK. TANGENT BRG.
A STA. 27+35.93	36°57'15" LT.	1213.65'	405.54'	782.77'	N 52°53'37" E
A STA. 16+25.04	2°33'07" RT.	11675.00'	260.04'	520.00'	N 50°20'30" E

SEC. 24, T. 13 N., R. 4 W., W.M.
LEWIS COUNTY

SR 6



PLAN

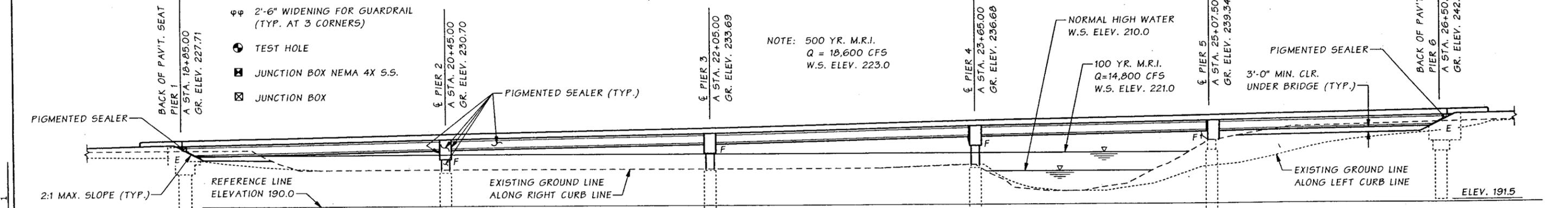
BEARINGS OF ALL PIERS ARE NORMAL TO THE A LINE.

LEGEND

- ◊◊ 2'-6" WIDENING FOR GUARDRAIL (TYP. AT 3 CORNERS)
- ⊙ TEST HOLE
- ⊠ JUNCTION BOX NEMA 4X 5.5.
- ⊞ JUNCTION BOX

NOTE: 500 YR. M.R.I.
Q = 18,600 CFS
W.S. ELEV. 223.0

100 YR. M.R.I.
Q = 14,800 CFS
W.S. ELEV. 221.0



ELEVATION

GRADE ELEVATIONS SHOWN ARE FINISH GRADES AT TOP OF ROADWAY SLAB ON THE A LINE AND ARE EQUAL TO PROFILE GRADE.

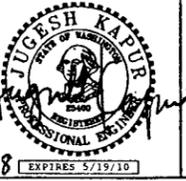
P.C. GIRDERS (WF74G)
CONT. FOR LL
LOADING: HL-93

DATUM
NGVD 1929

Bridge Design Engr.	Khaleghi, B	M:\X-Team\S FORK CHEHALIS R\window files\LAYOUT.WND
Supervisor	Anderson, MW	
Designed By	AAB/SLL/PRG	05/07
Checked By	AAB/SLL/PRG	03/08
Detailed By	McCarthy, DJ	10/07
Bridge Projects Engr.	Lewis, RA	05/07
Prelim. Plan By	Bushnaq, AA	05/07
Architect/Specialist	PDK/BK/GAW	05/07

REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
10	WASH.			
JOB NUMBER				
06X309				

BRIDGE AND STRUCTURES OFFICE



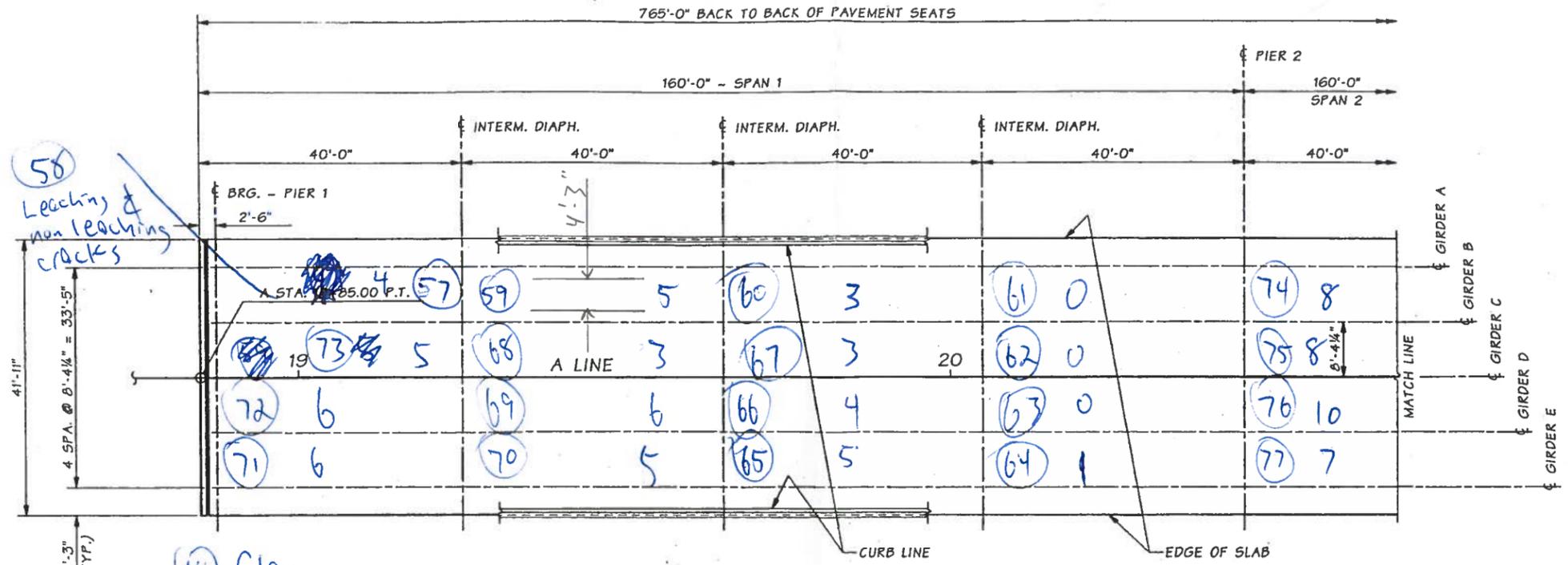
Washington State Department of Transportation

SR 6
SO. FORK CHEHALIS RIVER BRIDGE
SOUTH FORK CHEHALIS RIVER BR. 6/115 REPLACEMENT
LAYOUT

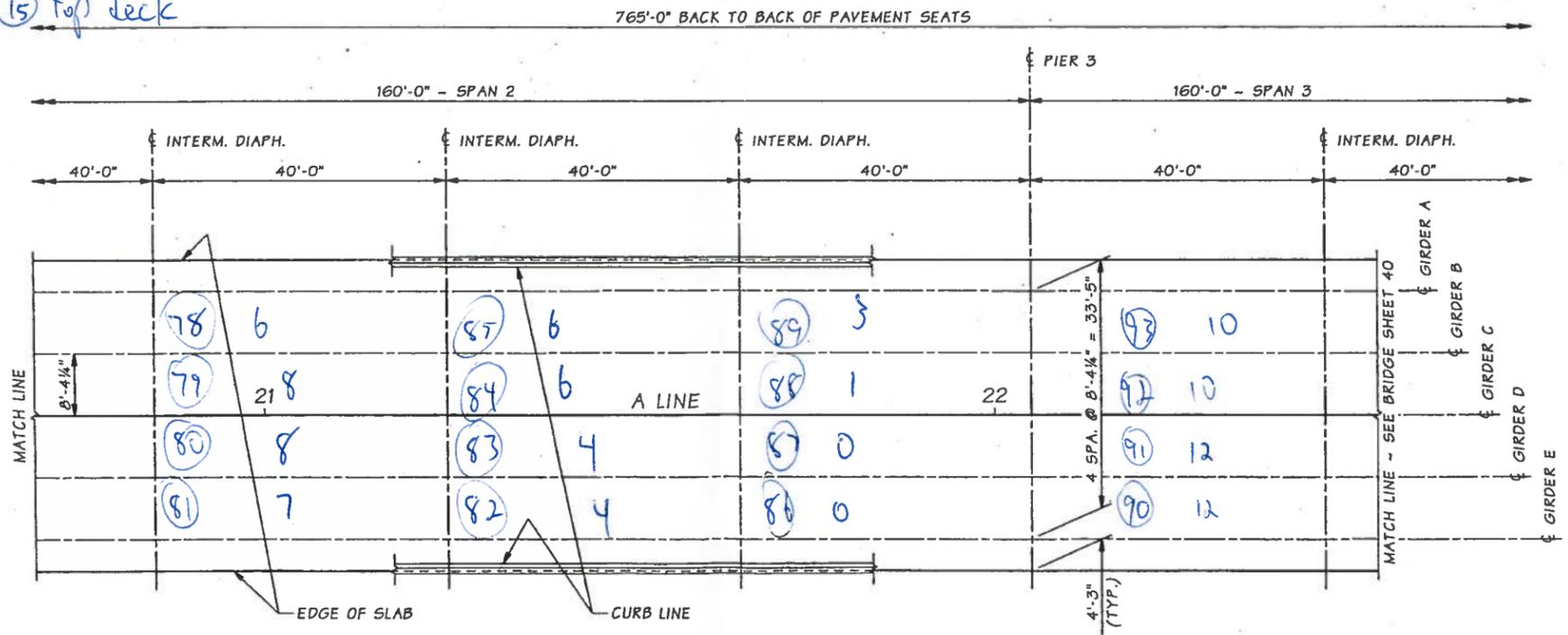
BRIDGE SHEET NO.	1
SHEET OF	61
SHEETS	149

SR 6 JOB NO. 7003 SHEET 1

C.S. 2105 ~ PROJ. NO. 010911 ~ SOUTHWEST REGION ~ M.P. 42.48 TO M.P. 42.91 ~ SR 6 ~ SOUTH FORK CHEHALIS RIVER BR. NO. 6/115 REPL.



(14) Elev
(15) Top Deck



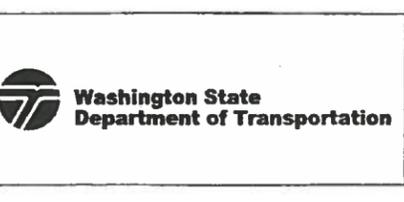
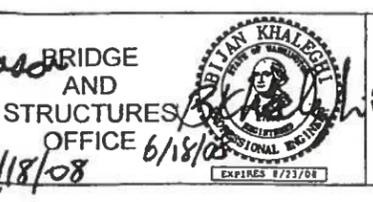
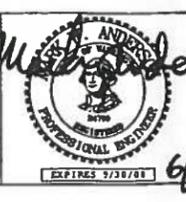
FRAMING PLAN SPANS 1 THROUGH PARTIAL SPAN 3

ALL DIMENSIONS ARE NORMAL TO OR ALONG THE A LINE, & BEARING & PIER UNLESS OTHERWISE SHOWN. BEARING OF ALL PIERS IS NORMAL TO THE A LINE.

JOB NO. 7003 SHEET 39

Bridge Design Engr.	Khaleghi, B	M:\X-Team\5 FORK CHEHALIS R\window files\FRAMING PLAN 1.WND
Supervisor	Anderson, MW	
Designed By	Lowry, S	05/07
Checked By	Bushnaq, AA	03/08
Detailed By	McCarthy, DJ	05/07
Bridge Projects Engr.		
Preim. Plan By		
Architect/Specialist		
DATE	REVISION	BY APPD

REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
10	WASH.			
JOB NUMBER 06X309				



SR 6
SO. FORK
CHEHALIS RIVER BRIDGE
SOUTH FORK CHEHALIS RIVER BR. 6/115 REPLACEMENT
FRAMING PLAN 1 OF 2

BRIDGE SHEET NO. 39
SHEET 99 of 149 SHEETS



Bridge #	6/115	Bridge Name	South Fork Chehalis River			Structure ID	0017587A	
Contract #	7587	Region	SW	Project Engineer	Collin Newell	Performance Deck Concrete?	No	
Contractor	Scarsella Bros.		Concrete Supplier			Deck Placement	≈ 2009	
Bridge Description	5-Span (160' / 160' / 160' / 142.5' / 142.5'), 5-WF74G Girders (765' bridge length), 2-Lanes (40' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	32%
Min. =	0%
Max. =	65%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	40.00	8.35	4	20	20%
1	1	B	C	40.00	8.35	5	20	25%
1	1	C	D	40.00	8.35	6	20	30%
1	1	D	E	40.00	8.35	6	20	30%
1	2	A	B	40.00	8.35	5	20	25%
1	2	B	C	40.00	8.35	3	20	15%
1	2	C	D	40.00	8.35	6	20	30%
1	2	D	E	40.00	8.35	5	20	25%
1	3	A	B	40.00	8.35	3	20	15%
1	3	B	C	40.00	8.35	3	20	15%
1	3	C	D	40.00	8.35	4	20	20%
1	3	D	E	40.00	8.35	5	20	25%
1	4	A	B	40.00	8.35	0	20	0%
1	4	B	C	40.00	8.35	0	20	0%
1	4	C	D	40.00	8.35	0	20	0%
1	4	D	E	40.00	8.35	1	20	5%
2	1	A	B	40.00	8.35	8	20	40%
2	1	B	C	40.00	8.35	8	20	40%
2	1	C	D	40.00	8.35	10	20	50%
2	1	D	E	40.00	8.35	7	20	35%
2	2	A	B	40.00	8.35	6	20	30%
2	2	B	C	40.00	8.35	8	20	40%
2	2	C	D	40.00	8.35	8	20	40%
2	2	D	E	40.00	8.35	7	20	35%
2	3	A	B	40.00	8.35	6	20	30%
2	3	B	C	40.00	8.35	6	20	30%
2	3	C	D	40.00	8.35	4	20	20%
2	3	D	E	40.00	8.35	4	20	20%
2	4	A	B	40.00	8.35	3	20	15%
2	4	B	C	40.00	8.35	1	20	5%
2	4	C	D	40.00	8.35	0	20	0%
2	4	D	E	40.00	8.35	0	20	0%
3	1	A	B	40.00	8.35	10	20	50%
3	1	B	C	40.00	8.35	10	20	50%
3	1	C	D	40.00	8.35	12	20	60%
3	1	D	E	40.00	8.35	12	20	60%
3	2	A	B	40.00	8.35	10	20	50%
3	2	B	C	40.00	8.35	11	20	55%
3	2	C	D	40.00	8.35	13	20	65%
3	2	D	E	40.00	8.35	12	20	60%
3	3	A	B	40.00	8.35	11	20	55%



Bridge #	6/115	Bridge Name	South Fork Chehalis River			Structure ID	0017587A	
Contract #	7587	Region	SW	Project Engineer	Collin Newell	Performance Deck Concrete?	No	
Contractor	Scarsella Bros.		Concrete Supplier			Deck Placement	≈ 2009	
Bridge Description	5-Span (160' / 160' / 160' / 142.5' / 142.5'), 5-WF74G Girders (765' bridge length), 2-Lanes (40' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

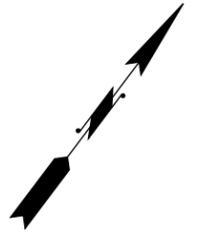
N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr} / N_{100} (rounded to the nearest 5%)

Avg. =	32%
Min. =	0%
Max. =	65%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
3	3	B	C	40.00	8.35	13	20	65%
3	3	C	D	40.00	8.35	12	20	60%
3	3	D	E	40.00	8.35	12	20	60%
3	4	A	B	40.00	8.35	4	20	20%
3	4	B	C	40.00	8.35	9	20	45%
3	4	C	D	40.00	8.35	11	20	55%
3	4	D	E	40.00	8.35	10	20	50%
4	1	A	B	35.63	8.35	3	18	15%
4	1	B	C	35.63	8.35	2	18	10%
4	1	C	D	35.63	8.35	2	18	10%
4	1	D	E	35.63	8.35	2	18	10%
4	2	A	B	35.63	8.35	8	18	45%
4	2	B	C	35.63	8.35	7	18	40%
4	2	C	D	35.63	8.35	7	18	40%
4	2	D	E	35.63	8.35	7	18	40%
4	3	A	B	35.63	8.35	7	18	40%
4	3	B	C	35.63	8.35	6	18	35%
4	3	C	D	35.63	8.35	5	18	30%
4	3	D	E	35.63	8.35	5	18	30%
4	4	A	B	35.63	8.35	0	18	0%
4	4	B	C	35.63	8.35	0	18	0%
4	4	C	D	35.63	8.35	2	18	10%
4	4	D	E	35.63	8.35	0	18	0%
5	1	A	B	35.63	8.35	4	18	20%
5	1	B	C	35.63	8.35	1	18	5%
5	1	C	D	35.63	8.35	0	18	0%
5	1	D	E	35.63	8.35	2	18	10%
5	2	A	B	35.63	8.35	10	18	55%
5	2	B	C	35.63	8.35	10	18	55%
5	2	C	D	35.63	8.35	10	18	55%
5	2	D	E	35.63	8.35	9	18	50%
5	3	A	B	35.63	8.35	10	18	55%
5	3	B	C	35.63	8.35	9	18	50%
5	3	C	D	35.63	8.35	9	18	50%
5	3	D	E	35.63	8.35	9	18	50%
5	4	A	B	35.63	8.35	9	18	50%
5	4	B	C	35.63	8.35	8	18	45%
5	4	C	D	35.63	8.35	6	18	35%
5	4	D	E	35.63	8.35	6	18	35%



	PIER 1				PIER 2				PIER 3			
GIR. A												
GIR. B	20%	25%	15%	0%		40%	30%	30%	15%		50%	
GIR. C	25%	15%	15%	0%		40%	40%	30%	5%		50%	
GIR. D	30%	30%	20%	0%		50%	40%	20%	0%		60%	
GIR. E	30%	25%	25%	5%		35%	35%	20%	0%		60%	

	PIER 4				PIER 5				PIER 6			
	50%	55%	20%	15%	45%	40%	0%	20%	55%	55%	50%	50%
	55%	65%	45%	10%	40%	35%	0%	5%	55%	50%	45%	45%
	65%	60%	55%	10%	40%	30%	10%	0%	55%	50%	35%	35%
	60%	60%	50%	10%	40%	30%	0%	10%	50%	50%	35%	35%

CRACKING INTENSITY ~ BRIDGE 6/115

100% = CRACK EVERY 2 FT.



BRIDGE NUMBER	6/115
BRIDGE NAME	SOUTH FORK CHEHALIS RIVER
INSPECTION DATE	4/8/2015
DECK CONCRETE	TRADITIONAL

BRIDGE 5/234W (I-5 OVER BLAKESLEE JUNCTION RAILROAD)

Bridge #	5/234W	Bridge Name	I-5 Over Blakeslee Jct RR		Structure ID	0018272C	
Contract #	8272	Region	SW	Project Engineer	Colin Newell	Performance Deck Concrete?	YES
Contractor	Cascade Bridge		Concrete Supplier	Miles Sand & Gravel		Deck Placement	3/25/2013
Bridge Description	3-Span (126' / 110' / 164.5'), 6-WF83G & WF74G Girders (400.5' bridge length), 3-Lanes (58' wide roadway)						



CONTENTS

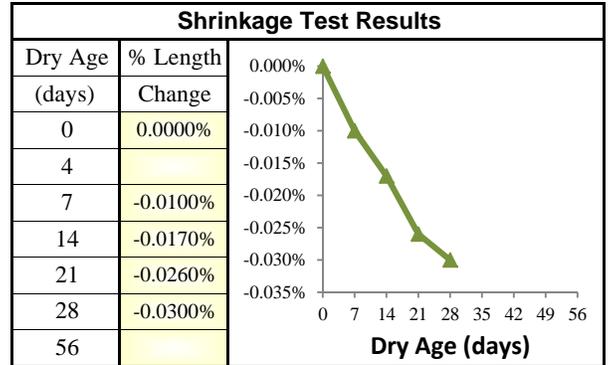
1. Layout Plan Sheet
2. Mix Design Summary
3. Concrete Mix Design Form
4. Concrete Test Results
5. Field Notes
6. Crack Summary
7. Crack Intensity Diagram



Bridge #	5/234W	Bridge Name	I-5 Over Blakeslee Jct RR		Structure ID	0018272C	
Contract #	8272	Region	SW	Project Engineer	Colin Newell	Performance Deck Concrete?	YES
Contractor	Cascade Bridge		Concrete Supplier	Miles Sand & Gravel		Deck Placement	3/25/2013
Bridge Description	3-Span (126' / 110' / 164.5'), 6-WF83G & WF74G Girders (400.5' bridge length), 3-Lanes (58' wide roadway)						

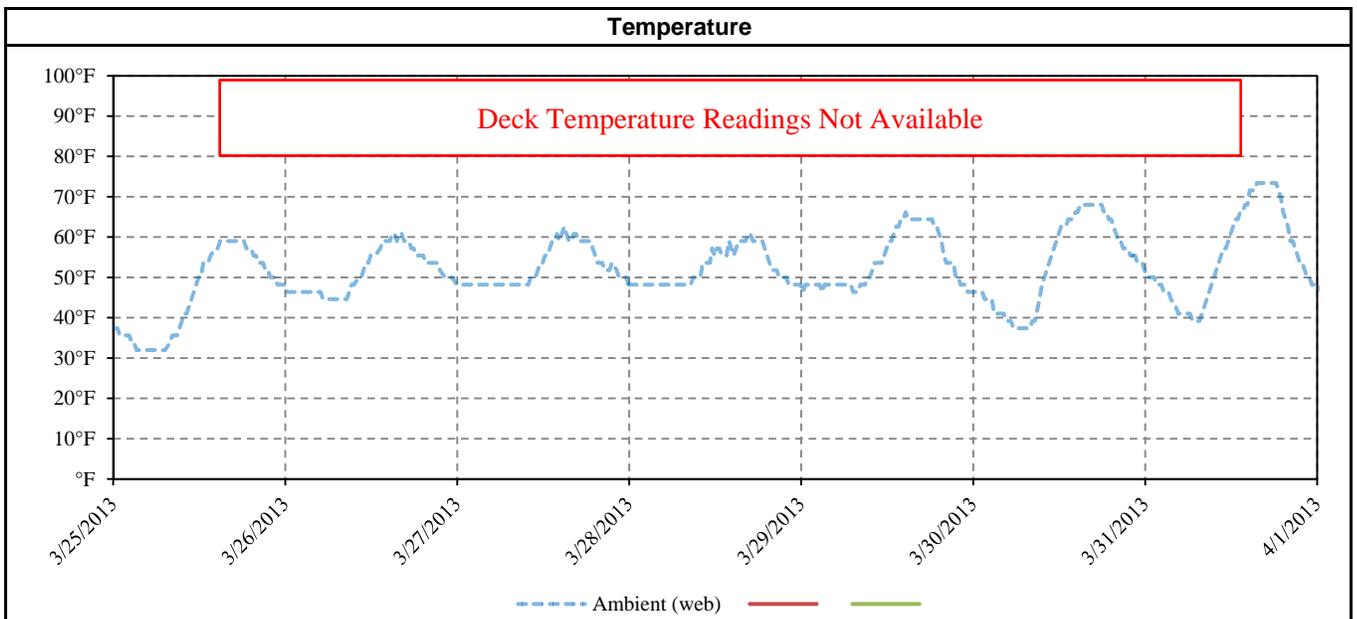
Mix Design (WSDOT Form 350-040)			
Water (max) =		223 lbs/cy	w/c = 0.40 max
Cementitious Materials	Lbs/cy	Source	Type, Class or Grade
cement	464	Lafarge	Type I-II
fly ash	116	Lafarge	Type F
slag			
latex			
microsilica			
Concrete Admixtures	oz/cy	Manufacturer	Product
air entrainment	1-15	BASF	MB-AE-90
water reducer			
HR water reduce	23-40	BASF	Glenium 7500
set retarder			
shrink. reducer	32	BASF	MasterLife SRA

Concrete Test Results		
compressive strength @ 28 days	5,507	psi
modulus of elasticity		psi
permeability @ 56 days	1,350	coulombs
mix design density	145.5	lb/cf



Aggregate					
	Comp. 1	Comp. 2	Comp. 3	Comp. 4	Comp. 5
WSDOT Pit #	B-329	B-329	B-329	B-333	
Grading	No. 4	No. 57	No. 8	Class 2	
% Total	15.4%	33.3%	16.0%	35.3%	
Lbs/cy	480	1040	500	1100	
ASR Mitigation	None Required				

Notes
Same Mix Design as:
* Bridge 5/232NCD
* Bridge 5/232SCD
Very Similar Mix Design as:
* Bridge 5/229



Contractor Cascade Bridge		Submitted By	Date 1-28-2013
Concrete Supplier Miles Sand & Gravel		Plant Location Rochester	
Contract Number 8272	Contract Name Blakeslee Jct to Mellen St		

This mix is to be used in the following Bid Item No(s): 92.18.01, 93.16.01, 94.17.01

Concrete Class: (check one only)
 3000 4000 4000^a 4000^aP 4000W Concrete Overlay Cement Concrete Pavement^d
 Other Shrinkage Reducer

Remarks: _____

Mix Design No. 0444AFL2 Plant No. 222

Cementitious Materials	Source	Type, Class or Grade	Sp. Gr.	Lbs/cy
Cement	Lafarge	I-II	3.15	464
Fly Ash ^a	Lafarge	F	2.54	116
GGBFS (Slag)				
Latex				
Microsilica				

Concrete Admixtures	Manufacturer	Product	Type	Est. Range (oz/cy)
Air Entrainment	BASF	MB-AE-90		1-15
Water Reducer				
High-Range Water Reducer	BASF	Glenium 7500	F	23-40
Set Retarder				
Other Shrinkage Reducer	BASF	MasterLife SRA		32

Water (Maximum) 233 lbs/cy Is any of the water Recycled or Reclaimed? Yes No

Water Cementitious Ratio (Maximum) 0.40 Mix Design Density 145.5 lbs/cf^d

Design Performance	1	2	3	4	5	Average ^f
28 Day Compressive Strength (cylinders) psi						5,507
14 Day Flexural ^d Strength (beams) psi						

Agency Use Only (Check appropriate Box)

This Mix Design MEETS CONTRACT SPECIFICATIONS and may be used on the bid items noted above

This Mix Design DOES NOT MEET CONTRACT SPECIFICATIONS and is being returned for corrections

Reviewed By: _____ PE Signature

RECEIVED

Aggregate Information

Concrete Aggregates	Component 1	Component 2	Component 3	Component 4	Component 5	Combined Gradation
WSDOT Pit No.	B-329	B-329	B-329	B-333		
WSDOT ASR 14-day Results (%) ^b	<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No				
Grading ^c	4	57	8	Class 2		
Percent of Total Aggregate						100%
Specific Gravity	2.71	2.69	2.68	2.65		
Lbs/cy (ssd)	480	1040	500	1100		

Percent Passing

2 inch	100	100	100	100		100
1-1/2 inch	100	100	100	100		100
1 inch	32.6	100	100	100		89.6
3/4 inch	1.6	80.0	100	100		78.2
1/2 inch	0.4	30.1	100	100		61.4
3/8 inch	0.2	7.8	88.6	100		52.1
No. 4	0.1	0.3	22.4	99.4		38.8
No. 8	0.1	0.2	1.4	90.2		32.1
No. 16	0.1	0.1	0.2	70		24.8
No. 30	0.1	0.1	0.2	44.1		15.6
No. 50	0.1	0.1	0.2	20		7.1
No. 100	0.1	0.1	0.2	6		2.2
No. 200	0.1	0.1	0.2	1.7		0.7

Fineness Modulus: 2.70 (Required for Class 2 Sand)

ASR Mitigation Method Proposed^b: _____

Notes:

- a Required for Class 4000D and 4000P mixes.
- b Alkali Silica Reactivity Mitigation is required for sources with expansions over 0.20% - Incidate method for ASR mitigation. For expansion of 0.21% - 0.45%, acceptable mitigation can be the use of low alkali cement or 25% type F fly ash. Any other proposed mitigation method or for pits with greater than 0.45% expansion, proof of mitigating measure, either ASTM C1260 / AASHTO T303 test results must be attached. If ASTM C 1293 testing has been submitted indicating 1-year expansion of 0.04% or less, mitigation is not required.
- c AASHTO No. 467, 57, 67, 7, 8; WSDOT Class 1, Class 2; or combined gradation. See Standard Specification 9-03.1.
- d Required for Cement Concrete Pavements.
- e Attach test results indicating conformance to Standard Specification 9-25.1.
- f Actual Average Strength as determined from testing or estimated from ACI 211.

RECEIVED

JAN 29 2017



Lafarge North America Concrete Lab
5400 W Marginal Way SW
Seattle, WA. 98106

Report To: Miles Sand & Gravel
Attention: Quality Control Personnel

Date: May 25, 2012

Subject: Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration: ASTM C-1202

Tested Materials: Date Sampled: March 2012
Mix Design: WSDOT Valley HPC

Curing: ASTM C-1202 Standard Cure

Results:

<u>Age</u>	<u>Coulombs</u>
56 day	1350
90 day	920

*The ASTM C-1202 procedure was followed.

The test result is only valid if the aggregate(s) sample(s) is(are) representative of the current production and it is to be noted that Lafarge has no knowledge of the representatives of the sample received for testing. Also, material quality can vary with different locations in a quarry. It is recommended that testing be carried out on an annual basis or more frequently if a variation in stone quality is suspected.

Although the Lafarge North America Seattle Concrete Lab. applies state-of-the-art test methods, Lafarge North America, and its affiliates (Lafarge) can not guarantee the results shown above and shall assume no liability whatsoever for any errors in such results and for the consequence of such errors.

Rob Shogren, P.E.
Technical Service Engineer
Lafarge North America

RECEIVED
JAN 29 2012
DEPT. OF TRANSPORTATION CHEHALIS ENGINEERING



Lafarge North America Concrete Lab
5400 W Marginal Way SW
Seattle, WA. 98106

Report To: Miles Sand & Gravel
Attention: Quality Control Personnel

Date: May 25, 2012

Subject: Length Change of Hardened Hydraulic-Cement Concrete Using Procedures of ASTM C-157

Tested Materials: Date Sampled: March, 2012
Source of Aggregates: Miles Sand & Gravel

Mix Design: WSDOT HPC

Results: Slump: 4.5" Specimen Size: 4"x4"x10"
Temp: 64°F Consolidation: Rodding
Initial Cure: Lime water submersion (28 day initial cure)

<u>Age (Days) After Initial Cure</u>	<u>Percent Length Change (Average of 3)</u>
7	0.010
14	0.017
21	0.026
28 (final)	0.030

*The ASTM C-157 procedure was followed.

The test result is only valid if the aggregate(s) sample(s) is(are) representative of the current production and it is to be noted that Lafarge has no knowledge of the representatives of the sample received for testing. Also, material quality can vary with different locations in a quarry. It is recommended that testing be carried out on an annual basis or more frequently if a variation in stone quality is suspected.

Although the Lafarge North America Seattle Concrete Lab. applies state-of-the-art test methods, Lafarge North America, and its affiliates (Lafarge) can not guarantee the results shown above and shall assume no liability whatsoever for any errors in such results and for the consequence of such errors.

Rob Shogren, P.E.
Technical Service Engineer
Lafarge North America

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JAN 29 2012

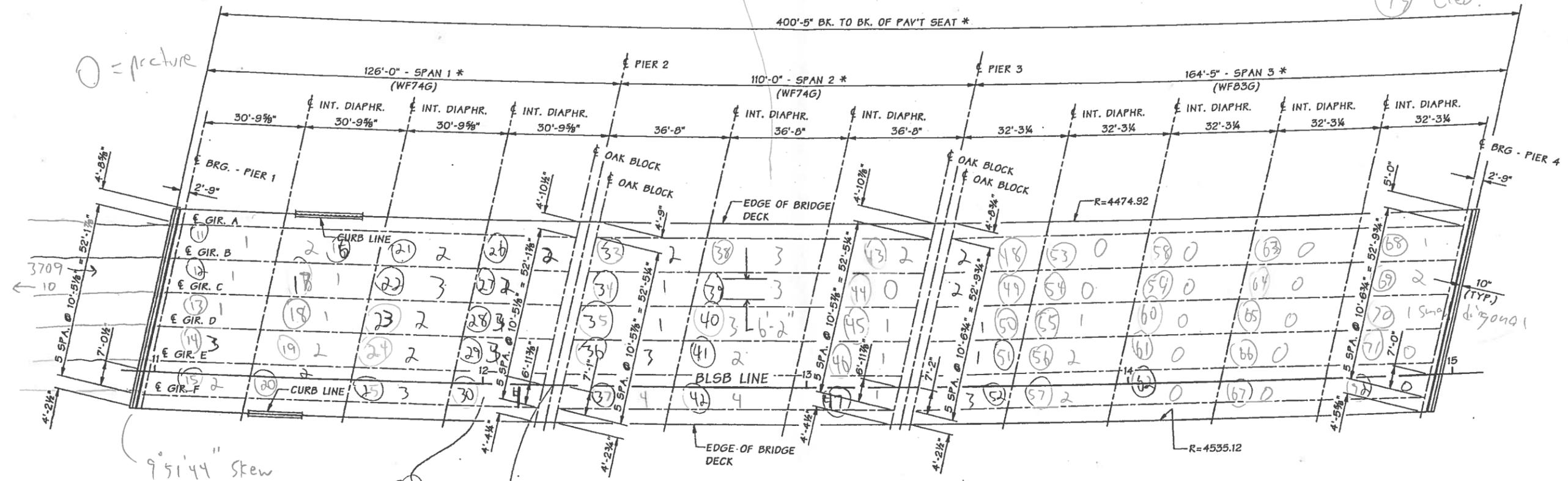
DEPT. OF TRANSPORTATION CHEHALIS ENGINEERING

* MEASURED ALONG BLSB LINE

73 Elev.

32 span 2 general pic

○ = fracture



31 of crack near X beam (Not really a crack)

FRAMING PLAN
BEARING OF ALL PIERS AND DIAPHRAGMS
IS N 77° 34' 08" W

SR 5 FILE NO. 7477 SHEET BW32

Bridge Design Engr.	Khaloghi, B	M:\X-Team\MELLEN TO BLAKESLEE JCT\5-234w\window files\FRAMING PLAN 1.wnd			
Supervisor	Stoddard, RB	REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.
Designed By	Collins, R	10	WASH.		
Checked By	Bedi, G	JOB NUMBER 12X304			
Detailed By	Plesha, GM	DATE			
Bridge Projects Engr.		REVISION			
Prelim. Plan By		BY APPD			
Architect/Specialist		DATE			



BRIDGE AND STRUCTURES OFFICE



I-5
MELLEN STREET TO
BLAKESLEE JUNCTION - STAGE 1
I-5 OVER BLAKESLEE JCT RR BRIDGE NO. 5/234W REPL.
FRAMING PLAN

BRIDGE SHEET NO. BW32
SHEET 325 OF 472 SHEETS



Bridge #	5/234W	Bridge Name	I-5 Over Blakeslee Jct RR			Structure ID	0018272C	
Contract #	8272	Region	SW	Project Engineer	Colin Newell	Performance Deck Concrete?	YES	
Contractor	Cascade Bridge		Concrete Supplier	Miles Sand & Gravel		Deck Placement	3/25/2013	
Bridge Description	3-Span (126' / 110' / 164.5'), 6-WF83G & WF74G Girders (400.5' bridge length), 3-Lanes (58' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	9%
Min. =	0%
Max. =	25%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	30.80	10.43	1	15	5%
1	1	B	C	30.80	10.43	1	15	5%
1	1	C	D	30.80	10.43	1	15	5%
1	1	D	E	30.80	10.43	3	15	20%
1	1	E	F	30.80	10.43	2	15	15%
1	2	A	B	30.80	10.43	2	15	15%
1	2	B	C	30.80	10.43	1	15	5%
1	2	C	D	30.80	10.43	1	15	5%
1	2	D	E	30.80	10.43	2	15	15%
1	2	E	F	30.80	10.43	2	15	15%
1	3	A	B	30.80	10.43	2	15	15%
1	3	B	C	30.80	10.43	3	15	20%
1	3	C	D	30.80	10.43	2	15	15%
1	3	D	E	30.80	10.43	2	15	15%
1	3	E	F	30.80	10.43	3	15	20%
1	4	A	B	30.80	10.43	2	15	15%
1	4	B	C	30.80	10.43	2	15	15%
1	4	C	D	30.80	10.43	3	15	20%
1	4	D	E	30.80	10.43	3	15	20%
1	4	E	F	30.80	10.43	4	15	25%
2	1	A	B	36.67	10.43	2	18	10%
2	1	B	C	36.67	10.43	1	18	5%
2	1	C	D	36.67	10.43	1	18	5%
2	1	D	E	36.67	10.43	3	18	15%
2	1	E	F	36.67	10.43	4	18	20%
2	2	A	B	36.67	10.43	3	18	15%
2	2	B	C	36.67	10.43	3	18	15%
2	2	C	D	36.67	10.43	3	18	15%
2	2	D	E	36.67	10.43	2	18	10%
2	2	E	F	36.67	10.43	4	18	20%
2	3	A	B	36.67	10.43	2	18	10%
2	3	B	C	36.67	10.43	0	18	0%
2	3	C	D	36.67	10.43	1	18	5%
2	3	D	E	36.67	10.43	1	18	5%
2	3	E	F	36.67	10.43	1	18	5%
3	1	A	B	32.27	10.43	2	16	15%
3	1	B	C	32.27	10.43	2	16	15%
3	1	C	D	32.27	10.43	1	16	5%
3	1	D	E	32.27	10.43	1	16	5%
3	1	E	F	32.27	10.43	3	16	20%



Bridge #	5/234W	Bridge Name	I-5 Over Blakeslee Jct RR			Structure ID	0018272C	
Contract #	8272	Region	SW	Project Engineer	Colin Newell	Performance Deck Concrete?	YES	
Contractor	Cascade Bridge		Concrete Supplier	Miles Sand & Gravel		Deck Placement	3/25/2013	
Bridge Description	3-Span (126' / 110' / 164.5'), 6-WF83G & WF74G Girders (400.5' bridge length), 3-Lanes (58' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

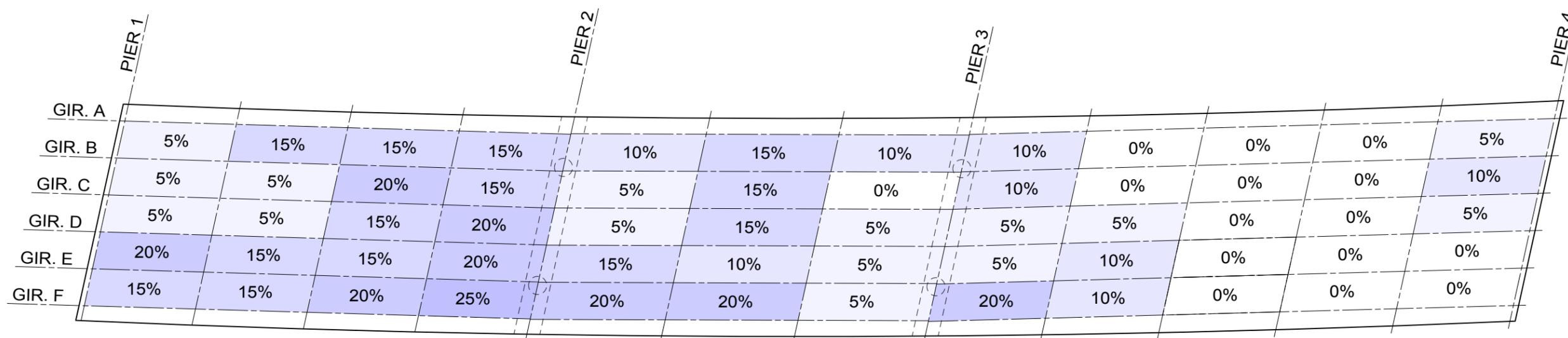
N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	9%
Min. =	0%
Max. =	25%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
3	2	A	B	32.27	10.43	0	16	0%
3	2	B	C	32.27	10.43	0	16	0%
3	2	C	D	32.27	10.43	1	16	5%
3	2	D	E	32.27	10.43	2	16	15%
3	2	E	F	32.27	10.43	2	16	15%
3	3	A	B	32.27	10.43	0	16	0%
3	3	B	C	32.27	10.43	0	16	0%
3	3	C	D	32.27	10.43	0	16	0%
3	3	D	E	32.27	10.43	0	16	0%
3	3	E	F	32.27	10.43	0	16	0%
3	4	A	B	32.27	10.43	0	16	0%
3	4	B	C	32.27	10.43	0	16	0%
3	4	C	D	32.27	10.43	0	16	0%
3	4	D	E	32.27	10.43	0	16	0%
3	4	E	F	32.27	10.43	0	16	0%
3	5	A	B	32.27	10.43	1	16	5%
3	5	B	C	32.27	10.43	2	16	15%
3	5	C	D	32.27	10.43	1	16	5%
3	5	D	E	32.27	10.43	0	16	0%
3	5	E	F	32.27	10.43	0	16	0%



CRACKING INTENSITY ~ BRIDGE 5/234W

100% = CRACK EVERY 2 FT.

LESS CRACKING

MORE CRACKING

BRIDGE NUMBER	5/234W
BRIDGE NAME	I-5 OVER BLAKESLEE JCT RR
INSPECTION DATE	4/8/2015
DECK CONCRETE	PERFORMANCE BASED

BRIDGE 105/4 (NORTH RIVER)

Bridge #	105/4	Bridge Name	North River			Structure ID	0018345B
Contract #	8345	Region	SW	Project Engineer	Lori Figone	Performance Deck Concrete?	YES
Contractor	Scarsella Bros.		Concrete Supplier	Bayview Redi Mix, Inc		Deck Placement	1/31/2014
Bridge Description	4-Span (120' / 160' / 160' / 160'), 4-WF83G Girders (600' bridge length), 2-Lanes (36' wide roadway)						

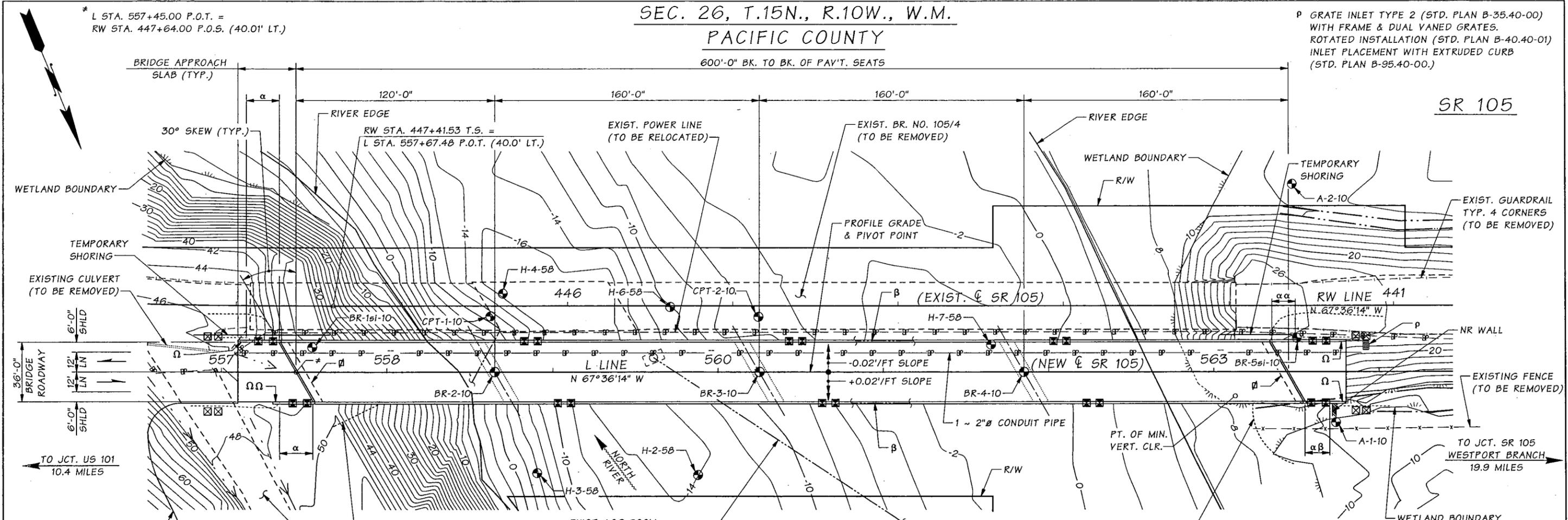


CONTENTS

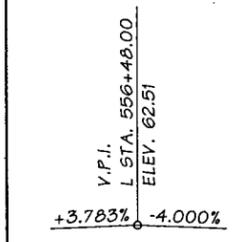
1. Layout Plan Sheet
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7. Crack Intensity Diagram

SEC. 26, T.15N., R.10W., W.M.
PACIFIC COUNTY

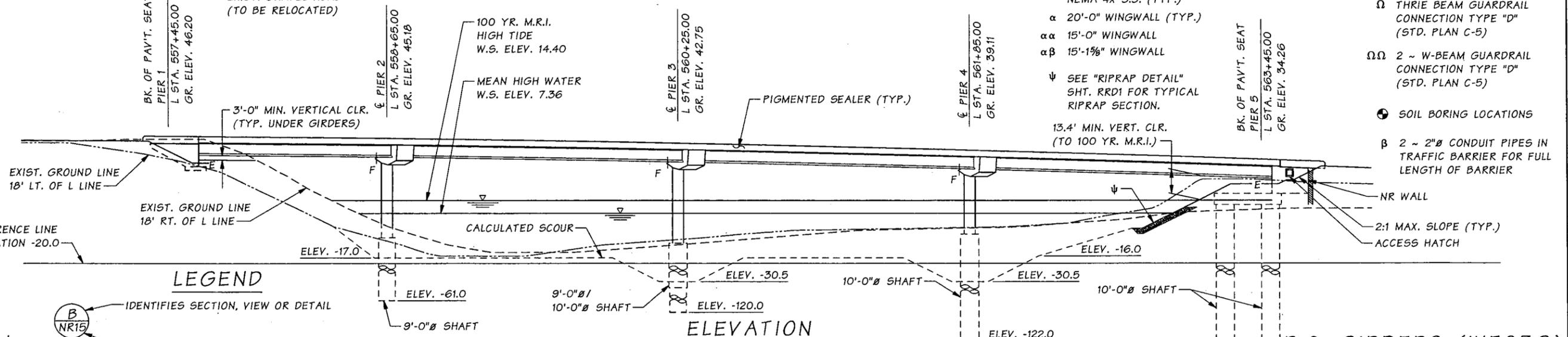
P GRATE INLET TYPE 2 (STD. PLAN B-35.40-00) WITH FRAME & DUAL VANED GRATES. ROTATED INSTALLATION (STD. PLAN B-40.40-01) INLET PLACEMENT WITH EXTRUDED CURB (STD. PLAN B-95.40-00.)



PLAN
BEARING OF ALL PIERS IS N 07°36'14" W



L LINE PROFILE



ELEVATION

GRADE ELEVATIONS SHOWN ARE FINISH GRADES AT TOP OF BRIDGE DECK ON L LINE AND ARE EQUAL TO PROFILE GRADE. SEE STD. PLAN A-50.10-00 FOR EMBANKMENT DETAILS AT BRIDGE ENDS.

- LEGEND**
- ⊠ IDENTIFIES SECTION, VIEW OR DETAIL
 - ⊠ TAKEN OR SHOWN ON BR. SHT. NR15
 - ⊠ TAKEN OR SHOWN ON THE SAME SHEET

- ⊠ JUNCTION BOX (TYP.)
- ⊠ JUNCTION BOX NEMA 4X S.S. (TYP.)
- α 20'-0" WINGWALL (TYP.)
- αα 15'-0" WINGWALL
- αβ 15'-1 1/2" WINGWALL
- ψ SEE "RIPRAP DETAIL" SHT. RRD1 FOR TYPICAL RIPRAP SECTION.
- 13.4' MIN. VERT. CLR. (TO 100 YR. M.R.I.)
- ⊠ FRONT FACE OF ABUTMENT WALL
- ⊠ THRIE BEAM GUARDRAIL CONNECTION TYPE "D" (STD. PLAN C-5)
- ⊠ 2 ~ W-BEAM GUARDRAIL CONNECTION TYPE "D" (STD. PLAN C-5)
- ⊠ SOIL BORING LOCATIONS
- β 2 ~ 2" CONDUIT PIPES IN TRAFFIC BARRIER FOR FULL LENGTH OF BARRIER

P.C. GIRDERS (WF83G)
LOADING: HL-93

SR 105 FILE NO. 7008 SHEET NR1

Bridge Design Engr. Khaleghi, B	M:\Y-Team\SR 105 BRIDGES\NORTH RIVER BR_NO_105-4 REPLACEMENT\window files\LAYO	REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
Supervisor Anderson, MW		10	WASH.			
Designed By Frymoyer, ML		JOB NUMBER				
Checked By Lee, CS		12X311				
Detailed By Bontemps, W						
Bridge Projects Engr. Lewis, RA						
Prelim. Plan By Wei, J						
Architect/Specialist PDK/BSA/GAW	DATE	REVISION	BY	APPD		

BRIDGE AND STRUCTURES OFFICE
6/19/12



SR 105
SMITH CREEK AND NORTH RIVER
REPLACE BRIDGES
NORTH RIVER BR. NO. 105/4
LAYOUT

Washington State Department of Transportation

BRIDGE SHEET NO. NR1
SHEET 133 OF 210 SHEETS

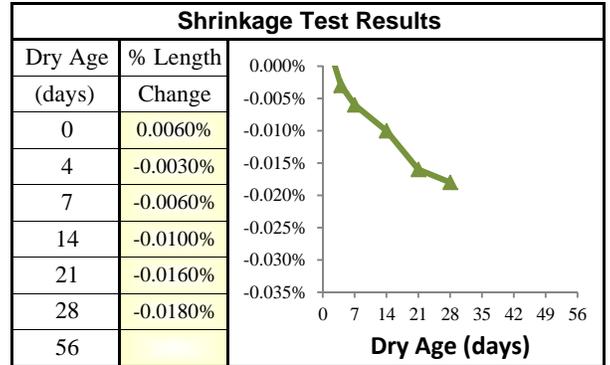
C.S. 2535 ~ PROJ. NO. XL2928 ~ SOUTHWEST REGION ~ SR 105 ~ MP 10.07 TO MP 10.66 ~ NORTH RIVER BR. NO. 105/4 REPLACEMENT.



Bridge #	105/4	Bridge Name	North River			Structure ID	0018345B
Contract #	8345	Region	SW	Project Engineer	Lori Figone	Performance Deck Concrete?	YES
Contractor	Scarsella Bros.		Concrete Supplier	Bayview Redi Mix, Inc		Deck Placement	1/31/2014
Bridge Description	4-Span (120' / 160' / 160' / 160'), 4-WF83G Girders (600' bridge length), 2-Lanes (36' wide roadway)						

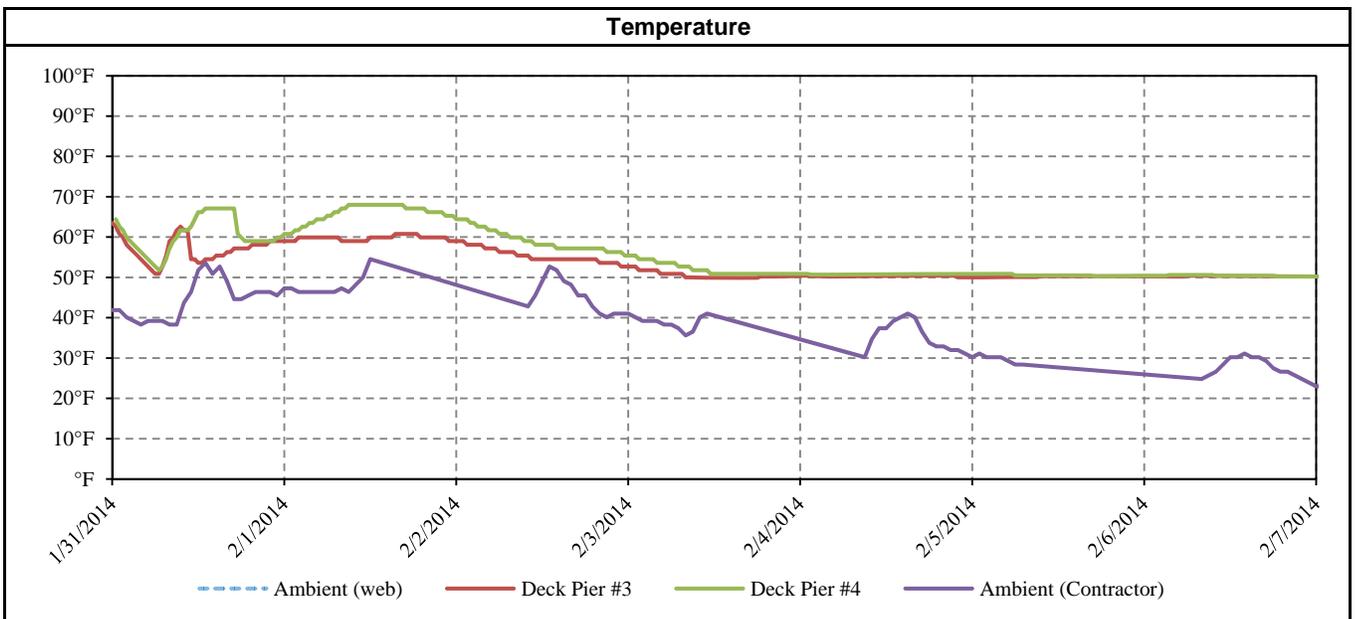
Mix Design (WSDOT Form 350-040)			
Water (max) =		230 lbs/cy	w/c = 0.38 max
Cementitious Materials	Lbs/cy	Source	Type, Class or Grade
cement	460	Ashgrove	Type I-II
fly ash	150	Lafarge	Type F
slag			
latex			
microsilica			
Concrete Admixtures	oz/cy	Manufacturer	Product
air entrainment	1-15	BASF	Micro Air
water reducer			
HR water reduce	20-30	BASF	Glenium 7500
set retarder			
shrink. reducer	120-140	BASF	Masterlife

Concrete Test Results		
compressive strength @ 28 days	5,691	psi
modulus of elasticity	4,012,122	psi
permeability @ 56 days	1,677	coulombs
mix design density	150.1	lb/cf



Aggregate					
	Comp. 1	Comp. 2	Comp. 3	Comp. 4	Comp. 5
WSDOT Pit #	PS-X-130	PS-X-130	PS-X-130		
Grading	#67	#4	Class II		
% Total	42.0%	20.0%	38.0%		
Lbs/cy	1350	650	1213		
ASR Mitigation	None Required				

Notes
Same Mix Design as:
* Bridge 6/8
* Bridge 101/31
* Bridge 101/44
* Bridge 105/3
if swell of concrete specimen is included, total change in length at 28 days drying is 240 microstrain (0.0060% + 0.0180%)



CMD-008



Concrete Mix Design

Contractor SB Structures		Submitted By Bayview Redi-Mix, Inc	Date 07/22/2013
Concrete Supplier Bayview Redi Mix, Inc		Plant Location Raymond 041, Aberdeen 011	
Contract Number 8344 8345	Contract Name SMITH CREEK AND NORTH RIVER REPLACE Middle Nemah River Bridge Replacement Bridge BRIDGES		

This mix is to be used in the following Bid Item No(s): 48 & 49

Concrete Class: (check one only)

- 3000
 4000
 4000^a
 4000^aP
 4000W
 Concrete Overlay
 Cement Concrete Pavement^d
 Other Shrinkage

Remarks: _____

Mix Design No. WSDT4DS130 Plant No. 041, 011

Cementitious Materials	Source	Type, Class or Grade	Sp. Gr.	Lbs/cy
Cement	Ashgrove, Seattle, WA	Type I-II	3.15	460
Fly Ash ^a	Lafarge, Centralia, WA	Type F	2.58	150
GGBFS (Slag)				
Latex				
Microsilica				

Concrete Admixtures	Manufacturer	Product	Type	Est. Range (oz/cy)
Air Entrainment	BASF Cleveland, OH	Micro Air		1-15
Water Reducer				
High-Range Water Reducer	BASF Cleveland, OH	Glenium 7500	F	20-30
Set Retarder				
Other Shrinkage	BASF Cleveland, OH	Masterlife		120-140

no standard
TRIAL
7
0.7625-7.15
CY
12.2-91.5
CY
64-192
CY

Water (Maximum) 230 lbs/cy $\frac{230}{60} = 0.377$ Is any of the water Recycled or Reclaimed? Yes^e No^e

Water Cementitious Ratio (Maximum) .38 Mix Design Density 150.1 lbs/cf^d

Design Performance	1	2	3	4	5	Average ^f
28 Day Compressive Strength (cylinders) psi	5,775	5,766	5,623	5,561	5,730	5,691
14 Day Flexural ^d Strength (beams) psi						

Agency Use Only (Check appropriate Box)

This Mix Design MEETS CONTRACT SPECIFICATIONS and may be used on the bid items noted above

This Mix Design DOES NOT MEET CONTRACT SPECIFICATIONS and is being returned for corrections

Reviewed By: [Signature] PE Signature 12/3/13 Date

Mix Design No. WSDT4DS130 Plant No. 041,011

Aggregate Information

Concrete Aggregates	Component 1	Component 2	Component 3	Component 4	Component 5	Combined Gradation
WSDOT Pit No.	PS-X-130	PS-X130	PS-X-130			
WSDOT ASR 14-day Results (%) ^b	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No	
Grading ^c	AAASHTO #67	AAASHTO #4	Class II			
Percent of Total Aggregate	42	20	38			100%
Specific Gravity	2.825	2.825	2.747			
Lbs/cy (ssd)	1350	650	1213			

Percent Passing

	Component 1	Component 2	Component 3	Component 4	Component 5	Combined	
2 inch	100	100	100			100	
1-1/2 inch	100	100	100			100	
1 inch	100	52	100			90	90.4
3/4 inch	93	1	100			77	77.3
1/2 inch	58	1	100			63	62.6
3/8 inch	30	1	100			51	50.8
No. 4	7	0	99			41	40.6
No. 8	0	0	78			30	29.6
No. 16	0	0	58			22	-
No. 30	0	0	35			13	13.3
No. 50	0	0	14			5	5.3
No. 100	0	0	3			1	1.1
No. 200	0	.1	1.1			0.5	0.4

Fineness Modulus: 3.14 (Required for Class 2 Sand)

ASR Mitigation Method Proposed^b: Not Required for this Source

Notes:

- ^a Required for Class 4000D and 4000P mixes.
- ^b Alkali Silica Reactivity Mitigation is required for sources with expansions over 0.20% - Incidate method for ASR mitigation. For expansion of 0.21% - 0.45%, acceptable mitigation can be the use of low alkali cement or 25% type F fly ash. Any other proposed mitigation method or for pits with greater than 0.45% expansion, proof of mitigating measure, either ASTM C1260 / AASHTO T303 test results must be attached. If ASTM C 1293 testing has been submitted indicating 1-year expansion of 0.04% or less, mitigation is not required.
- ^c AASHTO No. 467, 57, 67, 7, 8; WSDOT Class 1, Class 2; or combined gradation. See Standard Specification 9-03.1.
- ^d Required for Cement Concrete Pavements.
- ^e Attach test results indicating conformance to Standard Specification 9-25.1.
- ^f Actual Average Strength as determined from testing or estimated from ACI 211.

TEST RESULTS

ASTM C 192 - Standard Practice for Making and Curing Concrete Test Specimens in the Laboratory

Concrete Mixture Proportions

4,000 PSI Mix

Trial Mix Results Calculated to 1yd³

D-101112-01

<u>S-Number</u>	<u>Description</u>	<u>SpG</u>	<u>Mass, lbs</u>	<u>Vol. Cuft</u>
S-121541	AG Seattle Type I/II	3.15	462	2.35
S-120817	Lafarge Centralia Class F	2.58	151	0.94
S-122202	Pit X-130 Fine Agg.	2.75	1,217	7.09
S-122204	Pit X-130 1.5 to 3/4 Agg.	2.83	652	3.69
S-122203	Pit X-130 3/4 to No. 4 Agg.	2.83	1,357	7.68
---	Overland Park Municipal	1.00	233	3.73
-	Air	-	5.6%	1.51
Totals:			4,072	27.00

Admixtures

<u>S-Number</u>	<u>Description</u>	<u>Dosage, oz/cwt</u>
S-122303	BASF Micro-Air	1.0
S-122302	BASF Glenium 7500	4.0
S-122225	BASF Master Life SRA 20	21.0

Plastic Properties

D-101112-01

Slump, in:	6.75
Unit Weight, lbs/cuft	150.8
Air Content (Calculated), %:	5.6
w/cm ratio:	0.38
Concrete Temperature, F:	74°

between 4.5 and 7.5 pps AD5 p8

AASHTO T 277 - Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration
Accelerated Cure

<u>Sample No.</u>	<u>Diameter, in.</u>	<u>Charge Passed, C</u>	<u>Corrected Charge, C</u>	<u>Qualitative Equivalent</u>	<u>Age, days</u>
D-101112-01	4.00	739	650	Very Low	28

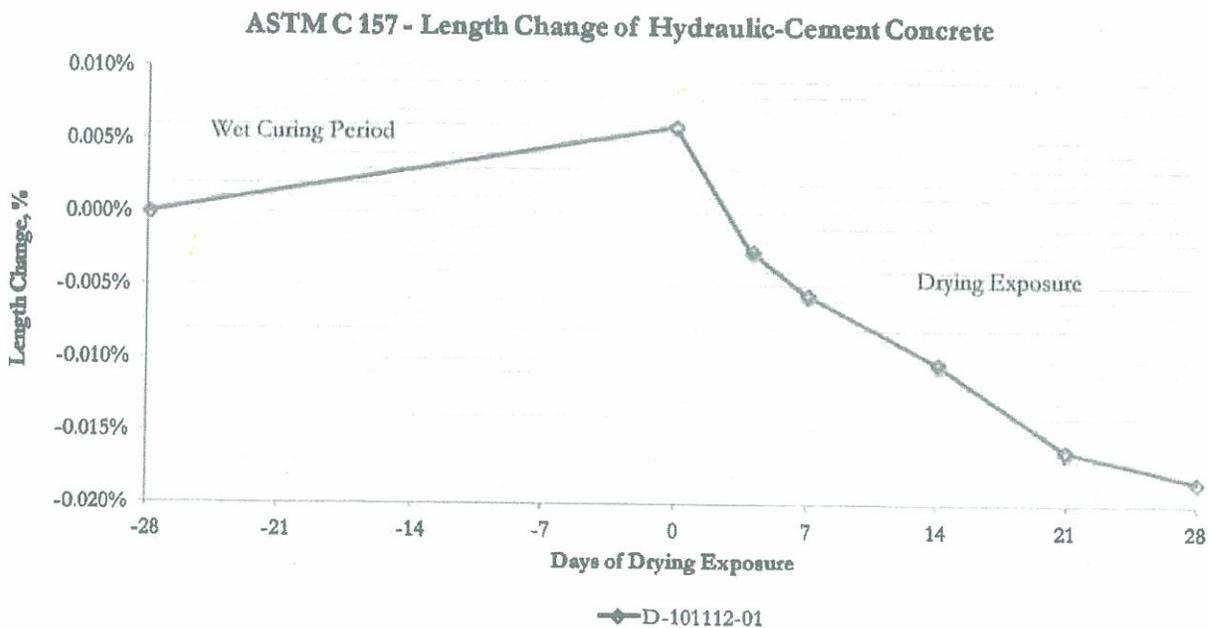
AASHTO T 277 - Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration
Standard Cure

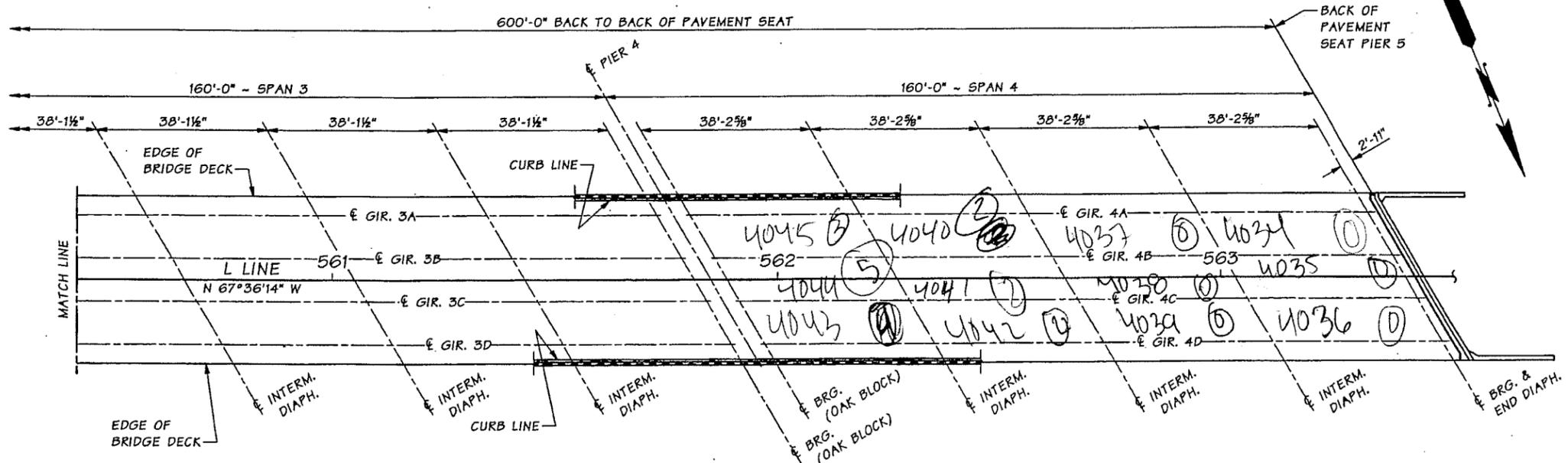
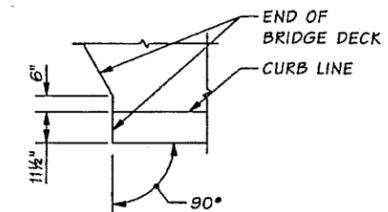
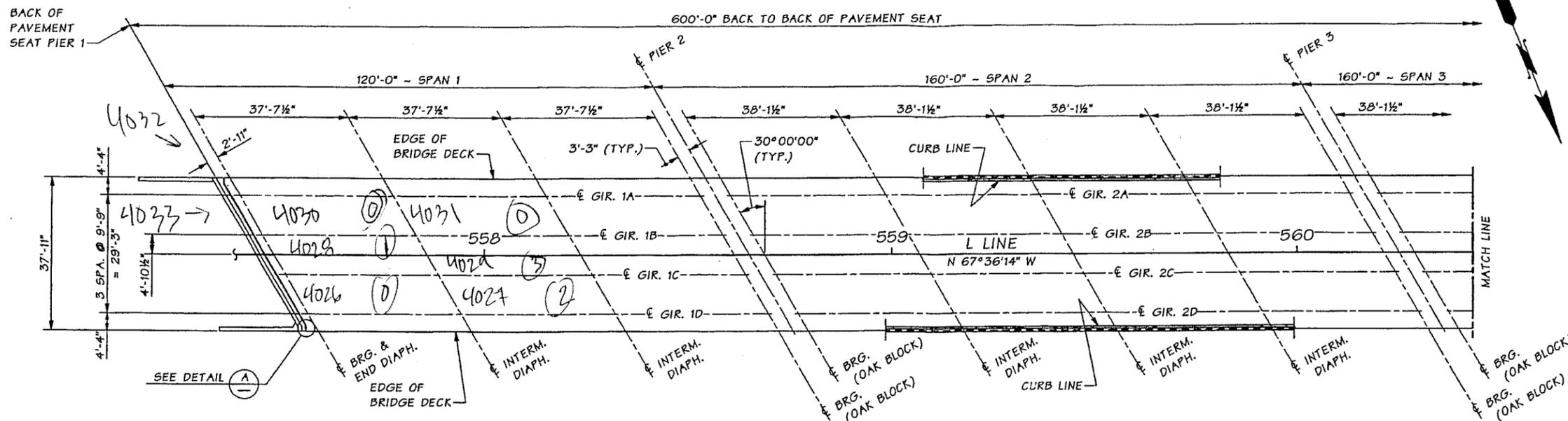
<u>Sample No.</u>	<u>Diameter, in.</u>	<u>Charge Passed, C</u>	<u>Corrected Charge, C</u>	<u>Qualitative Equivalent</u>	<u>Age, days</u>
D-101112-01	4.00	1,902	1,672	Low	28
	4.00	1,750	1,538	Low	56
	4.00	1,908	1,677	Low	56

ASTM C 157 Standard Test Method for Length Change of Hardened Hydraulic-Cement Mortar and Concrete

Material:	Concrete
Number of Specimens per Mixture:	4
Size of Specimens, in.:	Length: 10.0
	Width: 4.0
	Height: 4.0
Method of Consolidation:	4
Period of Moist Curing:	28-days
Drying Exposure Conditions:	23°C, 50% RH

Length Change	Reading	D-101112-01
	Initial	0.000%
	0-days dry	0.006%
	4-days dry	-0.003%
	7-days dry	-0.006%
	14-days dry	-0.010%
	21-days dry	-0.016%
	28-days dry	-0.018%





FRAMING PLAN

ALL LONGITUDINAL DIMENSIONS ARE ALONG L LINE UNLESS OTHERWISE SHOWN.

SR 105 FILE NO. 7008 SHEET NR36

Bridge Design Engr.	Khaloghi, B	M:\Y-Team\SR 105 BRIDGES\NORTH RIVER BR_NO_105-4 REPLACEMENT\window files\FRAMING PLAN.wnd			
Supervisor	Anderson, MW	REVISION	DATE	BY	APP'D
Designed By	Lee, CS 01/12				
Checked By	Olson, DE 04/12				
Detailed By	Bontemps, W 01/12				
Bridge Projects Engr.					
Prelim. Plan By					
Architect/Specialist					



BRIDGE AND STRUCTURES OFFICE
 6/13/12



SR 105
 SMITH CREEK AND NORTH RIVER
 REPLACE BRIDGES
 NORTH RIVER BR. NO. 105/4
 FRAMING PLAN

BRIDGE SHEET NO. NR36
 SHEET 168 OF 210 SHEETS



Bridge #	105/4	Bridge Name	North River			Structure ID	0018345B	
Contract #	8345	Region	SW	Project Engineer	Lori Figone	Performance Deck Concrete?	YES	
Contractor	Scarsella Bros.		Concrete Supplier	Bayview Redi Mix, Inc		Deck Placement	1/31/2014	
Bridge Description	4-Span (120' / 160' / 160' / 160'), 4-WF83G Girders (600' bridge length), 2-Lanes (36' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	7%
Min. =	0%
Max. =	25%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	37.63	9.75	0	19	0%
1	1	B	C	37.63	9.75	1	19	5%
1	1	C	D	37.63	9.75	0	19	0%
1	2	A	B	37.63	9.75	0	19	0%
1	2	B	C	37.63	9.75	3	19	15%
1	2	C	D	37.63	9.75	2	19	10%
1	3	A	B	37.63	9.75	#N/A	19	#N/A
1	3	B	C	37.63	9.75	#N/A	19	#N/A
1	3	C	D	37.63	9.75	#N/A	19	#N/A
2	1	A	B	38.13	9.75	#N/A	19	#N/A
2	1	B	C	38.13	9.75	#N/A	19	#N/A
2	1	C	D	38.13	9.75	#N/A	19	#N/A
2	2	A	B	38.13	9.75	#N/A	19	#N/A
2	2	B	C	38.13	9.75	#N/A	19	#N/A
2	2	C	D	38.13	9.75	#N/A	19	#N/A
2	3	A	B	38.13	9.75	#N/A	19	#N/A
2	3	B	C	38.13	9.75	#N/A	19	#N/A
2	3	C	D	38.13	9.75	#N/A	19	#N/A
2	4	A	B	38.13	9.75	#N/A	19	#N/A
2	4	B	C	38.13	9.75	#N/A	19	#N/A
2	4	C	D	38.13	9.75	#N/A	19	#N/A



Bridge #	105/4	Bridge Name	North River			Structure ID	0018345B	
Contract #	8345	Region	SW	Project Engineer	Lori Figone	Performance Deck Concrete?	YES	
Contractor	Scarsella Bros.		Concrete Supplier	Bayview Redi Mix, Inc		Deck Placement	1/31/2014	
Bridge Description	4-Span (120' / 160' / 160' / 160'), 4-WF83G Girders (600' bridge length), 2-Lanes (36' wide roadway)							

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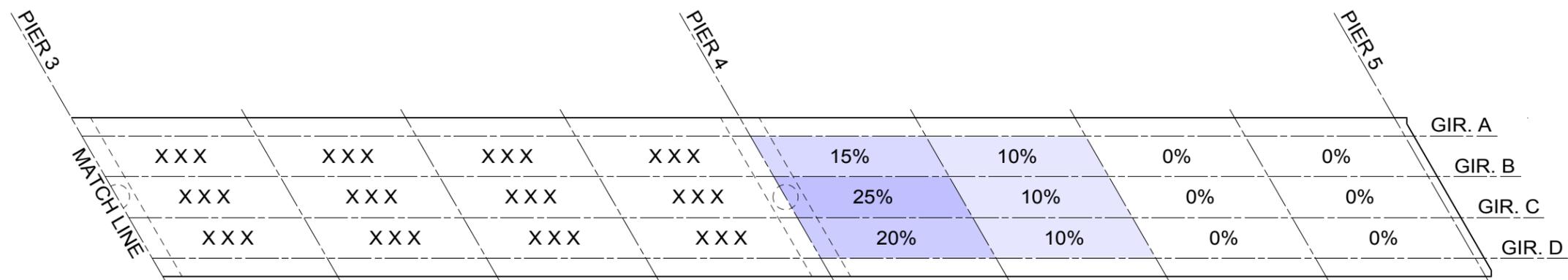
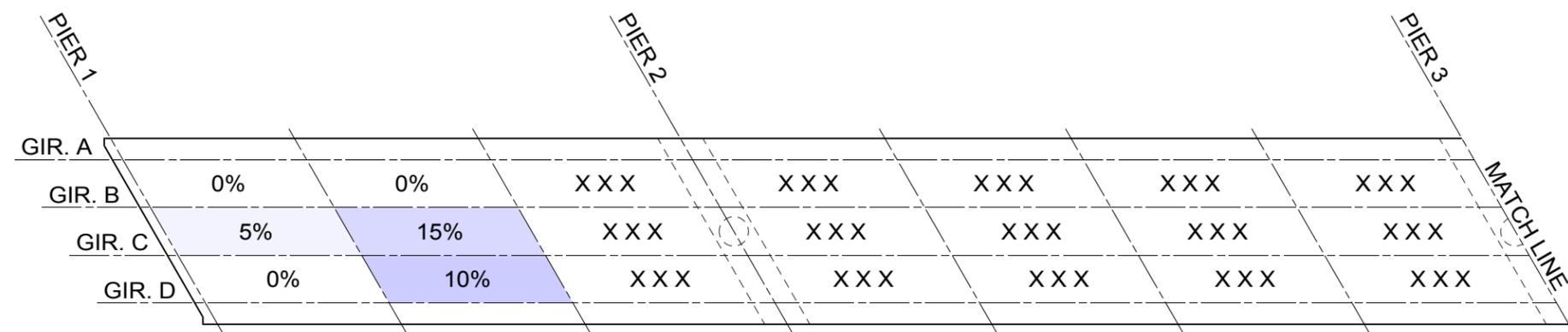
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N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	7%
Min. =	0%
Max. =	25%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
3	1	A	B	38.13	9.75	#N/A	19	#N/A
3	1	B	C	38.13	9.75	#N/A	19	#N/A
3	1	C	D	38.13	9.75	#N/A	19	#N/A
3	2	A	B	38.13	9.75	#N/A	19	#N/A
3	2	B	C	38.13	9.75	#N/A	19	#N/A
3	2	C	D	38.13	9.75	#N/A	19	#N/A
3	3	A	B	38.13	9.75	#N/A	19	#N/A
3	3	B	C	38.13	9.75	#N/A	19	#N/A
3	3	C	D	38.13	9.75	#N/A	19	#N/A
3	4	A	B	38.13	9.75	#N/A	19	#N/A
3	4	B	C	38.13	9.75	#N/A	19	#N/A
3	4	C	D	38.13	9.75	#N/A	19	#N/A
4	1	A	B	38.22	9.75	3	19	15%
4	1	B	C	38.22	9.75	5	19	25%
4	1	C	D	38.22	9.75	4	19	20%
4	2	A	B	38.22	9.75	2	19	10%
4	2	B	C	38.22	9.75	2	19	10%
4	2	C	D	38.22	9.75	2	19	10%
4	3	A	B	38.22	9.75	0	19	0%
4	3	B	C	38.22	9.75	0	19	0%
4	3	C	D	38.22	9.75	0	19	0%
4	4	A	B	38.22	9.75	0	19	0%
4	4	B	C	38.22	9.75	0	19	0%
4	4	C	D	38.22	9.75	0	19	0%



CRACKING INTENSITY ~ BRIDGE 105/4

100% = CRACK EVERY 2 FT.

X X X = CRACKS NOT COUNTED DUE TO LIMITED ACCESS

LESS CRACKING

MORE CRACKING



BRIDGE NUMBER	105/4
BRIDGE NAME	NORTH RIVER
INSPECTION DATE	5/7/2015
DECK CONCRETE	PERFORMANCE BASED

BRIDGE 105/3 (SMITH CREEK)

Bridge #	105/3	Bridge Name	Smith Creek			Structure ID	0018345A
Contract #	8345	Region	SW	Project Engineer	Lori Figone	Performance Deck Concrete?	YES
Contractor	Scarsella Bros.		Concrete Supplier	Bayview Redi Mix, Inc		Deck Placement	12/17/2013
Bridge Description	3-Span (105' / 110' / 105'), 5-WF42G Girders (320' bridge length), 2-Lanes (36' wide roadway)						



CONTENTS

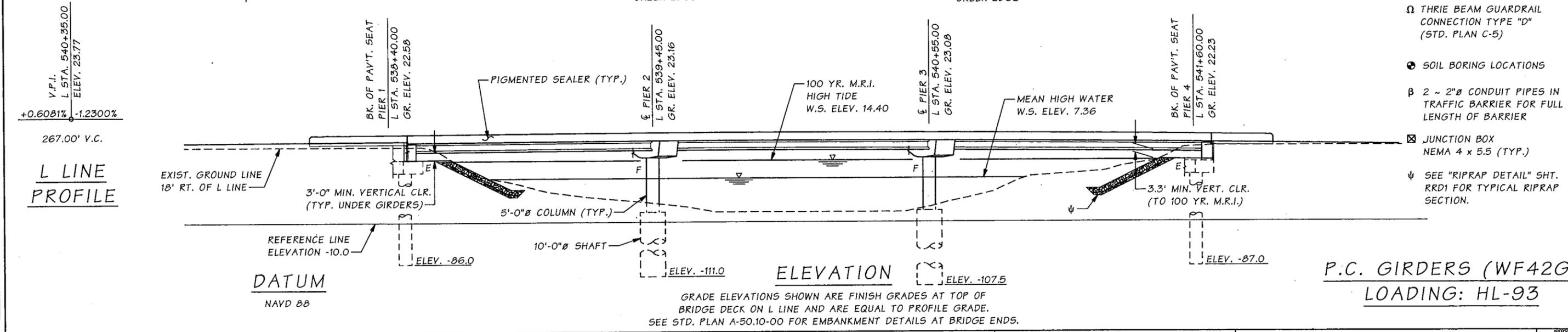
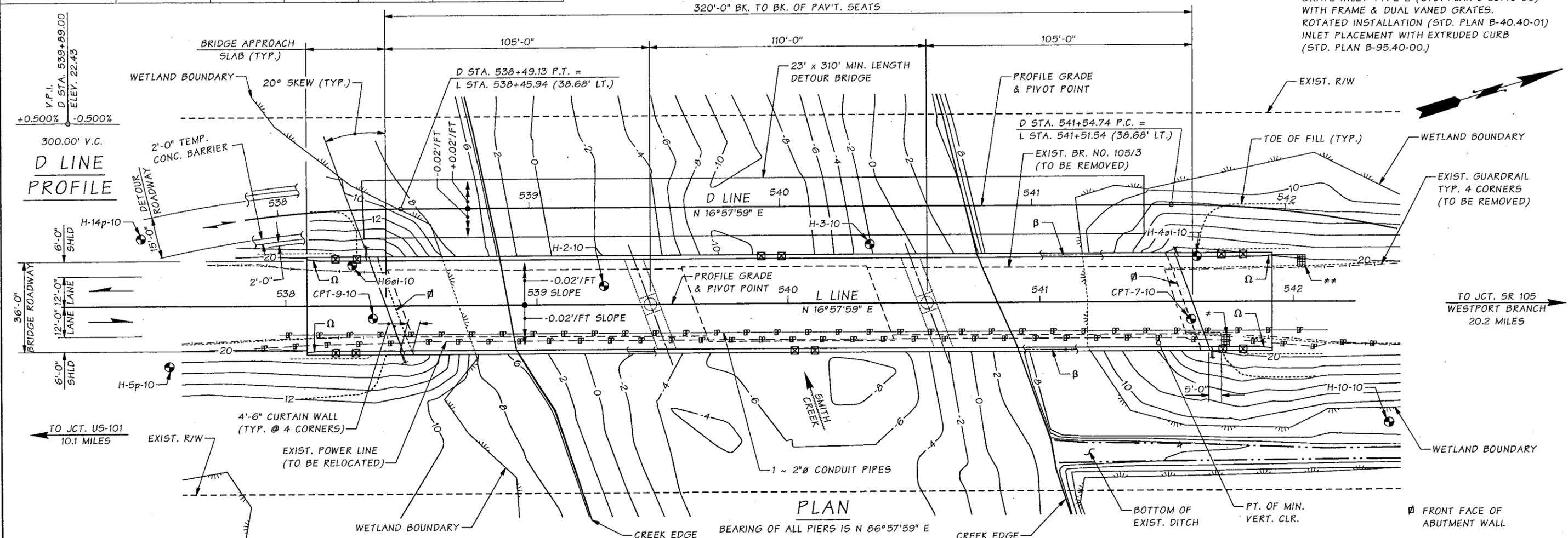
1. Layout Plan Sheet
2. Mix Design Summary
3. Concrete Mix Design Form
4. Concrete Test Results
5. Field Notes
6. Crack Summary
7. Crack Intensity Diagram

SEC. 26, T.15N., R.10W., W.M.
PACIFIC COUNTY

SR 105

- * GRATE INLET TYPE 2 (STD. PLAN B-35.40-00) WITH FRAME & DUAL VANED GRATES. ROTATED INSTALLATION (STD. PLAN B-40.40-01)
- ** GRATE INLET TYPE 2 (STD. PLAN B-35.40-00) WITH FRAME & DUAL VANED GRATES. ROTATED INSTALLATION (STD. PLAN B-40.40-01) INLET PLACEMENT WITH EXTRUDED CURB (STD. PLAN B-95.40-00.)

CURVE DATA					
P.I. STATION	Δ	RADIUS	TANGENT	LENGTH	BK. TANGENT BRG.
D STA. 537+92.85	14°05'30" RT.	460.00'	56.85'	113.14'	N 2°52'29" E
D STA. 542+05.15	14°01'11" RT.	410.00'	50.41'	100.32'	N 16°57'59" E



Bridge Design Engr.	Khaileghi, B	M:\Y-Team\SR 105 BRIDGES\SMITH CREEK BR_NO_105-3 REPLACEMENT>window files\LAYOUT.wnd
Supervisor	Anderson, MW	
Designed By	Glassford, P	11/12
Checked By	Burnham, B	05/12
Detailed By	Nettle, J	11/12
Bridge Projects Engr.	Lewis, RA	12/09
Prelim. Plan By	Wei, J	11/09
Architect/Specialist	PDK/BSA/GAW	
DATE	REVISION	BY APP'D

BRIDGE AND STRUCTURES OFFICE

6/14/12

Washington State Department of Transportation

SR 105 SMITH CREEK AND NORTH RIVER REPLACE BRIDGES SMITH CREEK BR. NO. 105-3 LAYOUT	BRIDGE SHEET NO. SC1 SHEET 87 OF 210 SHEETS
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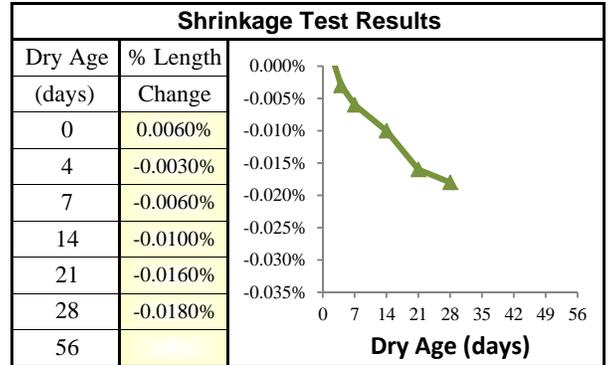
SR 105 FILE NO. SHEET SCI



Bridge #	105/3	Bridge Name	Smith Creek			Structure ID	0018345A
Contract #	8345	Region	SW	Project Engineer	Lori Figone	Performance Deck Concrete?	YES
Contractor	Scarsella Bros.		Concrete Supplier	Bayview Redi Mix, Inc		Deck Placement	12/17/2013
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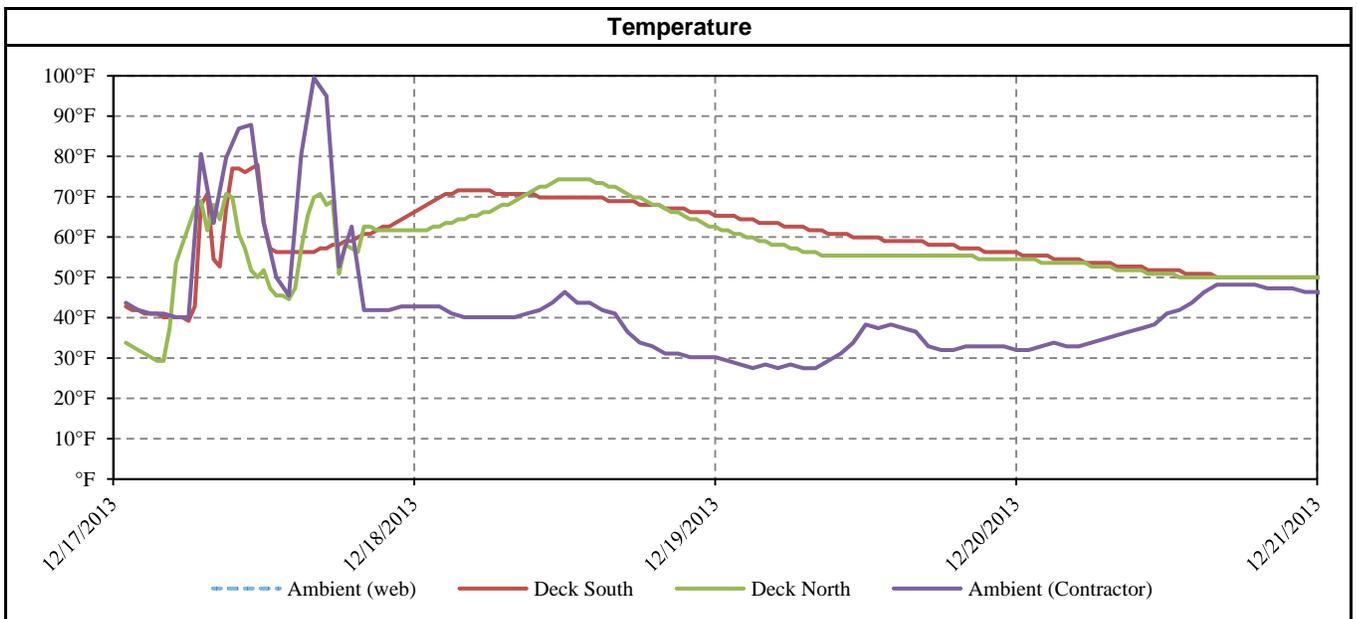
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latex			
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water reducer			
HR water reduce	20-30	BASF	Glenium 7500
set retarder			
shrink. reducer	120-140	BASF	Masterlife

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modulus of elasticity	4,012,122	psi
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Aggregate					
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% Total	42.0%	20.0%	38.0%		
Lbs/cy	1350	650	1213		
ASR Mitigation	None Required				

Notes
Same Mix Design as:
* Bridge 6/8
* Bridge 101/31
* Bridge 101/44
* Bridge 105/4
if swell of concrete specimen is included, total change in length at 28 days drying is 240 microstrain (0.0060% + 0.0180%)



CMD-008



Concrete Mix Design

Contractor SB Structures		Submitted By Bayview Redi-Mix, Inc	Date 07/22/2013
Concrete Supplier Bayview Redi Mix, Inc		Plant Location Raymond 041, Aberdeen 011	
Contract Number 8344 8345	Contract Name SMITH CREEK AND NORTH RIVER REPLACE Middle Nemah River Bridge Replacement Bridge BRIDGES		

This mix is to be used in the following Bid Item No(s): 48 & 49

Concrete Class: (check one only)

- 3000
 4000
 4000^a
 4000^aP
 4000W
 Concrete Overlay
 Cement Concrete Pavement^d
 Other Shrinkage

Remarks: _____

Mix Design No. WSDT4DS130 Plant No. 041, 011

Cementitious Materials	Source	Type, Class or Grade	Sp. Gr.	Lbs/cy
Cement	Ashgrove, Seattle, WA	Type I-II	3.15	460
Fly Ash ^a	Lafarge, Centralia, WA	Type F	2.58	150
GGBFS (Slag)				
Latex				
Microsilica				

Concrete Admixtures	Manufacturer	Product	Type	Est. Range (oz/cy)
Air Entrainment	BASF Cleveland, OH	Micro Air		1-15
Water Reducer				
High-Range Water Reducer	BASF Cleveland, OH	Glenium 7500	F	20-30
Set Retarder				
Other Shrinkage	BASF Cleveland, OH	Masterlife		120-140

no standard
TRIAL
7
0.7625-7.15
CY
12.2-91.5
CY
64-192
CY

Water (Maximum) 230 lbs/cy $\frac{230}{60} = 0.377$ Is any of the water Recycled or Reclaimed? Yes^e No^e

Water Cementitious Ratio (Maximum) .38 Mix Design Density 150.1 lbs/cf^d

Design Performance	1	2	3	4	5	Average ^f
28 Day Compressive Strength (cylinders) psi	5,775	5,766	5,623	5,561	5,730	5,691
14 Day Flexural ^d Strength (beams) psi						

Agency Use Only (Check appropriate Box)

This Mix Design MEETS CONTRACT SPECIFICATIONS and may be used on the bid items noted above

This Mix Design DOES NOT MEET CONTRACT SPECIFICATIONS and is being returned for corrections

Reviewed By: [Signature] 12/3/13

PE Signature Date

Mix Design No. WSDT4DS130 Plant No. 041,011

Aggregate Information

Concrete Aggregates	Component 1	Component 2	Component 3	Component 4	Component 5	Combined Gradation
WSDOT Pit No.	PS-X-130	PS-X130	PS-X-130			
WSDOT ASR 14-day Results (%) ^b	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No	
Grading ^c	AAASHTO #67	AAASHTO #4	Class II			
Percent of Total Aggregate	42	20	38			100%
Specific Gravity	2.825	2.825	2.747			
Lbs/cy (ssd)	1350	650	1213			

Percent Passing

	Component 1	Component 2	Component 3	Component 4	Component 5	Combined Gradation
2 inch	100	100	100			100
1-1/2 inch	100	100	100			100
1 inch	100	52	100			90
3/4 inch	93	1	100			77
1/2 inch	58	1	100			63
3/8 inch	30	1	100			51
No. 4	7	0	99			41
No. 8	0	0	78			30
No. 16	0	0	58			22
No. 30	0	0	35			13
No. 50	0	0	14			5
No. 100	0	0	3			1
No. 200	0	.1	1.1			0.5

Fineness Modulus: 3.14 (Required for Class 2 Sand)

ASR Mitigation Method Proposed^b: Not Required for this Source

Notes:

- ^a Required for Class 4000D and 4000P mixes.
- ^b Alkali Silica Reactivity Mitigation is required for sources with expansions over 0.20% - Incidate method for ASR mitigation. For expansion of 0.21% - 0.45%, acceptable mitigation can be the use of low alkali cement or 25% type F fly ash. Any other proposed mitigation method or for pits with greater than 0.45% expansion, proof of mitigating measure, either ASTM C1260 / AASHTO T303 test results must be attached. If ASTM C 1293 testing has been submitted indicating 1-year expansion of 0.04% or less, mitigation is not required.
- ^c AASHTO No. 467, 57, 67, 7, 8; WSDOT Class 1, Class 2; or combined gradation. See Standard Specification 9-03.1.
- ^d Required for Cement Concrete Pavements.
- ^e Attach test results indicating conformance to Standard Specification 9-25.1.
- ^f Actual Average Strength as determined from testing or estimated from ACI 211.

TEST RESULTS

ASTM C 192 - Standard Practice for Making and Curing Concrete Test Specimens in the Laboratory

Concrete Mixture Proportions

4,000 PSI Mix

Trial Mix Results Calculated to 1yd³

D-101112-01

<u>S-Number</u>	<u>Description</u>	<u>SpG</u>	<u>Mass, lbs</u>	<u>Vol. Cuft</u>
S-121541	AG Seattle Type I/II	3.15	462	2.35
S-120817	Lafarge Centralia Class F	2.58	151	0.94
S-122202	Pit X-130 Fine Agg.	2.75	1,217	7.09
S-122204	Pit X-130 1.5 to 3/4 Agg.	2.83	652	3.69
S-122203	Pit X-130 3/4 to No. 4 Agg.	2.83	1,357	7.68
---	Overland Park Municipal	1.00	233	3.73
-	Air	-	5.6%	1.51
Totals:			4,072	27.00

Admixtures

<u>S-Number</u>	<u>Description</u>	<u>Dosage, oz/cwt</u>
S-122303	BASF Micro-Air	1.0
S-122302	BASF Glenium 7500	4.0
S-122225	BASF Master Life SRA 20	21.0

Plastic Properties

D-101112-01

Slump, in:	6.75
Unit Weight, lbs/cuft	150.8
Air Content (Calculated), %:	5.6
w/cm ratio:	0.38
Concrete Temperature, F:	74°

between 4.5 and 7.5 pps AD5 p8

AASHTO T 277 - Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration
Accelerated Cure

<u>Sample No.</u>	<u>Diameter, in.</u>	<u>Charge Passed, C</u>	<u>Corrected Charge, C</u>	<u>Qualitative Equivalent</u>	<u>Age, days</u>
D-101112-01	4.00	739	650	Very Low	28

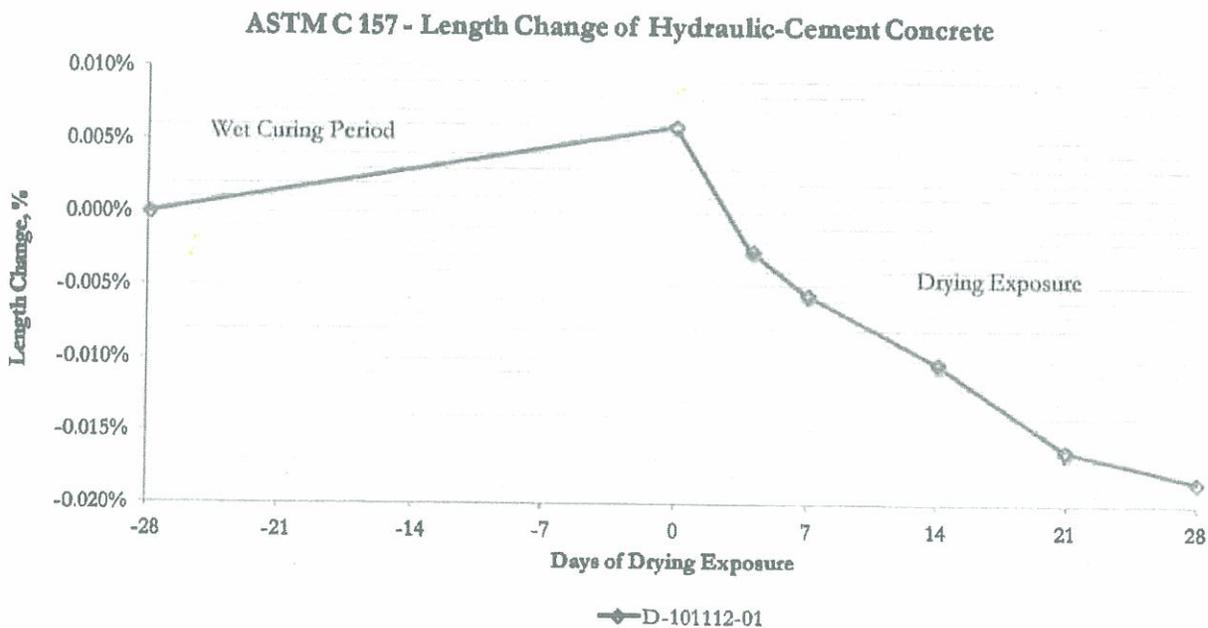
AASHTO T 277 - Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration
Standard Cure

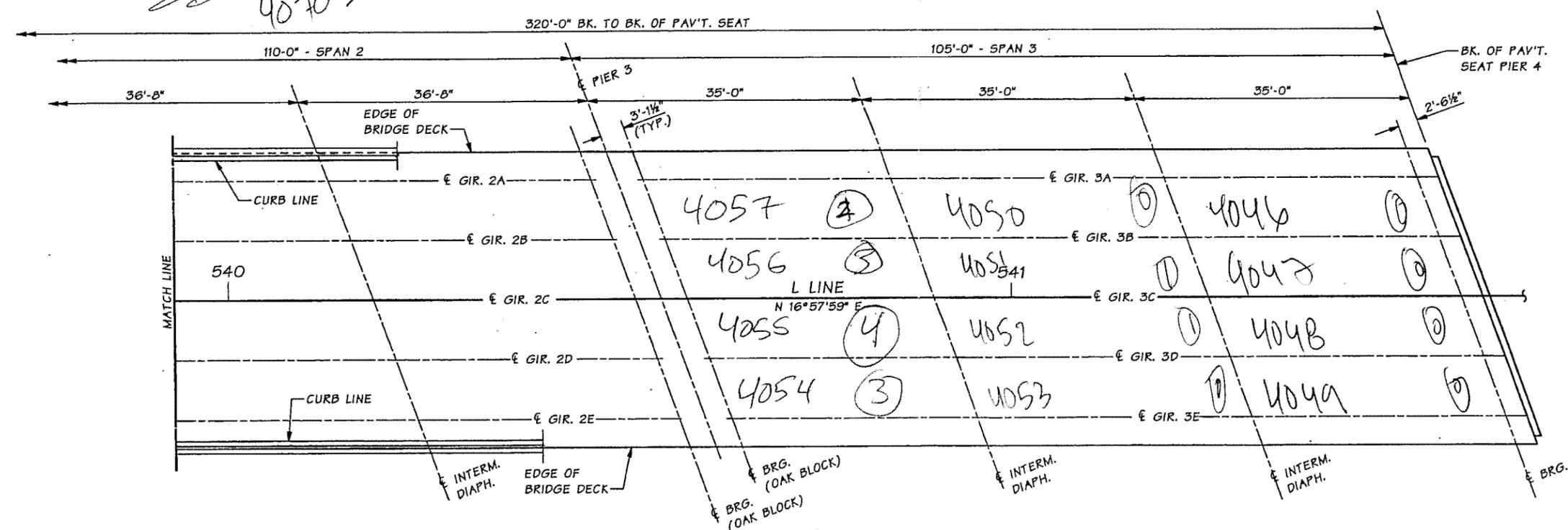
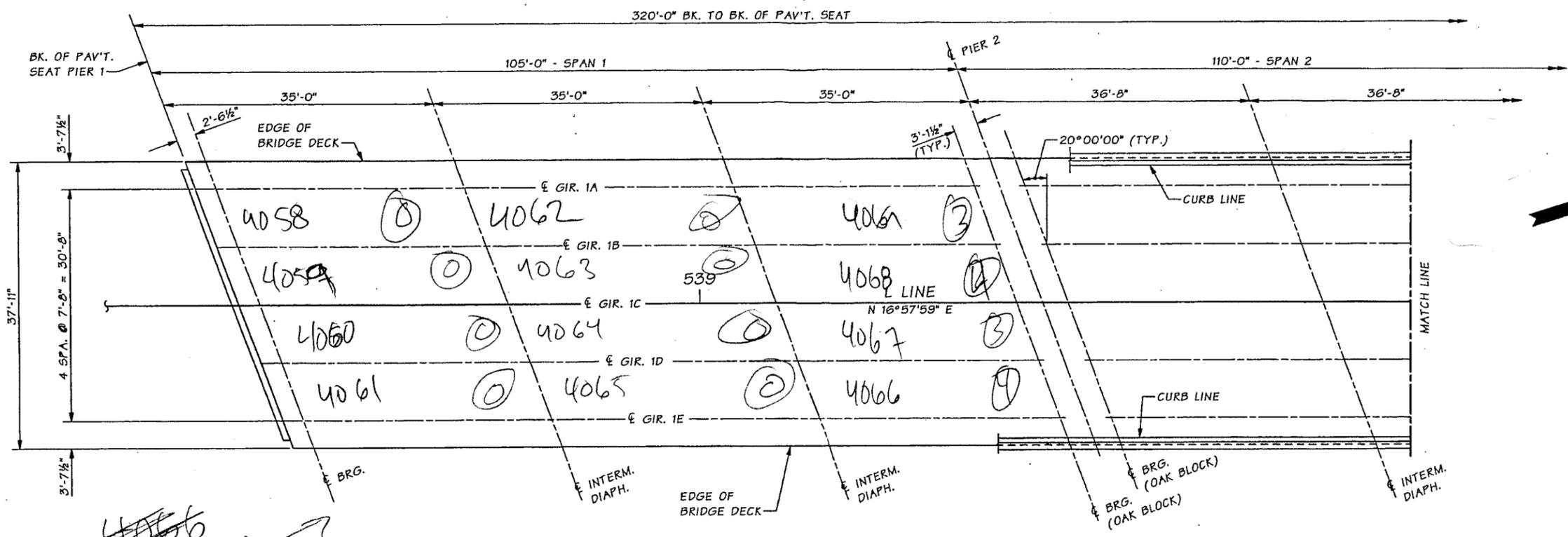
<u>Sample No.</u>	<u>Diameter, in.</u>	<u>Charge Passed, C</u>	<u>Corrected Charge, C</u>	<u>Qualitative Equivalent</u>	<u>Age, days</u>
D-101112-01	4.00	1,902	1,672	Low	28
	4.00	1,750	1,538	Low	56
	4.00	1,908	1,677	Low	56

ASTM C 157 Standard Test Method for Length Change of Hardened Hydraulic-Cement Mortar and Concrete

Material:	Concrete
Number of Specimens per Mixture:	4
Size of Specimens, in.:	Length: 10.0
	Width: 4.0
	Height: 4.0
Method of Consolidation:	4
Period of Moist Curing:	28-days
Drying Exposure Conditions:	23°C, 50% RH

Length Change	Reading	D-101112-01
	Initial	0.000%
	0-days dry	0.006%
	4-days dry	-0.003%
	7-days dry	-0.006%
	14-days dry	-0.010%
	21-days dry	-0.016%
	28-days dry	-0.018%





FRAMING PLAN

ALL LONGITUDINAL DIMENSIONS ARE ALONG L LINE UNLESS OTHERWISE SHOWN.

SR 105 FILE NO. SHEET SC28

Bridge Design Engr.	Khaleghi, B	M:\Y-Team\SR 105 BRIDGES\SMITH CREEK BR. NO. 105-3 REPLACEMENT\window files\FRAMING PLAN.wnd
Supervisor	Anderson, MW	
Designed By	Glassford, P	01/12
Checked By	Burnham, B	05/12
Detailed By	Nettle, J	01/12
Bridge Projects Engr.		
Prelim. Plan By		
Architect/Specialist		
DATE	REVISION	BY APPD

BRIDGE AND STRUCTURES OFFICE

6/13/12

Washington State Department of Transportation

SR 105
SMITH CREEK AND NORTH RIVER
REPLACE BRIDGES
SMITH CREEK BR. NO. 105-3
FRAMING PLAN

BRIDGE SHEET NO.	SC28
SHEET	114
OF	210
SHEETS	



Bridge #	105/3	Bridge Name	Smith Creek			Structure ID	0018345A	
Contract #	8345	Region	SW	Project Engineer	Lori Figone	Performance Deck Concrete?	YES	
Contractor	Scarsella Bros.		Concrete Supplier	Bayview Redi Mix, Inc		Deck Placement	12/17/2013	
Bridge Description	3-Span (105' / 110' / 105'), 5-WF42G Girders (320' bridge length), 2-Lanes (36' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

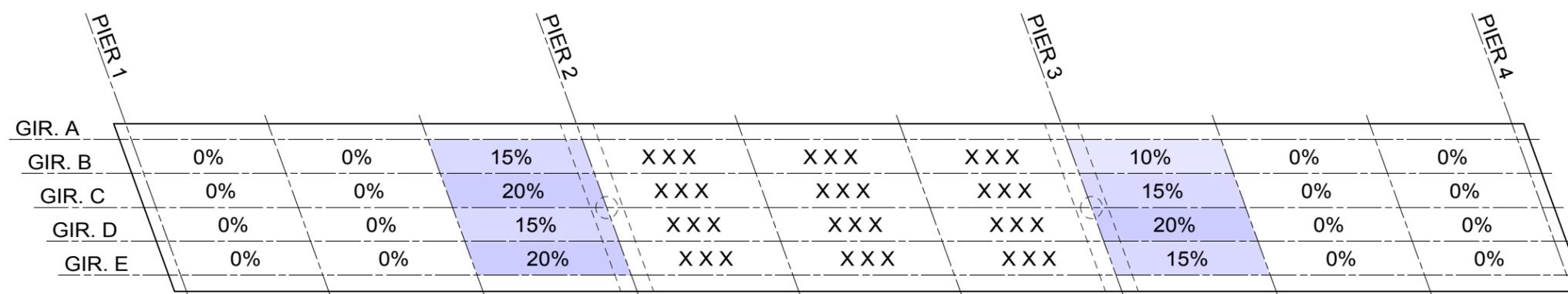
N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr} / N_{100} (rounded to the nearest 5%)

Avg. =	6%
Min. =	0%
Max. =	20%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	35.00	7.67	0	18	0%
1	1	B	C	35.00	7.67	0	18	0%
1	1	C	D	35.00	7.67	0	18	0%
1	1	D	E	35.00	7.67	0	18	0%
1	2	A	B	35.00	7.67	0	18	0%
1	2	B	C	35.00	7.67	0	18	0%
1	2	C	D	35.00	7.67	0	18	0%
1	2	D	E	35.00	7.67	0	18	0%
1	3	A	B	35.00	7.67	3	18	15%
1	3	B	C	35.00	7.67	4	18	20%
1	3	C	D	35.00	7.67	3	18	15%
1	3	D	E	35.00	7.67	4	18	20%
2	1	A	B	35.00	7.67	#N/A	18	#N/A
2	1	B	C	35.00	7.67	#N/A	18	#N/A
2	1	C	D	35.00	7.67	#N/A	18	#N/A
2	1	D	E	35.00	7.67	#N/A	18	#N/A
2	2	A	B	35.00	7.67	#N/A	18	#N/A
2	2	B	C	35.00	7.67	#N/A	18	#N/A
2	2	C	D	35.00	7.67	#N/A	18	#N/A
2	2	D	E	35.00	7.67	#N/A	18	#N/A
2	3	A	B	35.00	7.67	#N/A	18	#N/A
2	3	B	C	35.00	7.67	#N/A	18	#N/A
2	3	C	D	35.00	7.67	#N/A	18	#N/A
2	3	D	E	35.00	7.67	#N/A	18	#N/A
3	1	A	B	35.00	7.67	2	18	10%
3	1	B	C	35.00	7.67	3	18	15%
3	1	C	D	35.00	7.67	4	18	20%
3	1	D	E	35.00	7.67	3	18	15%
3	2	A	B	35.00	7.67	0	18	0%
3	2	B	C	35.00	7.67	1	18	5%
3	2	C	D	35.00	7.67	1	18	5%
3	2	D	E	35.00	7.67	0	18	0%
3	3	A	B	35.00	7.67	0	18	0%
3	3	B	C	35.00	7.67	0	18	0%
3	3	C	D	35.00	7.67	0	18	0%
3	3	D	E	35.00	7.67	0	18	0%



CRACKING INTENSITY ~ BRIDGE 105/3

100% = CRACK EVERY 2 FT.

X X X = CRACKS NOT COUNTED DUE TO LIMITED ACCESS

LESS CRACKING

MORE CRACKING

BRIDGE NUMBER	105/3
BRIDGE NAME	SMITH CREEK
INSPECTION DATE	5/7/2015
DECK CONCRETE	PERFORMANCE BASED

BRIDGE 6/8 (WILLAPA RIVER)

Bridge #	6/8	Bridge Name	Willapa River Bridge		Structure ID	0018464A	
Contract #	8464	Region	SW	Project Engineer	Colin Newell	Performance Deck Concrete?	YES
Contractor	Rotschy, Inc.		Concrete Supplier	Bayview Redi Mix, Inc		Deck Placement	12/24/13 & 12/30/13
Bridge Description	3-Span (75' / 125' / 75'), 4-WF58G Girders (275' bridge length), 2-Lanes (36' wide roadway)						



CONTENTS

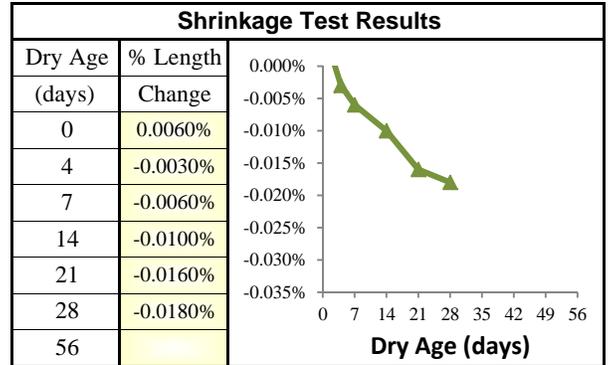
1. Layout Plan Sheet
2. Mix Design Summary
3. Concrete Mix Design Form
4. Concrete Test Results
5. Field Notes
6. Crack Summary
7. Crack Intensity Diagram



Bridge #	6/8	Bridge Name	Willapa River Bridge			Structure ID	0018464A
Contract #	8464	Region	SW	Project Engineer	Colin Newell	Performance Deck Concrete?	YES
Contractor	Rotschy, Inc.		Concrete Supplier	Bayview Redi Mix, Inc		Deck Placement	12/24/13 & 12/30/13
Bridge Description	3-Span (75' / 125' / 75'), 4-WF58G Girders (275' bridge length), 2-Lanes (36' wide roadway)						

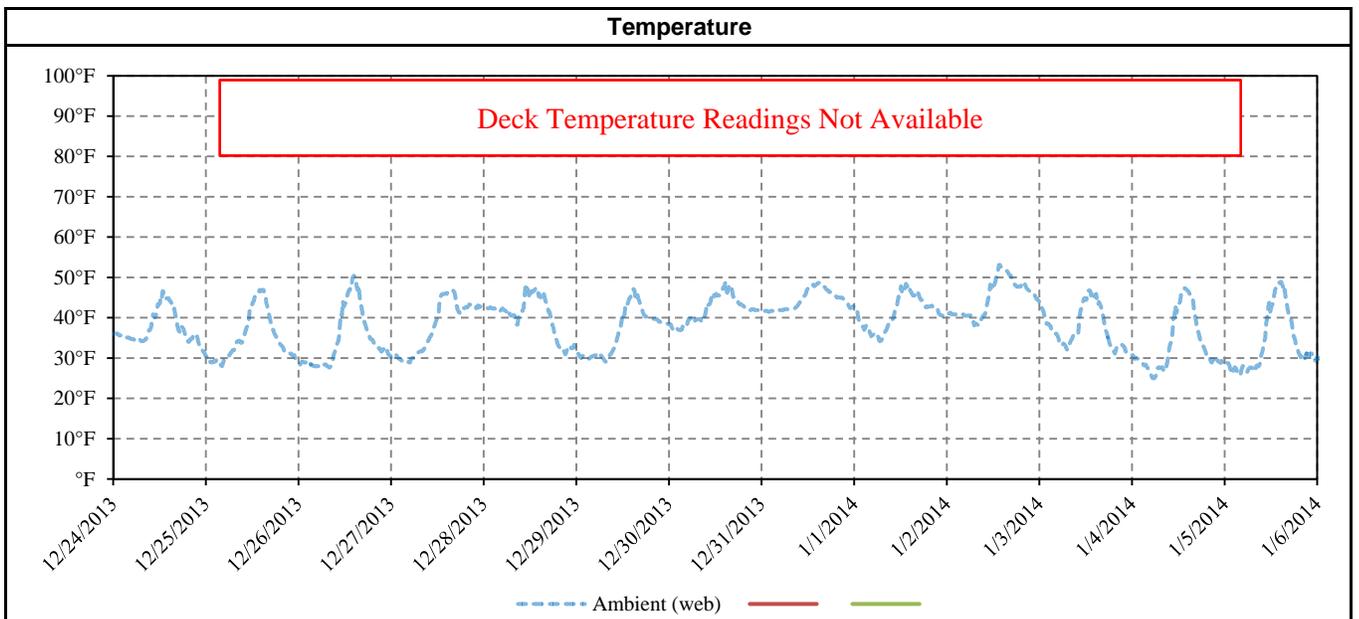
Mix Design (WSDOT Form 350-040)			
Water (max) =		230 lbs/cy	w/c = 0.38 max
Cementitious Materials	Lbs/cy	Source	Type, Class or Grade
cement	460	Ashgrove	Type I-II
fly ash	150	Laafarge	Type F
slag			
latex			
microsilica			
Concrete Admixtures	oz/cy	Manufacturer	Product
air entrainment	1-15	BASF	Micro Air
water reducer			
HR water reduce	20-30	BASF	Glenium 7500
set retarder			
shrink. reducer	120-140	BASF	Masterlife

Concrete Test Results		
compressive strength @ 28 days	5,691	psi
modulus of elasticity	4,012,122	psi
permeability @ 56 days	1,677	coulombs
mix design density	150.1	lb/cf



Aggregate					
	Comp. 1	Comp. 2	Comp. 3	Comp. 4	Comp. 5
WSDOT Pit #	PS-X-130	PS-X-130	PS-X-130		
Grading	#67	#4	Class II		
% Total	42.0%	20.0%	38.0%		
Lbs/cy	1350	650	1213		
ASR Mitigation	None Required				

Notes
Same Mix Design as:
* Bridge 101/31
* Bridge 101/44
* Bridge 105/4
* Bridge 105/3
if swell of concrete specimen is included, total change in length at 28 days drying is 240 microstrain (0.0060% + 0.0180%)



CMD #4

Concrete Mix Design

Contractor Rotschy Inc		Submitted By Bayview Redi-Mix, Inc	Date 05/24/2013
Concrete Supplier Bayview Redi Mix, Inc		Plant Location Raymond 041, Aberdeen 011	
Contract Number 13X307	Contract Name SR 6 Willapa River Bridge Replace Bridge		<i>8464</i>

This mix is to be used in the following Bid Item No(s): 42.18

Concrete Class: (check one only)

- 3000
 4000
 4000D^a
 4000P^a
 4000W
 Concrete Overlay
 Cement Concrete Pavement^d
 Other Shrinkage

Remarks: _____

Mix Design No. WSDT4DS130 Plant No. 041, 011

Cementitious Materials	Source	Type, Class or Grade	Sp. Gr.	Lbs/cy
Cement	Ashgrove, Seattle, WA	Type I-II ✓	3.15	460
Fly Ash ^a	Lafarge, Centralia, WA	Type F ✓	2.58	150
GGBFS (Slag)				
Latex				
Microsilica				

Concrete Admixtures	Manufacturer	Product	Type	Est. Range (oz/cy)
Air Entrainment	BASF Cleveland, OH	Micro Air		1-15
Water Reducer				
High-Range Water Reducer	BASF Cleveland, OH	Glenium 7500	F ✓	20-30
Set Retarder				
Other Shrinkage	BASF Cleveland, OH	Masterlife		120-140

Water (Maximum) 230 lbs/cy Is any of the water Recycled or Reclaimed? Yes No^e

Water Cementitious Ratio (Maximum) .38 Mix Design Density 150.1 lbs/cf^d

Design Performance	1	2	3	4	5	Average ^f
28 Day Compressive Strength (cylinders) psi	5,775	5,766	5,623	5,561	5,730	5,691
14 Day Flexural ^d Strength (beams) psi						

Agency Use Only (Check appropriate Box)

This Mix Design **MEETS CONTRACT SPECIFICATIONS** and may be used on the bid items noted above
 This Mix Design **DOES NOT MEET CONTRACT SPECIFICATIONS** and is being returned for corrections

Reviewed By: Flock / Cooper 8/15/2013
PE Signature Doc Date

CMD #4

6/6/2013

Aggregate Information

Concrete Aggregates	Component 1	Component 2	Component 3	Component 4	Component 5	Combined Gradation
WSDOT Pit No.	PS-X-130	PS-X130	PS-X-130			
WSDOT ASR 14-day Results (%) ^b	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No	
Grading ^c	AAASHTO #67	AAASHTO #4	Class II			
Percent of Total Aggregate	42	20	38			100%
Specific Gravity	2.825	2.825	2.747			
Lbs/cy (ssd)	1350	650	1213			

Percent Passing

2 inch	100	100	100			100
1-1/2 inch	100	100	100			100
1 inch	100	52	100			90 <i>90.4</i>
3/4 inch	93	1	100			77 <i>72.3</i>
1/2 inch	58	1	100			63 <i>62.6</i>
3/8 inch	30	1	100			51 <i>51.8</i>
No. 4	7	0	99			41 <i>40.6</i>
No. 8	0	0	78			30 <i>29.6</i>
No. 16	0	0	58			22 <i>22.0</i>
No. 30	0	0	35			13 <i>13.3</i>
No. 50	0	0	14			5 <i>5.3</i>
No. 100	0	0	3			1 <i>1.1</i>
No. 200	0	.1	1.1			0.5 <i>.4</i>

Fineness Modulus: 3.14 (Required for Class 2 Sand)

ASR Mitigation Method Proposed^b: Not Required for this Source

Notes:

- a Required for Class 4000D and 4000P mixes.
- b Alkali Silica Reactivity Mitigation is required for sources with expansions over 0.20% - Incidate method for ASR mitigation. For expansion of 0.21% - 0.45%, acceptable mitigation can be the use of low alkali cement or 25% type F fly ash. Any other proposed mitigation method or for pits with greater than 0.45% expansion, proof of mitigating measure, either ASTM C1260 / AASHTO T303 test results must be attached. If ASTM C 1293 testing has been submitted indicating 1-year expansion of 0.04% or less, mitigation is not required.
- c AASHTO No. 467, 57, 67, 7, 8; WSDOT Class 1, Class 2; or combined gradation. See Standard Specification 9-03.1.
- d Required for Cement Concrete Pavements.
- e Attach test results indicating conformance to Standard Specification 9-25.1.
- f Actual Average Strength as determined from testing or estimated from ACI 211.

TEST RESULTS

ASTM C 192 - Standard Practice for Making and Curing Concrete Test Specimens in the Laboratory

Concrete Mixture Proportions

4,000 PSI Mix

Trial Mix Results Calculated to 1yd³

D-101112-01

<u>S-Number</u>	<u>Description</u>	<u>SpG</u>	<u>Mass. lbs</u>	<u>Vol. Cuft</u>
S-121541	AG Seattle Type I/II	3.15	462	2.35
S-120817	Lafarge Centralia Class F	2.58	151	0.94
S-122202	Pit X-130 Fine Agg.	2.75	1,217	7.09
S-122204	Pit X-130 1.5 to 3/4 Agg.	2.83	652	3.69
S-122203	Pit X-130 3/4 to No. 4 Agg.	2.83	1,357	7.68
---	Overland Park Municipal	1.00	233	3.73
-	Air	-	<u>5.6%</u>	<u>1.51</u>
Totals:			4,072	27.00

Admixtures

<u>S-Number</u>	<u>Description</u>	<u>Dosage. oz/cwt</u>
S-122303	BASF Micro-Air	1.0
S-122302	BASF Glenium 7500	4.0
S-122225	BASF Master Life SRA 20	21.0

Plastic Properties

D-101112-01

Slump, in:	6.75
Unit Weight, lbs/cuft:	150.8
Air Content (Calculated), %:	5.6
w/cm ratio:	0.38
Concrete Temperature, F:	74°

AASHTO T 277 - Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration
Accelerated Cure

<u>Sample No.</u>	<u>Diameter. in.</u>	<u>Charge Passed. C</u>	<u>Corrected Charge. C</u>	<u>Qualitative Equivalent</u>	<u>Age. days</u>
D-101112-01	4.00	739	650	Very Low	28

AASHTO T 277 - Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration
Standard Cure

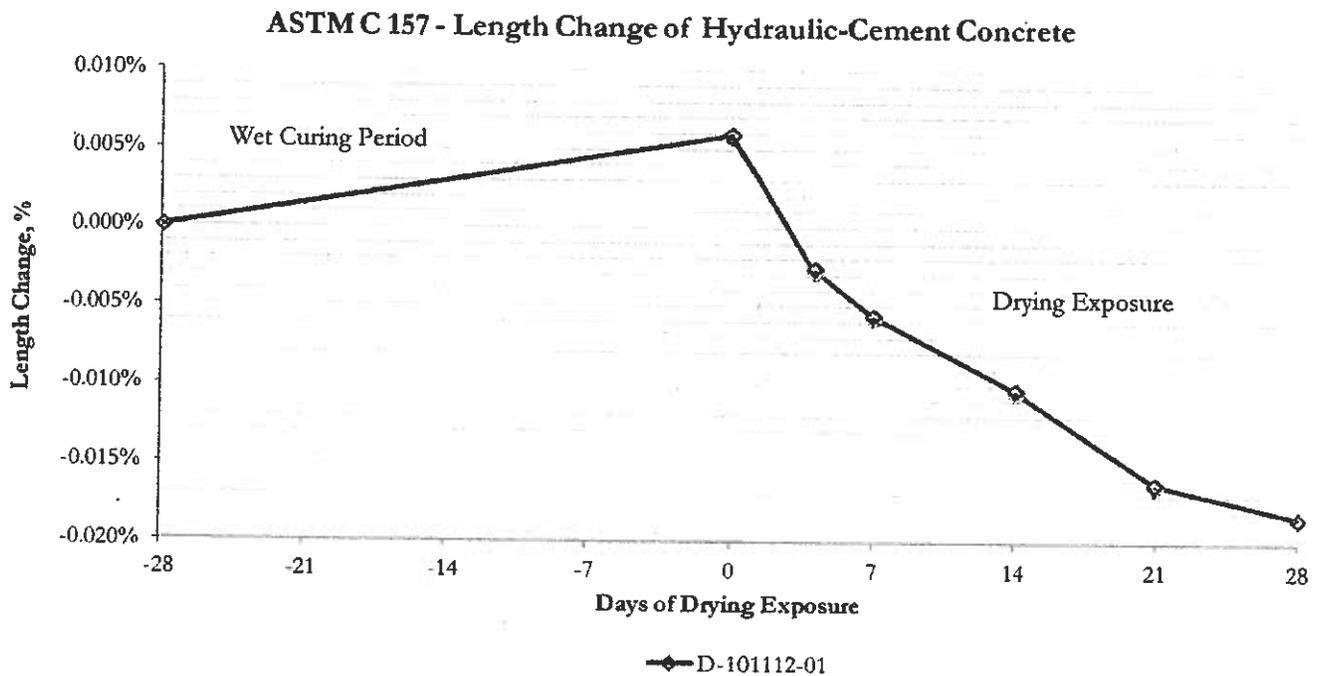
<u>Sample No.</u>	<u>Diameter. in.</u>	<u>Charge Passed. C</u>	<u>Corrected Charge. C</u>	<u>Qualitative Equivalent</u>	<u>Age. days</u>
D-101112-01	4.00	1,902	1,672	Low	28
	4.00	1,750	1,538	Low	56
	4.00	1,908	1,677	Low	56

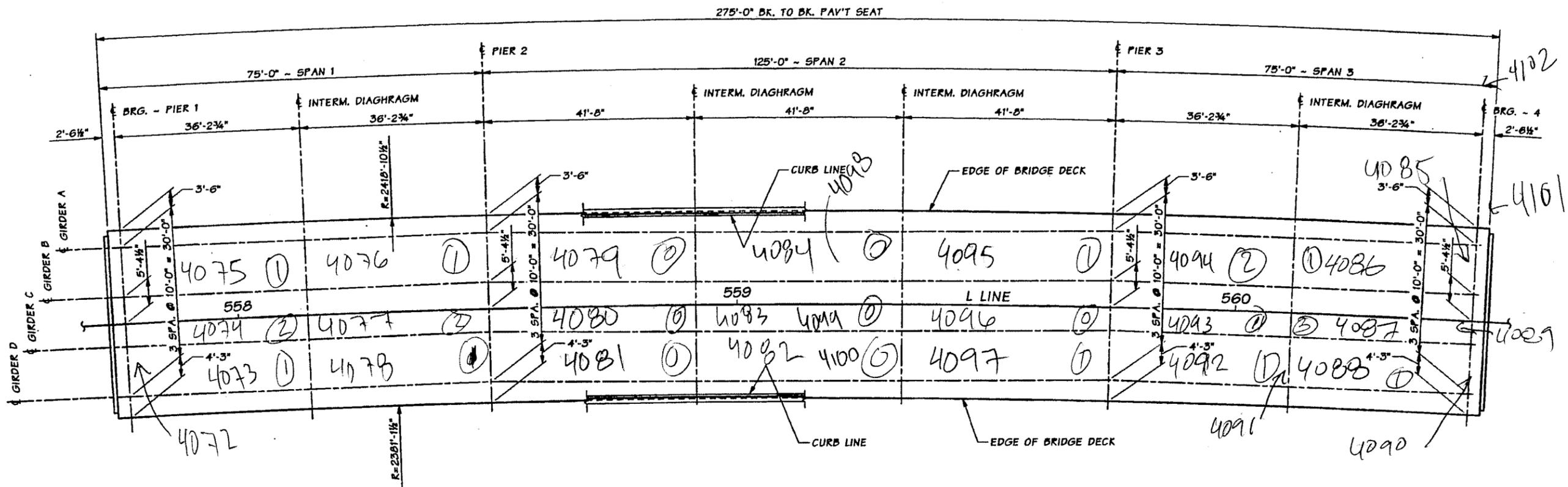
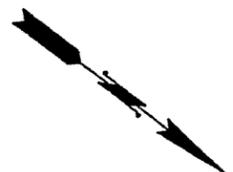
ASTM C 157 Standard Test Method for Length Change of Hardened Hydraulic-Cement Mortar and Concrete

Material:	Concrete
Number of Specimens per Mixture:	4
Size of Specimens, in.:	Length: 10.0
	Width: 4.0
	Height: 4.0
Method of Consolidation:	4
Period of Moist Curing:	28-days
Drying Exposure Conditions:	23°C, 50% RH

Length Change

<u>Reading</u>	<u>D-101112-01</u>
Initial	0.000%
0-days dry	0.006%
4-days dry	-0.003%
7-days dry	-0.006%
14-days dry	-0.010%
21-days dry	-0.016%
28-days dry	-0.018%





FRAMING PLAN

ALL DIMENSIONS ARE NORMAL TO OR ALONG THE L LINE,
BACK OF PAVEMENT SEAT & PIER UNLESS OTHERWISE SHOWN.

SR 6 FILE NO. 7006 SHEET 23

Bridge Design Engr.	Khalleghi, B	M:\X-Team\SR6 WILLAPA RIVER BR 6-8 REPL>window files\FRAMING PLAN.wid			
Supervisor	Khalleghi, B	REVISION	DATE	BY	APPD
Designed By	Hsieh, JC	04/12			
Checked By	Sawahata, D	03/13			
Detaild By	McCarthy, DJ	04/12			
Bridge Projects Engr.					
Prelim. Plan By					
Architect/Specialist					



BRIDGE AND STRUCTURES OFFICE



Washington State Department of Transportation

SR 6
WILLAPA RIVER BRIDGE
REPLACE BRIDGE
WILLAPA RIVER (LILLY WHEATON) BR NO 6/8 REPLACEMENT
FRAMING PLAN

BRIDGE SHEET NO. 23
PAGE 95 OF 122 SHEETS



Bridge #	6/8	Bridge Name	Willapa River Bridge			Structure ID	0018464A
Contract #	8464	Region	SW	Project Engineer	Colin Newell	Performance Deck Concrete?	YES
Contractor	Rotschy, Inc.		Concrete Supplier	Bayview Redi Mix, Inc		Deck Placement	12/24/13 & 12/30/13
Bridge Description	3-Span (75' / 125' / 75'), 4-WF58G Girders (275' bridge length), 2-Lanes (36' wide roadway)						

L = length between diaphragms (or length of "bay")

S = girder spacing

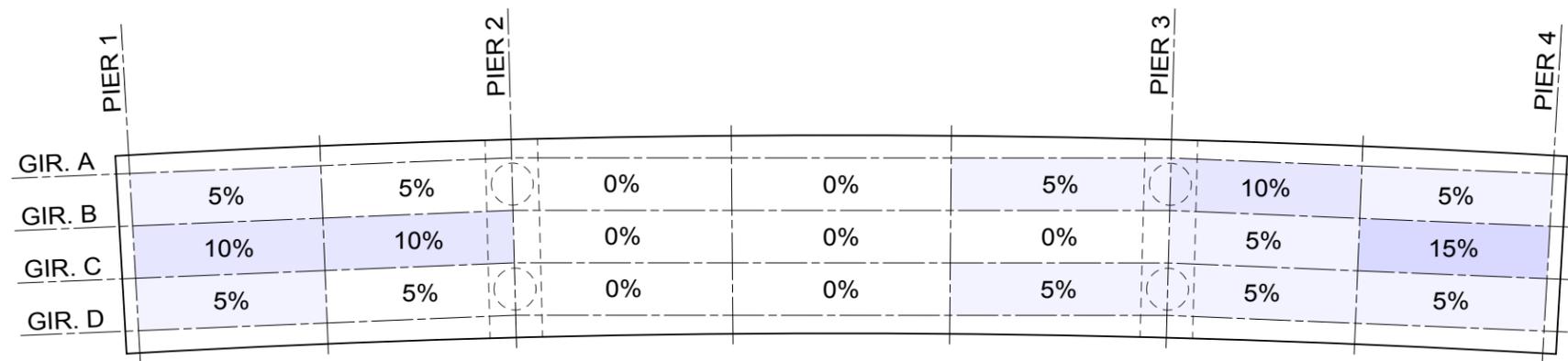
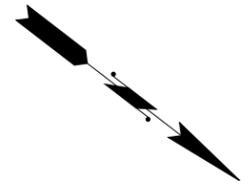
N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	5%
Min. =	0%
Max. =	15%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	36.23	10.00	1	18	5%
1	1	B	C	36.23	10.00	2	18	10%
1	1	C	D	36.23	10.00	1	18	5%
1	2	A	B	36.23	10.00	1	18	5%
1	2	B	C	36.23	10.00	2	18	10%
1	2	C	D	36.23	10.00	1	18	5%
2	1	A	B	41.67	10.00	0	21	0%
2	1	B	C	41.67	10.00	0	21	0%
2	1	C	D	41.67	10.00	0	21	0%
2	2	A	B	41.67	10.00	0	21	0%
2	2	B	C	41.67	10.00	0	21	0%
2	2	C	D	41.67	10.00	0	21	0%
2	3	A	B	41.67	10.00	1	21	5%
2	3	B	C	41.67	10.00	0	21	0%
2	3	C	D	41.67	10.00	1	21	5%
2	4	A	B	36.23	10.00	2	18	10%
2	4	B	C	36.23	10.00	1	18	5%
2	4	C	D	36.23	10.00	1	18	5%
2	5	A	B	36.23	10.00	1	18	5%
2	5	B	C	36.23	10.00	3	18	15%
2	5	C	D	36.23	10.00	1	18	5%



CRACKING INTENSITY ~ BRIDGE 6/8

100% = CRACK EVERY 2 FT.



BRIDGE NUMBER	6/8
BRIDGE NAME	WILLAPA RIVER
INSPECTION DATE	5/7/2015
DECK CONCRETE	PERFORMANCE BASED

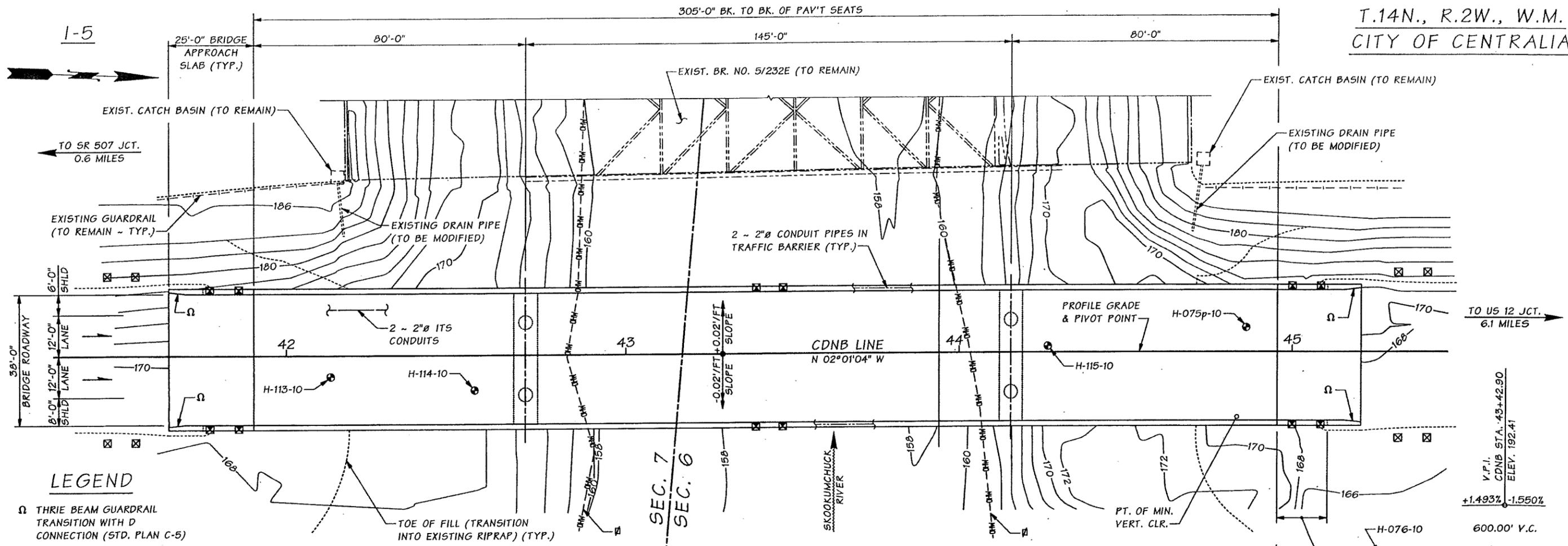
BRIDGE 5/232NCD (SKOOKUMCHUCK RIVER NBCD)

Bridge #	5/232NCD	Bridge Name	Skookumchuck River NBCD		Structure ID	0018272A	
Contract #	8272	Region	SW	Project Engineer	Colin Newell	Performance Deck Concrete?	YES
Contractor	Cascade Bridge		Concrete Supplier	Miles Sand & Gravel	Deck Placement	2/14/2013	
Bridge Description	3-Span (80' / 145' / 80'), 5-WF66G Girders (305' bridge length), 2-Lanes (38' wide roadway)						



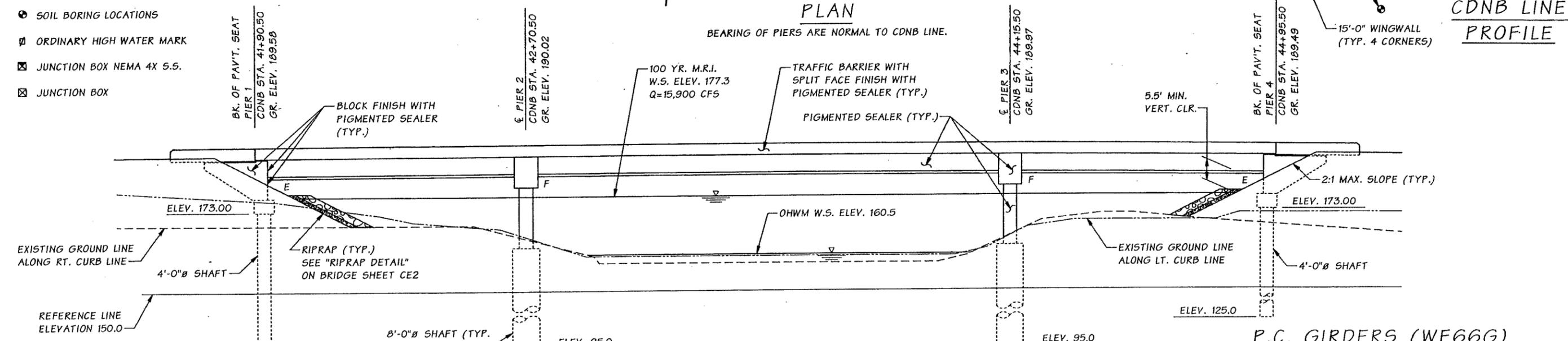
CONTENTS

1. Layout Plan Sheet
2. Mix Design Summary
3. Concrete Mix Design Form
4. Concrete Test Results
5. Field Notes
6. Crack Summary
7. Crack Intensity Diagram



PLAN

BEARING OF PIERS ARE NORMAL TO CDNB LINE.



ELEVATION

GRADE ELEVATIONS SHOWN ARE FINISH GRADES AT TOP OF BRIDGE DECK ON CDNB LINE AND ARE EQUAL TO PROFILE GRADE. SEE STD. PLAN A-50.10 FOR EMBANKMENT DETAILS AT BRIDGE ENDS.

NOTE: 500 YR M.R.I. W.S. ELEV. 180.0 Q = 18,700 CFS

P.C. GIRDERS (WF66G)
CONT. FOR LL
LOADING: HL-93

LEGEND

- Ω THRIE BEAM GUARDRAIL TRANSITION WITH D CONNECTION (STD. PLAN C-5)
- SOIL BORING LOCATIONS
- ⊕ ORDINARY HIGH WATER MARK
- ⊠ JUNCTION BOX NEMA 4X 5.5.
- ⊞ JUNCTION BOX

DATUM

NAVD 88

SR 5 FILE NO. 7481 SHEET CE1

Bridge Design Engr. Khaileghi, B	M:\X-Team\MELLEN TO BLAKESLEE JCT\CDNB BR\window files\LAYOUT.WND	REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
Supervisor Stoddard, RB		10	WASH.			
Designed By PMN/MCF	03/12					
Checked By JCH/LHT	03/12					
Detailed By McCarthy, DJ	10/11					
Bridge Projects Engr. Lewis, RA	06/10					
Prelim. Plan By Wei, J	03/10					
Architect/Specialist PDK/BSA/GAW	04/10					

BRIDGE AND STRUCTURES OFFICE



Washington State Department of Transportation

3/7/12

I-5
MELLEN STREET TO
BLAKESLEE JUNCTION - STAGE 1
SKOOKUMCHUCK RIVER BRIDGE NO. 5/232NCD
LAYOUT

BRIDGE SHEET NO.	CE1
SHEET	220
OF	472
SHEETS	

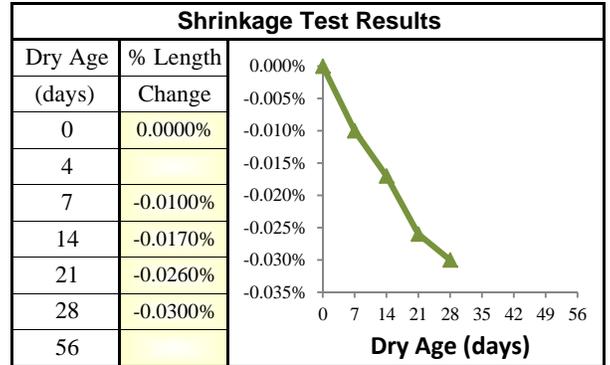
C.S. 2101 ~ PROJ. NO. TA4572D ~ SOUTHWEST REGION ~ I-5 ~ MELLEN TO BLAKESLEE JCT. ~ NORTHBOUND CD BRIDGE ~ NEW STRUCTURE



Bridge #	5/232NCD	Bridge Name	Skookumchuck River NBCD		Structure ID	0018272A	
Contract #	8272	Region	SW	Project Engineer	Colin Newell	Performance Deck Concrete?	YES
Contractor	Cascade Bridge		Concrete Supplier	Miles Sand & Gravel		Deck Placement	2/14/2013
Bridge Description	3-Span (80' / 145' / 80'), 5-WF66G Girders (305' bridge length), 2-Lanes (38' wide roadway)						

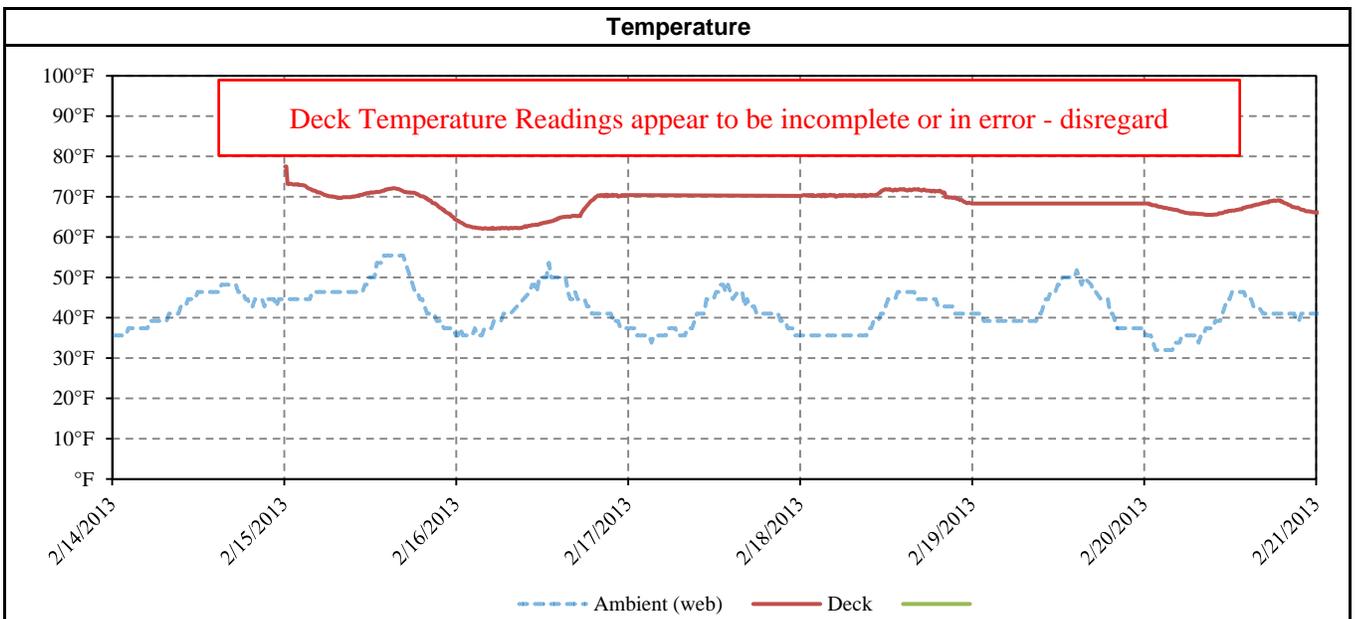
Mix Design (WSDOT Form 350-040)			
Water (max) =		223 lbs/cy	w/c = 0.40 max
Cementitious Materials	Lbs/cy	Source	Type, Class or Grade
cement	464	Lafarge	Type I-II
fly ash	116	Lafarge	Type F
slag			
latex			
microsilica			
Concrete Admixtures	oz/cy	Manufacturer	Product
air entrainment	1-15	BASF	MB-AE-90
water reducer			
HR water reduce	23-40	BASF	Glenium 7500
set retarder			
shrink. reducer	32	BASF	MasterLife SRA

Concrete Test Results		
compressive strength @ 28 days	5,507	psi
modulus of elasticity		psi
permeability @ 56 days	1,350	coulombs
mix design density	145.5	lb/cf



Aggregate					
	Comp. 1	Comp. 2	Comp. 3	Comp. 4	Comp. 5
WSDOT Pit #	B-329	B-329	B-329	B-333	
Grading	No. 4	No. 57	No. 8	Class 2	
% Total	15.4%	33.3%	16.0%	35.3%	
Lbs/cy	480	1040	500	1100	
ASR Mitigation	None Required				

Notes
Same Mix Design as:
* Bridge 5/232SCD
* Bridge 5/234W
Very Similar Mix Design as:
* Bridge 5/229



Contractor Cascade Bridge		Submitted By	Date 1-28-2013
Concrete Supplier Miles Sand & Gravel		Plant Location Rochester	
Contract Number 8272	Contract Name Blakeslee Jct to Mellen St		

This mix is to be used in the following Bid Item No(s): 92.18.01, 93.16.01, 94.17.01

Concrete Class: (check one only)

- 3000
 4000
 4000^a
 4000^aP
 4000W
 Concrete Overlay
 Cement Concrete Pavement^d
 Other Shrinkage Reducer

Remarks: _____

Mix Design No. 0444AFL2 Plant No. 222

Cementitious Materials	Source	Type, Class or Grade	Sp. Gr.	Lbs/cy
Cement	Lafarge	I-II	3.15	464
Fly Ash ^a	Lafarge	F	2.54	116
GGBFS (Slag)				
Latex				
Microsilica				

Concrete Admixtures	Manufacturer	Product	Type	Est. Range (oz/cy)
Air Entrainment	BASF	MB-AE-90		1-15
Water Reducer				
High-Range Water Reducer	BASF	Glenium 7500	F	23-40
Set Retarder				
Other Shrinkage Reducer	BASF	MasterLife SRA		32

Water (Maximum) 233 lbs/cy Is any of the water Recycled or Reclaimed? Yes^e No

Water Cementitious Ratio (Maximum) 0.40 Mix Design Density 145.5 lbs/cf^d

Design Performance	1	2	3	4	5	Average ^f
28 Day Compressive Strength (cylinders) psi						5,507
14 Day Flexural ^d Strength (beams) psi						

Agency Use Only (Check appropriate Box)

This Mix Design **MEETS CONTRACT SPECIFICATIONS** and may be used on the bid items noted above
 This Mix Design **DOES NOT MEET CONTRACT SPECIFICATIONS** and is being returned for corrections

Reviewed By: _____ PE Signature

RECEIVED

Aggregate Information

Concrete Aggregates	Component 1	Component 2	Component 3	Component 4	Component 5	Combined Gradation
WSDOT Pit No.	B-329	B-329	B-329	B-333		
WSDOT ASR 14-day Results (%) ^b	<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No				
Grading ^c	4	57	8	Class 2		
Percent of Total Aggregate						100%
Specific Gravity	2.71	2.69	2.68	2.65		
Lbs/cy (ssd)	480	1040	500	1100		

Percent Passing

2 inch	100	100	100	100		100
1-1/2 inch	100	100	100	100		100
1 inch	32.6	100	100	100		89.6
3/4 inch	1.6	80.0	100	100		78.2
1/2 inch	0.4	30.1	100	100		61.4
3/8 inch	0.2	7.8	88.6	100		52.1
No. 4	0.1	0.3	22.4	99.4		38.8
No. 8	0.1	0.2	1.4	90.2		32.1
No. 16	0.1	0.1	0.2	70		24.8
No. 30	0.1	0.1	0.2	44.1		15.6
No. 50	0.1	0.1	0.2	20		7.1
No. 100	0.1	0.1	0.2	6		2.2
No. 200	0.1	0.1	0.2	1.7		0.7

Fineness Modulus: 2.70 (Required for Class 2 Sand)

ASR Mitigation Method Proposed^b: _____

Notes:

- a Required for Class 4000D and 4000P mixes.
- b Alkali Silica Reactivity Mitigation is required for sources with expansions over 0.20% - Incidate method for ASR mitigation. For expansion of 0.21% - 0.45%, acceptable mitigation can be the use of low alkali cement or 25% type F fly ash. Any other proposed mitigation method or for pits with greater than 0.45% expansion, proof of mitigating measure, either ASTM C1260 / AASHTO T303 test results must be attached. If ASTM C 1293 testing has been submitted indicating 1-year expansion of 0.04% or less, mitigation is not required.
- c AASHTO No. 467, 57, 67, 7, 8; WSDOT Class 1, Class 2; or combined gradation. See Standard Specification 9-03.1.
- d Required for Cement Concrete Pavements.
- e Attach test results indicating conformance to Standard Specification 9-25.1.
- f Actual Average Strength as determined from testing or estimated from ACI 211.

RECEIVED

JAN 29 2017



Lafarge North America Concrete Lab
5400 W Marginal Way SW
Seattle, WA. 98106

Report To: Miles Sand & Gravel
Attention: Quality Control Personnel

Date: May 25, 2012

Subject: Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration: ASTM C-1202

Tested Materials: Date Sampled: March 2012
Mix Design: WSDOT Valley HPC

Curing: ASTM C-1202 Standard Cure

Results:

<u>Age</u>	<u>Coulombs</u>
56 day	1350
90 day	920

*The ASTM C-1202 procedure was followed.

The test result is only valid if the aggregate(s) sample(s) is(are) representative of the current production and it is to be noted that Lafarge has no knowledge of the representatives of the sample received for testing. Also, material quality can vary with different locations in a quarry. It is recommended that testing be carried out on an annual basis or more frequently if a variation in stone quality is suspected.

Although the Lafarge North America Seattle Concrete Lab. applies state-of-the-art test methods, Lafarge North America, and its affiliates (Lafarge) can not guarantee the results shown above and shall assume no liability whatsoever for any errors in such results and for the consequence of such errors.

Rob Shogren, P.E.
Technical Service Engineer
Lafarge North America

RECEIVED
JAN 29 2012
DEPT. OF TRANSPORTATION CHEHALIS ENGINEERING



Lafarge North America Concrete Lab
5400 W Marginal Way SW
Seattle, WA. 98106

Report To: Miles Sand & Gravel
Attention: Quality Control Personnel

Date: May 25, 2012

Subject: Length Change of Hardened Hydraulic-Cement Concrete Using Procedures of ASTM C-157

Tested Materials: Date Sampled: March, 2012
Source of Aggregates: Miles Sand & Gravel

Mix Design: WSDOT HPC

Results: Slump: 4.5" Specimen Size: 4"x4"x10"
Temp: 64°F Consolidation: Rodding
Initial Cure: Lime water submersion (28 day initial cure)

<u>Age (Days) After Initial Cure</u>	<u>Percent Length Change (Average of 3)</u>
7	0.010
14	0.017
21	0.026
28 (final)	0.030

*The ASTM C-157 procedure was followed.

The test result is only valid if the aggregate(s) sample(s) is(are) representative of the current production and it is to be noted that Lafarge has no knowledge of the representatives of the sample received for testing. Also, material quality can vary with different locations in a quarry. It is recommended that testing be carried out on an annual basis or more frequently if a variation in stone quality is suspected.

Although the Lafarge North America Seattle Concrete Lab. applies state-of-the-art test methods, Lafarge North America, and its affiliates (Lafarge) can not guarantee the results shown above and shall assume no liability whatsoever for any errors in such results and for the consequence of such errors.

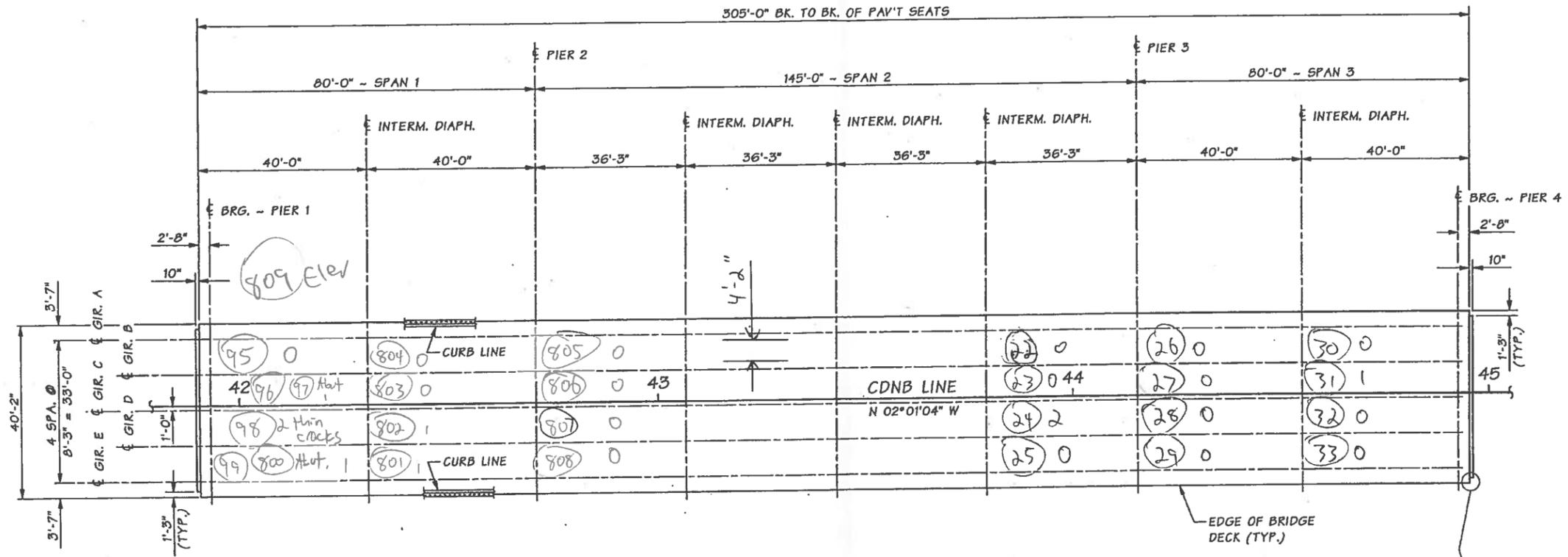
Rob Shogren, P.E.
Technical Service Engineer
Lafarge North America

RECEIVED

JAN 29 2012

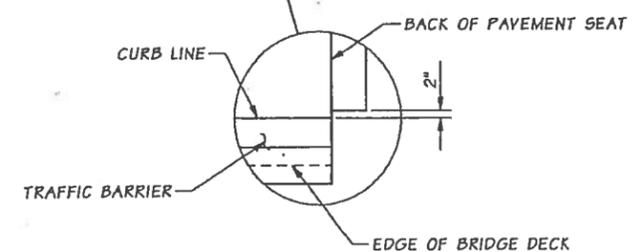
DEPT. OF TRANSPORTATION CHEHALIS ENGINEERING

3795-3809
3822-3833



FRAMING PLAN

BEARING OF PIERS ARE NORMAL TO CDNB LINE.



NOTE:
OTHERS CORNERS SIMILAR.

SR 5 FILE NO. 7481 SHEET CE20

Bridge Design Engr.	Khalighi, B	M:\X-Team\MELLEN TO BLAKESLEE JCT\CDNB BR>window files\FRAMING PLAN.WND		REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
Supervisor	Stoddard, RB			10	WASH.			
Designed By	Nash, PH	05/11		JOB NUMBER				
Checked By	Hsieh, JC	03/12		12X304				
Detail By	McCarthy, DJ	10/11						
Bridge Projects Engr.								
Prelim. Plan By								
Architect/Specialist		DATE	REVISION	BY	APPD			



BRIDGE AND STRUCTURES OFFICE



I-5
MELLEN STREET TO
BLAKESLEE JUNCTION - STAGE 1
SKOOKUMCHUCK RIVER BRIDGE NO. 5/232NCD
FRAMING PLAN

BRIDGE SHEET NO.
CE20
SHEET 239
OF 472
SHEETS



Bridge #	5/232NCD	Bridge Name	Skookumchuck River NBCD			Structure ID	0018272A	
Contract #	8272	Region	SW	Project Engineer	Colin Newell	Performance Deck Concrete?	YES	
Contractor	Cascade Bridge		Concrete Supplier	Miles Sand & Gravel		Deck Placement	2/14/2013	
Bridge Description	3-Span (80' / 145' / 80'), 5-WF66G Girders (305' bridge length), 2-Lanes (38' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg =	2%
Min. =	0%
Max. =	10%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	40.00	8.25	0	20	0%
1	1	B	C	40.00	8.25	1	20	5%
1	1	C	D	40.00	8.25	2	20	10%
1	1	D	E	40.00	8.25	1	20	5%
1	2	A	B	40.00	8.25	0	20	0%
1	2	B	C	40.00	8.25	0	20	0%
1	2	C	D	40.00	8.25	1	20	5%
1	2	D	E	40.00	8.25	1	20	5%
2	1	D	E	36.25	8.25	0	18	0%
2	1	D	E	36.25	8.25	0	18	0%
2	1	D	E	36.25	8.25	0	18	0%
2	1	D	E	36.25	8.25	0	18	0%
2	2	D	E	36.25	8.25	#N/A	18	#N/A
2	2	D	E	36.25	8.25	#N/A	18	#N/A
2	2	D	E	36.25	8.25	#N/A	18	#N/A
2	2	D	E	36.25	8.25	#N/A	18	#N/A
2	3	D	E	36.25	8.25	#N/A	18	#N/A
2	3	D	E	36.25	8.25	#N/A	18	#N/A
2	3	D	E	36.25	8.25	#N/A	18	#N/A
2	3	D	E	36.25	8.25	#N/A	18	#N/A
2	4	D	E	36.25	8.25	0	18	0%
2	4	D	E	36.25	8.25	0	18	0%
2	4	D	E	36.25	8.25	2	18	10%
2	4	D	E	36.25	8.25	0	18	0%
3	1	D	E	40.00	8.25	0	20	0%
3	1	D	E	40.00	8.25	0	20	0%
3	1	D	E	40.00	8.25	0	20	0%
3	1	D	E	40.00	8.25	0	20	0%
3	2	D	E	40.00	8.25	0	20	0%
3	2	D	E	40.00	8.25	1	20	5%
3	2	D	E	40.00	8.25	0	20	0%



	PIER 1			PIER 2			PIER 3		PIER 4
GIR. A									
GIR. B	0%	0%	0%	XXX	XXX	0%	0%	0%	
GIR. C	5%	0%	0%	XXX	XXX	0%	0%	5%	
GIR. D	10%	5%	0%	XXX	XXX	10%	0%	0%	
GIR. E	5%	5%	0%	XXX	XXX	0%	0%	0%	

CRACKING INTENSITY ~ BRIDGE 5/232NCD

100% = CRACK EVERY 2 FT.

X X X = CRACKS NOT COUNTED DUE TO LIMITED ACCESS

LESS CRACKING

MORE CRACKING

BRIDGE NUMBER	5/232NCD
BRIDGE NAME	SKOOKUMCHUCK RIVER NBCD
INSPECTION DATE	4/8/2015
DECK CONCRETE	PERFORMANCE BASED

BRIDGE 5/232SCD (SKOOKUMCHUCK RIVER SBCD)

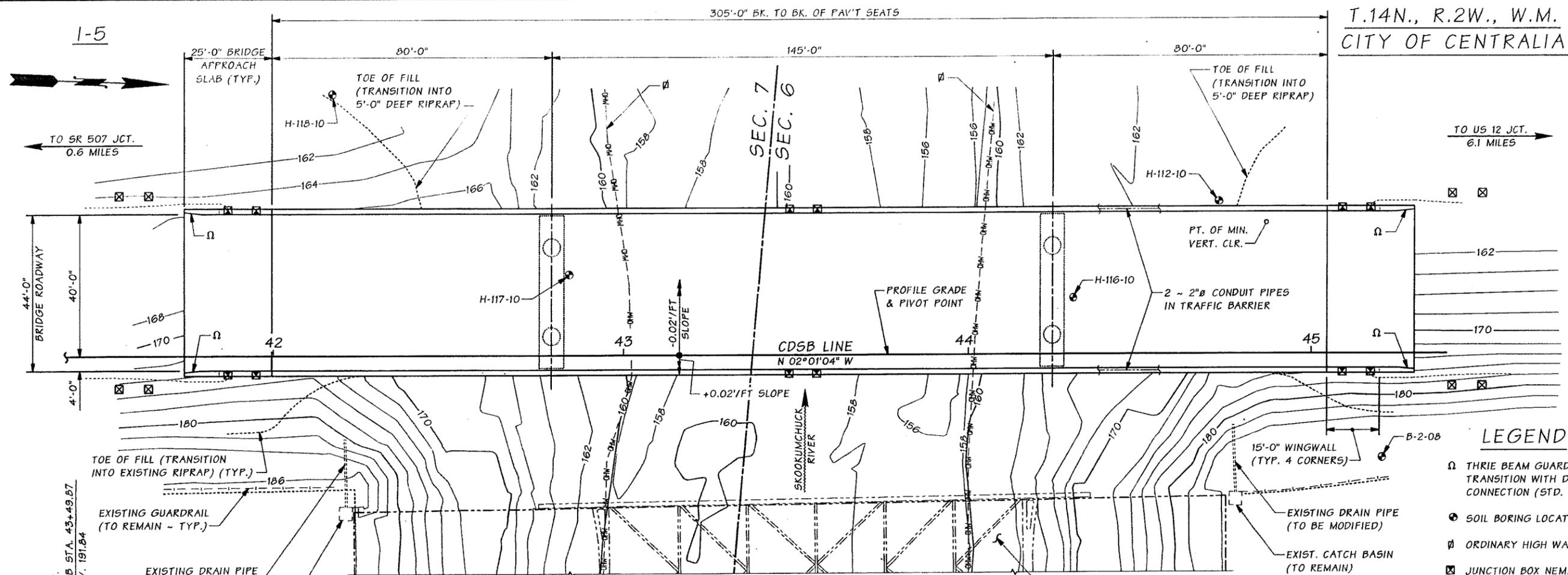
Bridge #	5/232SCD	Bridge Name	Skookumchuck River SBCD		Structure ID	0018272A	
Contract #	8272	Region	SW	Project Engineer	Colin Newell	Performance Deck Concrete?	YES
Contractor	Cascade Bridge		Concrete Supplier	Miles Sand & Gravel		Deck Placement	3/2/2013
Bridge Description	3-Span (80' / 145' / 80'), 5-WF66G Girders (305' bridge length), 2-Lanes (38' wide roadway)						



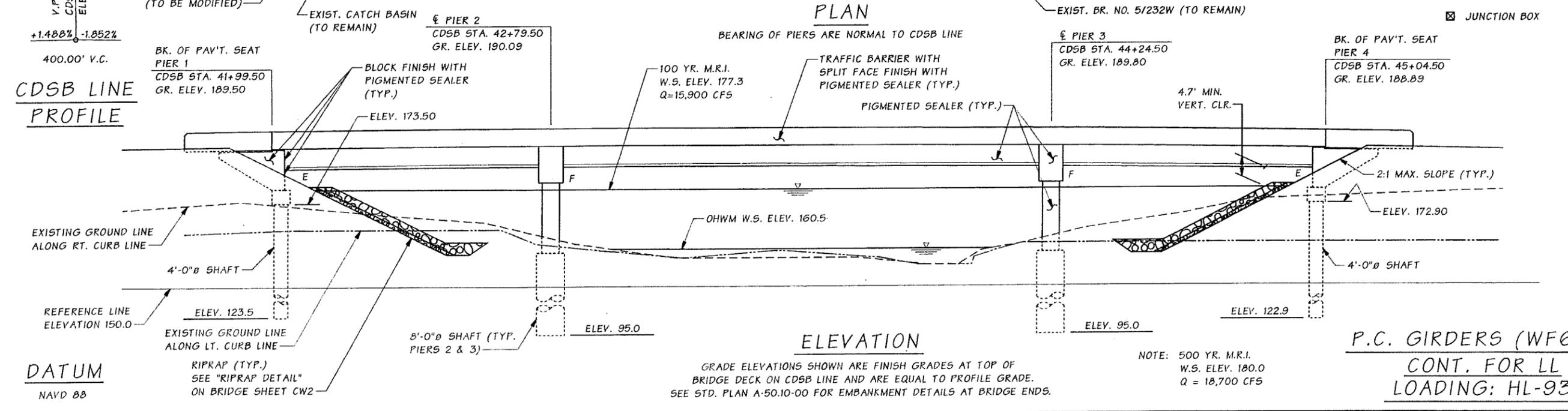
CONTENTS

1. Layout Plan Sheet
2. Mix Design Summary
3. Concrete Mix Design Form
4. Concrete Test Results
5. Field Notes
6. Crack Summary
7. Crack Intensity Diagram

T.14N., R.2W., W.M.
CITY OF CENTRALIA



- LEGEND**
- Ω THRIE BEAM GUARDRAIL TRANSITION WITH D CONNECTION (STD. PLAN C-5)
 - SOIL BORING LOCATIONS
 - ⊕ ORDINARY HIGH WATER MARK
 - ⊠ JUNCTION BOX NEMA 4X 5.5.
 - ⊞ JUNCTION BOX



CDSB LINE PROFILE

DATUM
NAVD 88

ELEVATION
GRADE ELEVATIONS SHOWN ARE FINISH GRADES AT TOP OF BRIDGE DECK ON CDSB LINE AND ARE EQUAL TO PROFILE GRADE. SEE STD. PLAN A-50.10-00 FOR EMBANKMENT DETAILS AT BRIDGE ENDS.

NOTE: 500 YR. M.R.I.
W.S. ELEV. 180.0
Q = 18,700 CFS

**P.C. GIRDERS (WF66G)
CONT. FOR LL
LOADING: HL-93.**

SR 5 FILE NO. 7480 SHEET CW1

Bridge Design Engr.	M:\X-Team\MELLEN TO BLAKESLEE JCT\CDSB BR>window files\LAYOUT.WND			REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
Supervisor	Elkey, WE			10	WASH.			
Designed By	Herzstein, Eric	10/11						
Checked By	Kotsonis, A	03/12						
Detailed By	McCarthy, DJ	10/11						
Bridge Projects Engr.	Lewis, RA	06/10						
Prelim. Plan By	Wei, J	03/10						
Architect/Specialist	PDK/BSA/GAW	04/10	DATE	REVISION	BY	APPD		

PARSONS



Washington State Department of Transportation

I-5
MELLEN STREET TO
BLAKESLEE JUNCTION - STAGE 1
SKOOKUMCHUCK RIVER BRIDGE NO. 5/232SCD
LAYOUT

BRIDGE SHEET NO.
CW1
258
OF
472
SHEETS

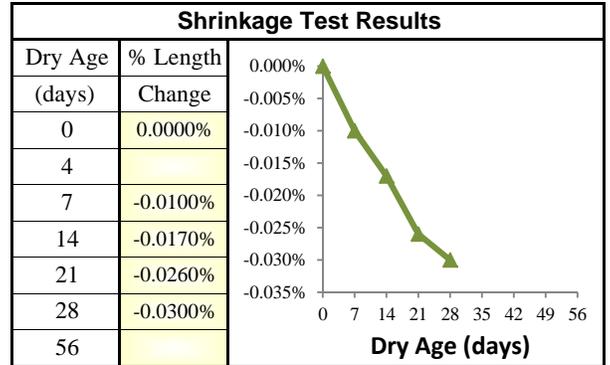
C.S. 2101 ~ PROJ. NO. TA 4572E ~ SOUTHWEST REGION ~ I-5 ~ MELLEN TO BLAKESLEE JCT. ~ SOUTHBOUND CD BRIDGE ~ NEW STRUCTURE



Bridge #	5/232SCD	Bridge Name	Skookumchuck River SBCD	Structure ID	0018272A
Contract #	8272	Region	SW	Project Engineer	Colin Newell
Contractor	Cascade Bridge	Concrete Supplier	Miles Sand & Gravel	Performance Deck Concrete?	YES
Bridge Description	3-Span (80' / 145' / 80'), 5-WF66G Girders (305' bridge length), 2-Lanes (38' wide roadway)				

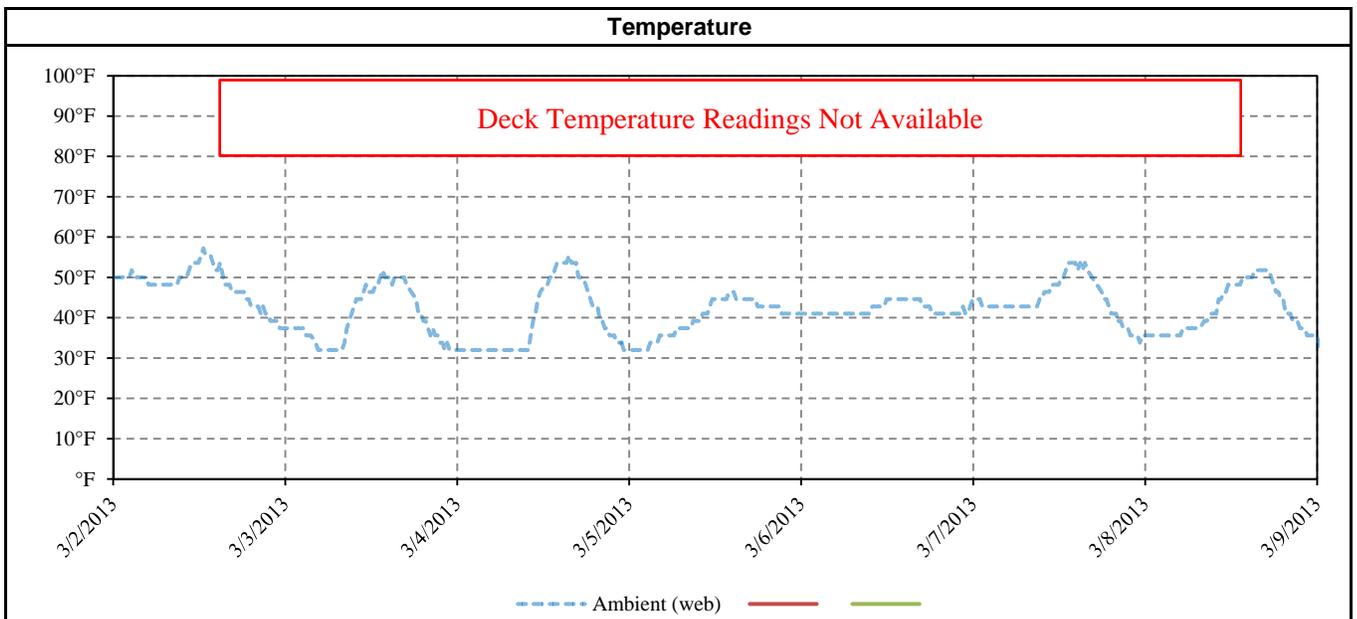
Mix Design (WSDOT Form 350-040)			
Water (max) =		223 lbs/cy	w/c = 0.40 max
Cementitious Materials	Lbs/cy	Source	Type, Class or Grade
cement	464	Lafarge	Type I-II
fly ash	116	Lafarge	Type F
slag			
latex			
microsilica			
Concrete Admixtures	oz/cy	Manufacturer	Product
air entrainment	1-15	BASF	MB-AE-90
water reducer			
HR water reduce	23-40	BASF	Glenium 7500
set retarder			
shrink. reducer	32	BASF	MasterLife SRA

Concrete Test Results		
compressive strength @ 28 days	5,507	psi
modulus of elasticity		psi
permeability @ 56 days	1,350	coulombs
mix design density	145.5	lb/cf



Aggregate					
	Comp. 1	Comp. 2	Comp. 3	Comp. 4	Comp. 5
WSDOT Pit #	B-329	B-329	B-329	B-333	
Grading	No. 4	No. 57	No. 8	Class 2	
% Total	15.4%	33.3%	16.0%	35.3%	
Lbs/cy	480	1040	500	1100	
ASR Mitigation	None Required				

Notes
Same Mix Design as:
* Bridge 5/232NCD
* Bridge 5/234W
Very Similar Mix Design as:
* Bridge 5/229



Contractor Cascade Bridge		Submitted By	Date 1-28-2013
Concrete Supplier Miles Sand & Gravel		Plant Location Rochester	
Contract Number 8272	Contract Name Blakeslee Jct to Mellen St		

This mix is to be used in the following Bid Item No(s): 92.18.01, 93.16.01, 94.17.01

Concrete Class: (check one only)
 3000 4000 4000^a 4000^aP 4000W Concrete Overlay Cement Concrete Pavement^d
 Other Shrinkage Reducer

Remarks: _____

Mix Design No. 0444AFL2 Plant No. 222

Cementitious Materials	Source	Type, Class or Grade	Sp. Gr.	Lbs/cy
Cement	Lafarge	I-II	3.15	464
Fly Ash ^a	Lafarge	F	2.54	116
GGBFS (Slag)				
Latex				
Microsilica				

Concrete Admixtures	Manufacturer	Product	Type	Est. Range (oz/cy)
Air Entrainment	BASF	MB-AE-90		1-15
Water Reducer				
High-Range Water Reducer	BASF	Glenium 7500	F	23-40
Set Retarder				
Other Shrinkage Reducer	BASF	MasterLife SRA		32

Water (Maximum) 233 lbs/cy Is any of the water Recycled or Reclaimed? Yes No

Water Cementitious Ratio (Maximum) 0.40 Mix Design Density 145.5 lbs/cf^d

Design Performance	1	2	3	4	5	Average ^f
28 Day Compressive Strength (cylinders) psi						5,507
14 Day Flexural ^d Strength (beams) psi						

Agency Use Only (Check appropriate Box)

This Mix Design MEETS CONTRACT SPECIFICATIONS and may be used on the bid items noted above

This Mix Design DOES NOT MEET CONTRACT SPECIFICATIONS and is being returned for corrections

Reviewed By: _____ PE Signature

RECEIVED

Aggregate Information

Concrete Aggregates	Component 1	Component 2	Component 3	Component 4	Component 5	Combined Gradation
WSDOT Pit No.	B-329	B-329	B-329	B-333		
WSDOT ASR 14-day Results (%) ^b	<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No				
Grading ^c	4	57	8	Class 2		
Percent of Total Aggregate						100%
Specific Gravity	2.71	2.69	2.68	2.65		
Lbs/cy (ssd)	480	1040	500	1100		

Percent Passing

Size	Component 1	Component 2	Component 3	Component 4	Component 5	Combined
2 inch	100	100	100	100		100
1-1/2 inch	100	100	100	100		100
1 inch	32.6	100	100	100		89.6
3/4 inch	1.6	80.0	100	100		78.2
1/2 inch	0.4	30.1	100	100		61.4
3/8 inch	0.2	7.8	88.6	100		52.1
No. 4	0.1	0.3	22.4	99.4		38.8
No. 8	0.1	0.2	1.4	90.2		32.1
No. 16	0.1	0.1	0.2	70		24.8
No. 30	0.1	0.1	0.2	44.1		15.6
No. 50	0.1	0.1	0.2	20		7.1
No. 100	0.1	0.1	0.2	6		2.2
No. 200	0.1	0.1	0.2	1.7		0.7

Fineness Modulus: 2.70 (Required for Class 2 Sand)

ASR Mitigation Method Proposed^b: _____

Notes:

- a Required for Class 4000D and 4000P mixes.
- b Alkali Silica Reactivity Mitigation is required for sources with expansions over 0.20% - Incidate method for ASR mitigation. For expansion of 0.21% - 0.45%, acceptable mitigation can be the use of low alkali cement or 25% type F fly ash. Any other proposed mitigation method or for pits with greater than 0.45% expansion, proof of mitigating measure, either ASTM C1260 / AASHTO T303 test results must be attached. If ASTM C 1293 testing has been submitted indicating 1-year expansion of 0.04% or less, mitigation is not required.
- c AASHTO No. 467, 57, 67, 7, 8; WSDOT Class 1, Class 2; or combined gradation. See Standard Specification 9-03.1.
- d Required for Cement Concrete Pavements.
- e Attach test results indicating conformance to Standard Specification 9-25.1.
- f Actual Average Strength as determined from testing or estimated from ACI 211.

RECEIVED

JAN 29 2017



Lafarge North America Concrete Lab
5400 W Marginal Way SW
Seattle, WA. 98106

Report To: Miles Sand & Gravel
Attention: Quality Control Personnel

Date: May 25, 2012

Subject: Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration: ASTM C-1202

Tested Materials: Date Sampled: March 2012
Mix Design: WSDOT Valley HPC

Curing: ASTM C-1202 Standard Cure

Results:

<u>Age</u>	<u>Coulombs</u>
56 day	1350
90 day	920

*The ASTM C-1202 procedure was followed.

The test result is only valid if the aggregate(s) sample(s) is(are) representative of the current production and it is to be noted that Lafarge has no knowledge of the representatives of the sample received for testing. Also, material quality can vary with different locations in a quarry. It is recommended that testing be carried out on an annual basis or more frequently if a variation in stone quality is suspected.

Although the Lafarge North America Seattle Concrete Lab. applies state-of-the-art test methods, Lafarge North America, and its affiliates (Lafarge) can not guarantee the results shown above and shall assume no liability whatsoever for any errors in such results and for the consequence of such errors.

Rob Shogren, P.E.
Technical Service Engineer
Lafarge North America

RECEIVED
JAN 29 2012
DEPT. OF TRANSPORTATION CHEHALIS ENGINEERING



Lafarge North America Concrete Lab
5400 W Marginal Way SW
Seattle, WA. 98106

Report To: Miles Sand & Gravel
Attention: Quality Control Personnel

Date: May 25, 2012

Subject: Length Change of Hardened Hydraulic-Cement Concrete Using Procedures of ASTM C-157

Tested Materials: Date Sampled: March, 2012
Source of Aggregates: Miles Sand & Gravel

Mix Design: WSDOT HPC

Results: Slump: 4.5" Specimen Size: 4"x4"x10"
Temp: 64°F Consolidation: Rodding
Initial Cure: Lime water submersion (28 day initial cure)

<u>Age (Days) After Initial Cure</u>	<u>Percent Length Change (Average of 3)</u>
7	0.010
14	0.017
21	0.026
28 (final)	0.030

*The ASTM C-157 procedure was followed.

The test result is only valid if the aggregate(s) sample(s) is(are) representative of the current production and it is to be noted that Lafarge has no knowledge of the representatives of the sample received for testing. Also, material quality can vary with different locations in a quarry. It is recommended that testing be carried out on an annual basis or more frequently if a variation in stone quality is suspected.

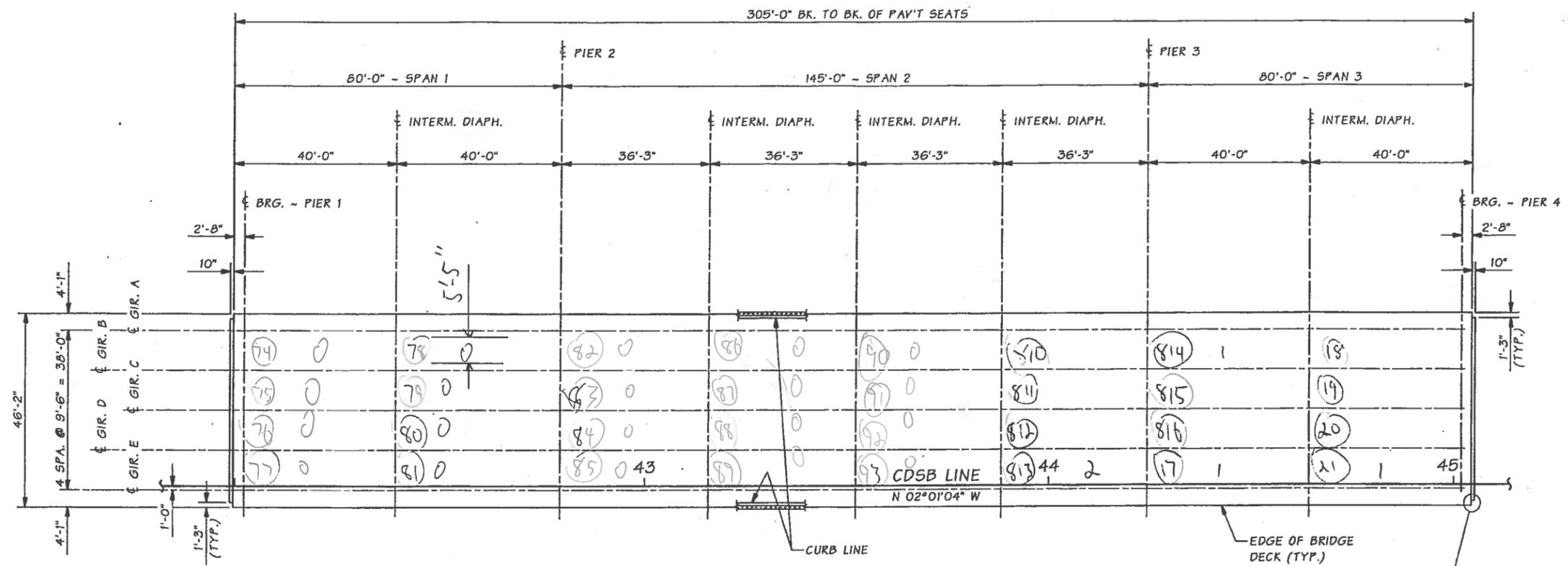
Although the Lafarge North America Seattle Concrete Lab. applies state-of-the-art test methods, Lafarge North America, and its affiliates (Lafarge) can not guarantee the results shown above and shall assume no liability whatsoever for any errors in such results and for the consequence of such errors.

Rob Shogren, P.E.
Technical Service Engineer
Lafarge North America

RECEIVED

JAN 29 2012

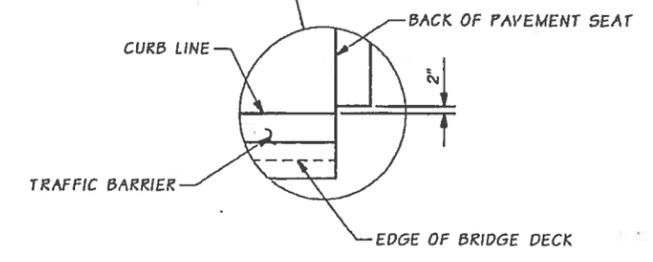
DEPT. OF TRANSPORTATION CHEHALIS ENGINEERING



94 General Elev.

FRAMING PLAN

BEARING OF PIERS ARE NORMAL TO CDSB LINE.



NOTE:
OTHERS CORNERS SIMILAR.

SR 5 FILE NO. 7480 SHEET CW20

Bridge Design Engr.	M:\X-Team\MELLEN TO BLAKESLEE JCT\CDSB BR>window files\FRAMING PLAN.wnd			
Supervisor	Elkey, WE	REGION NO.	STATE	FED. AID PROJ. NO.
Designed By	Herzstein, Eric	10	WASH	
Checked By	Kotsonis, A	JOB NUMBER		
Detailed By	McCarthy, DJ	12X304		
Bridge Projects Engr.		DATE	REVISION	BY
Prep. Plan By				APPD
Architect/Specialist				

PARSONS



I-5
MELLEN STREET TO
BLAKESLEE JUNCTION - STAGE 1
SKOOKUMCHUCK RIVER BRIDGE NO. 5/232SCD
FRAMING PLAN

BRIDGE SHEET NO.	CW20
SHEET OF SHEETS	277 OF 472



Bridge #	5/232SCD	Bridge Name	Skookumchuck River SBCD			Structure ID	0018272A	
Contract #	8272	Region	SW	Project Engineer	Colin Newell	Performance Deck Concrete?	YES	
Contractor	Cascade Bridge		Concrete Supplier	Miles Sand & Gravel		Deck Placement	3/2/2013	
Bridge Description	3-Span (80' / 145' / 80'), 5-WF66G Girders (305' bridge length), 2-Lanes (38' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr} / N_{100} (rounded to the nearest 5%)

Avg. =	1%
Min. =	0%
Max. =	10%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	40.00	9.50	0	20	0%
1	1	B	C	40.00	9.50	0	20	0%
1	1	C	D	40.00	9.50	0	20	0%
1	1	D	E	40.00	9.50	0	20	0%
1	2	A	B	40.00	9.50	0	20	0%
1	2	B	C	40.00	9.50	0	20	0%
1	2	C	D	40.00	9.50	0	20	0%
1	2	D	E	40.00	9.50	0	20	0%
2	1	A	B	36.25	9.50	0	18	0%
2	1	B	C	36.25	9.50	0	18	0%
2	1	C	D	36.25	9.50	0	18	0%
2	1	D	E	36.25	9.50	0	18	0%
2	2	A	B	36.25	9.50	0	18	0%
2	2	B	C	36.25	9.50	0	18	0%
2	2	C	D	36.25	9.50	0	18	0%
2	2	D	E	36.25	9.50	0	18	0%
2	3	A	B	36.25	9.50	0	18	0%
2	3	B	C	36.25	9.50	0	18	0%
2	3	C	D	36.25	9.50	0	18	0%
2	3	D	E	36.25	9.50	0	18	0%
2	4	A	B	36.25	9.50	0	18	0%
2	4	B	C	36.25	9.50	0	18	0%
2	4	C	D	36.25	9.50	0	18	0%
2	4	D	E	36.25	9.50	2	18	10%
3	1	A	B	40.00	9.50	1	20	5%
3	1	B	C	40.00	9.50	0	20	0%
3	1	C	D	40.00	9.50	0	20	0%
3	1	D	E	40.00	9.50	1	20	5%
3	2	A	B	40.00	9.50	0	20	0%
3	2	B	C	40.00	9.50	0	20	0%
3	2	C	D	40.00	9.50	0	20	0%
3	2	D	E	40.00	9.50	1	20	5%



	PIER 1			PIER 2			PIER 3		PIER 4
GIR. A									
GIR. B	0%	0%	0%	0%	0%	0%	0%	5%	0%
GIR. C	0%	0%	0%	0%	0%	0%	0%	0%	0%
GIR. D	0%	0%	0%	0%	0%	0%	0%	0%	0%
GIR. E	0%	0%	0%	0%	0%	10%	5%	5%	

CRACKING INTENSITY ~ BRIDGE 5/232SCD

100% = CRACK EVERY 2 FT.

LESS CRACKING

MORE CRACKING

BRIDGE NUMBER	5/232SCD
BRIDGE NAME	SKOOKUMCHUCK RIVER SBCD
INSPECTION DATE	4/8/2015
DECK CONCRETE	PERFORMANCE BASED

BRIDGE 101/44 (BONE RIVER)

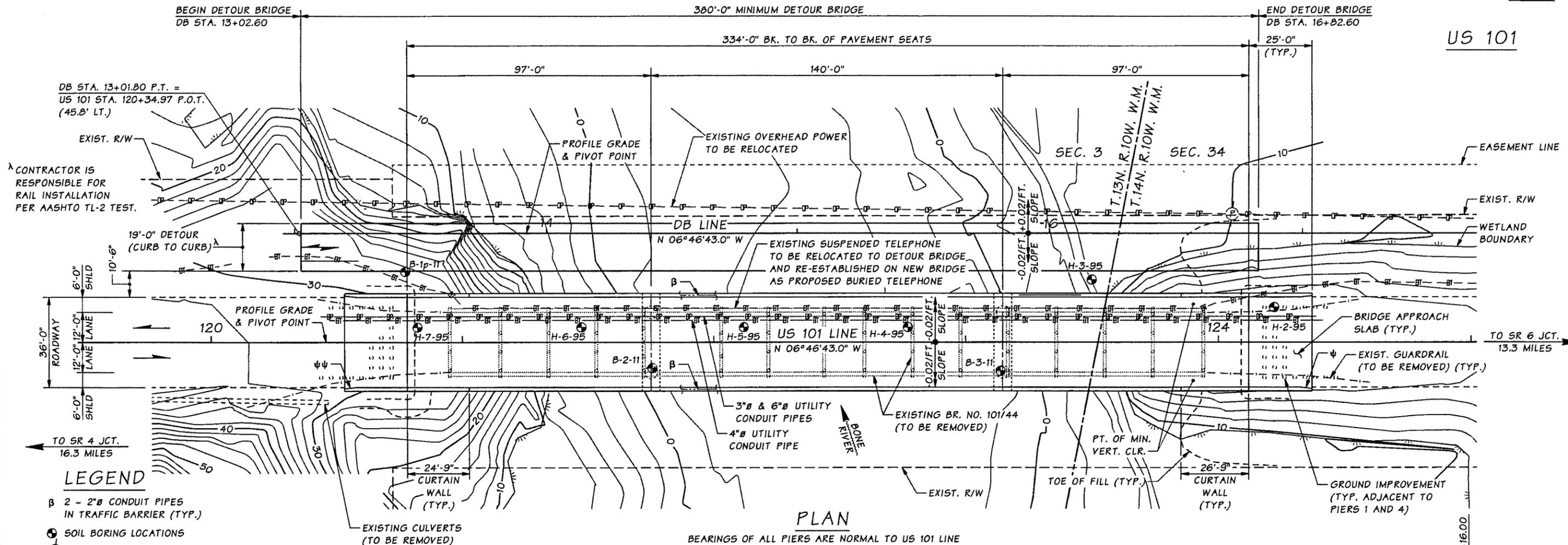
Bridge #	101/44	Bridge Name	Bone River		Structure ID	0018292A	
Contract #	8292	Region	SW	Project Engineer	Lori Figone	Performance Deck Concrete?	YES
Contractor	Cascade Bridge		Concrete Supplier	Bayview Redi Mix, Inc		Deck Placement	4/24/2013
Bridge Description	3-Span (97' / 140' / 97'), 4-WF74G Girders (334" bridge length), 2-Lanes (36' wide roadway)						



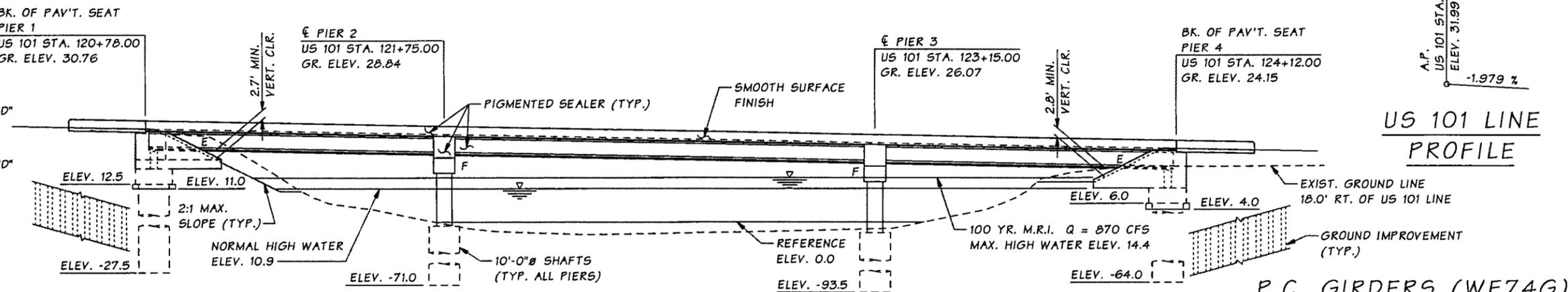
CONTENTS

1. Layout Plan Sheet
2. Mix Design Summary
3. Concrete Mix Design Form
4. Concrete Test Results
5. Field Notes
6. Crack Summary
7. Crack Intensity Diagram

PACIFIC COUNTY



- LEGEND**
- β 2 - 2" Ø CONDUIT PIPES IN TRAFFIC BARRIER (TYP.)
 - ⊕ SOIL BORING LOCATIONS
 - ⊖ EXIST. POWER POLE
 - — — — — EXIST. OVERHEAD POWER
 - — — — — EXIST. UNDERGROUND TELEPHONE CABLE (TO BE RELOCATED AND RE-ESTABLISHED)
 - — — — — PROPOSED BURIED TELEPHONE
 - — — — — PROPOSED BURIED POWER
 - ψ THRIE BEAM GUARDRAIL CONNECTION TYPE "D" (STD. PLAN C-5 & C-25.18-02 WITH TRANSITION TYPE 20) (TYP. 1 LOCATION)
 - ψψ THRIE BEAM GUARDRAIL CONNECTION TYPE "D" (STD. PLAN C-5 & C-25.20-04 WITH TRANSITION TYPE 21) (TYP. 3 LOCATIONS)
 - Ⓟ IDENTIFIES SECTION, VIEW OR DETAIL
 - Ⓟ TAKEN OR SHOWN ON BRIDGE SHEET 15
 - Ⓟ TAKEN OR SHOWN ON THE SAME SHEET



DATUM
N.A.V.D. OF 1988

P.C. GIRDERS (WF74G)
CONT. FOR LL
LOADING: HL-93

SR 101 FILE NO. 7021 SHEET BR.1

Bridge Design Engr.	khalleghi, B	06/10	M:\Z-team\US 101 Bone Rv. Bridge\window files\Layout.WND
Supervisor	Zeldenrust, RP		
Designed By	PRG / HZ	05/11	
Checked By	HZ / PRG	12/11	
Detailed By	Foote, H	05/11	
Bridge Projects Engr.	Lewis, RA	06/10	
Prelim. Plan By	Bauer, M	06/10	
Architect/Specialist	GAW, PDK, BSA	06/10	DATE REVISION BY APP'D

BRIDGE AND STRUCTURES OFFICE

Washington State Department of Transportation

3/13/12

US 101 BONE RIVER BRIDGE REPLACE BRIDGE		BRIDGE SHEET NO. BR1
BR. NO. 101/44		
LAYOUT		SHEET OF 94 SHEETS

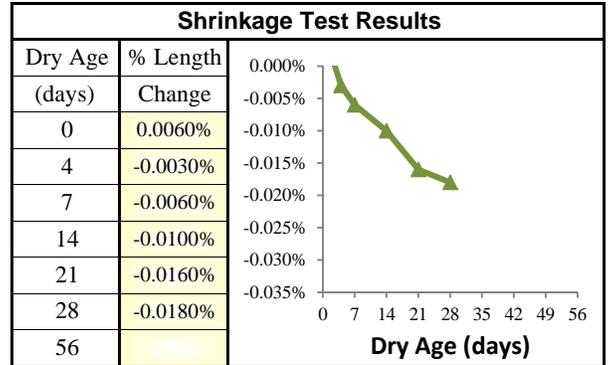
C.S. 2501 ~ PROJ. NO. XL3345 ~ SOUTHWEST REGION ~ US 101 ~ MP 45.09 TO MP 45.27 ~ BONE RIVER BRIDGE NO. 101/44 REPLACEMENT (NEW STRUCTURE)



Bridge #	101/44	Bridge Name	Bone River			Structure ID	0018292A
Contract #	8292	Region	SW	Project Engineer	Lori Figone	Performance Deck Concrete?	YES
Contractor	Cascade Bridge		Concrete Supplier	Bayview Redi Mix, Inc		Deck Placement	4/24/2013
Bridge Description	3-Span (97' / 140' / 97'), 4-WF74G Girders (334" bridge length), 2-Lanes (36' wide roadway)						

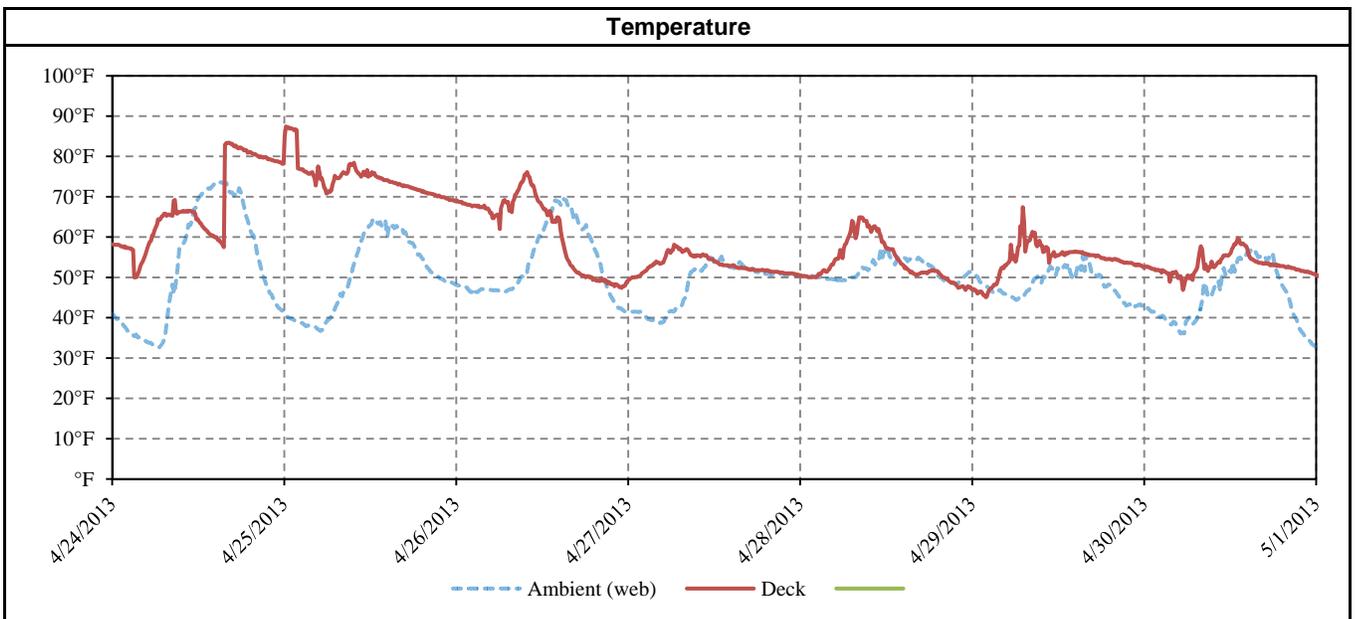
Mix Design (WSDOT Form 350-040)			
Water (max) =		230 lbs/cy	w/c = 0.38 max
Cementitious Materials	Lbs/cy	Source	Type, Class or Grade
cement	460	Ashgrove	Type I-II
fly ash	150	Lafarge	Type F
slag			
latex			
microsilica			
Concrete Admixtures	oz/cy	Manufacturer	Product
air entrainment	1-15	BASF	Micro Air
water reducer			
HR water reduce	20-30	BASF	Glenium 7500
set retarder			
shrink. reducer	120-140	BASF	Masterlife

Concrete Test Results		
compressive strength @ 28 days	5,691	psi
modulus of elasticity	4,012,122	psi
permeability @ 56 days	1,677	coulombs
mix design density	150.1	lb/cf



Aggregate					
	Comp. 1	Comp. 2	Comp. 3	Comp. 4	Comp. 5
WSDOT Pit #	PS-X-130	PS-X-130	PS-X-130		
Grading	#67	#4	Class II		
% Total	42.0%	20.0%	38.0%		
Lbs/cy	1350	650	1213		
ASR Mitigation	None Required				

Notes
Same Mix Design as:
* Bridge 6/8
* Bridge 101/31
* Bridge 105/4
* Bridge 105/3
if swell of concrete specimen is included, total change in length at 28 days drying is 240 microstrain (0.0060% + 0.0180%)



Concrete Mix Design

Contractor Cascade Bridge		Submitted By Bayview Redi-Mix, Inc.		Date 3-12-2013
Concrete Supplier Bayview Redi-Mix, Inc			Plant Location Aberdeen 011, Raymond 041	
Contract Number		Contract Name SR 101 Bone River		

This mix is to be used in the following Bid Item No(s): 40.13

Concrete Class: (check one only)

3000
 4000
 4000^a
 4000^aP
 4000W
 Concrete Overlay
 Cement Concrete Pavement^d
 Other Shrinkage

Remarks: _____

Mix Design No. WSDT4DS130 Plant No. 011, 041

Cementitious Materials	Source	Type, Class or Grade	Sp. Gr.	Lbs/cy
Cement	Ashgrove, Seattle, WA	Type I-II 6-02.3(2)	3.15	460
Fly Ash ^a	Lafarge, Centralia, WA	Type F	2.58	150
GGBFS (Slag)				
Latex				
Microsilica				

Concrete Admixtures	Manufacturer	Product	Type	Est. Range (oz/cy)
Air Entrainment	BASF, Cleveland, OH	Micro-Air		1.15
Water Reducer				
High-Range Water Reducer	BASF, Cleveland, OH	Glenium 7500	F	20-30
Set Retarder				
Other Shrinkage	BASF, Cleveland, OH	Masterlife		120-140

HIGH
30.5-52
← NORMAL
12.2-91.5
64-192
CP

Water (Maximum) 230 lbs/cy Is any of the water Recycled or Reclaimed? Yes^e No

Water Cementitious Ratio (Maximum) 0.38 Mix Design Density 150.1 lbs/cf^d

Design Performance	1	2	3	4	5	Average ^f
28 Day Compressive Strength (cylinders) psi	5,775	5,766	5,623	5,561	5,730	5,691
14 Day Flexural ^d Strength (beams) psi						

Agency Use Only (Check appropriate Box)

This Mix Design **MEETS CONTRACT SPECIFICATIONS** and may be used on the bid items noted above
 This Mix Design **DOES NOT MEET CONTRACT SPECIFICATIONS** and is being returned for corrections

Reviewed By: *Ami Tjorne* 4/16/13
PE Signature Date

Aggregate Information

Concrete Aggregates	Component 1	Component 2	Component 3	Component 4	Component 5	Combined Gradation
WSDOT Pit No.	PS-X-130	PS-X-130	PS-X-130			
WSDOT ASR 14-day Results (%) ^b	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No	
Grading ^c	AASHTO #4	AASHTO #67	Class II			
Percent of Total Aggregate	20	42	38			100%
Specific Gravity	2.825	2.825	2.747			
Lbs/cy (ssd)	650	1350	1213			

Percent Passing

2 inch	100					100
1-1/2 inch	100	100				100
1 inch	52	100				90
3/4 inch	1	93				77
1/2 inch	1	58				63
3/8 inch	1	30	100			51
No. 4	0	7	99			41
No. 8	0	0	78			30
No. 16	0	0	58			22
No. 30	0	0	35			13
No. 50	0	0	14			5
No. 100	0	0	3			1
No. 200	0.1	0.1	1			0.5

Fineness Modulus: 3.14 (Required for Class 2 Sand)

ASR Mitigation Method Proposed^b: Not Required for this Source

Notes:

- ^a Required for Class 4000D and 4000P mixes.
- ^b Alkali Silica Reactivity Mitigation is required for sources with expansions over 0.20% - Incidate method for ASR mitigation. For expansion of 0.21% - 0.45%, acceptable mitigation can be the use of low alkali cement or 25% type F fly ash. Any other proposed mitigation method or for pits with greater than 0.45% expansion, proof of mitigating measure, either ASTM C1260 / AASHTO T303 test results must be attached. If ASTM C 1293 testing has been submitted indicating 1-year expansion of 0.04% or less, mitigation is not required.
- ^c AASHTO No. 467, 57, 67, 7, 8; WSDOT Class 1, Class 2; or combined gradation. See Standard Specification 9-03.1.
- ^d Required for Cement Concrete Pavements.
- ^e Attach test results indicating conformance to Standard Specification 9-25.1.
- ^f Actual Average Strength as determined from testing or estimated from ACI 211.

TEST RESULTS

ASTM C 192 - Standard Practice for Making and Curing Concrete Test Specimens in the Laboratory

Concrete Mixture Proportions

4,000 PSI Mix

Trial Mix Results Calculated to 1yd³

D-101112-01

<u>S-Number</u>	<u>Description</u>	<u>SpG</u>	<u>Mass, lbs</u>	<u>Vol. Cuft</u>
S-121541	AG Seattle Type I/II	3.15	462	2.35
S-120817	Lafarge Centralia Class F	2.58	151	0.94
S-122202	Pit X-130 Fine Agg.	2.75	1,217	7.09
S-122204	Pit X-130 1.5 to 3/4 Agg.	2.83	652	3.69
S-122203	Pit X-130 3/4 to No. 4 Agg.	2.83	1,357	7.68
---	Overland Park Municipal	1.00	233	3.73
-	Air	-	<u>5.6%</u>	<u>1.51</u>
Totals:			4,072	27.00

Admixtures

<u>S-Number</u>	<u>Description</u>	<u>Dosage, oz/cwt</u>
S-122303	BASF Micro-Air	1.0
S-122302	BASF Glenium 7500	4.0
S-122225	BASF Master Life SRA 20	21.0

Plastic Properties

D-101112-01

Slump, in:	6.75
Unit Weight, lbs/cuft:	150.8
Air Content (Calculated), %:	5.6
w/cm ratio:	0.38
Concrete Temperature, F:	74°

Specs 3.93 / mcs 28-29

AASHTO T 277 - Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration
Accelerated Cure

<u>Sample No.</u>	<u>Diameter, in.</u>	<u>Charge Passed, C</u>	<u>Corrected Charge, C</u>	<u>Qualitative Equivalent</u>	<u>Age, days</u>
D-101112-01	4.00	739	650	Very Low	28

AASHTO T 277 - Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration
Standard Cure

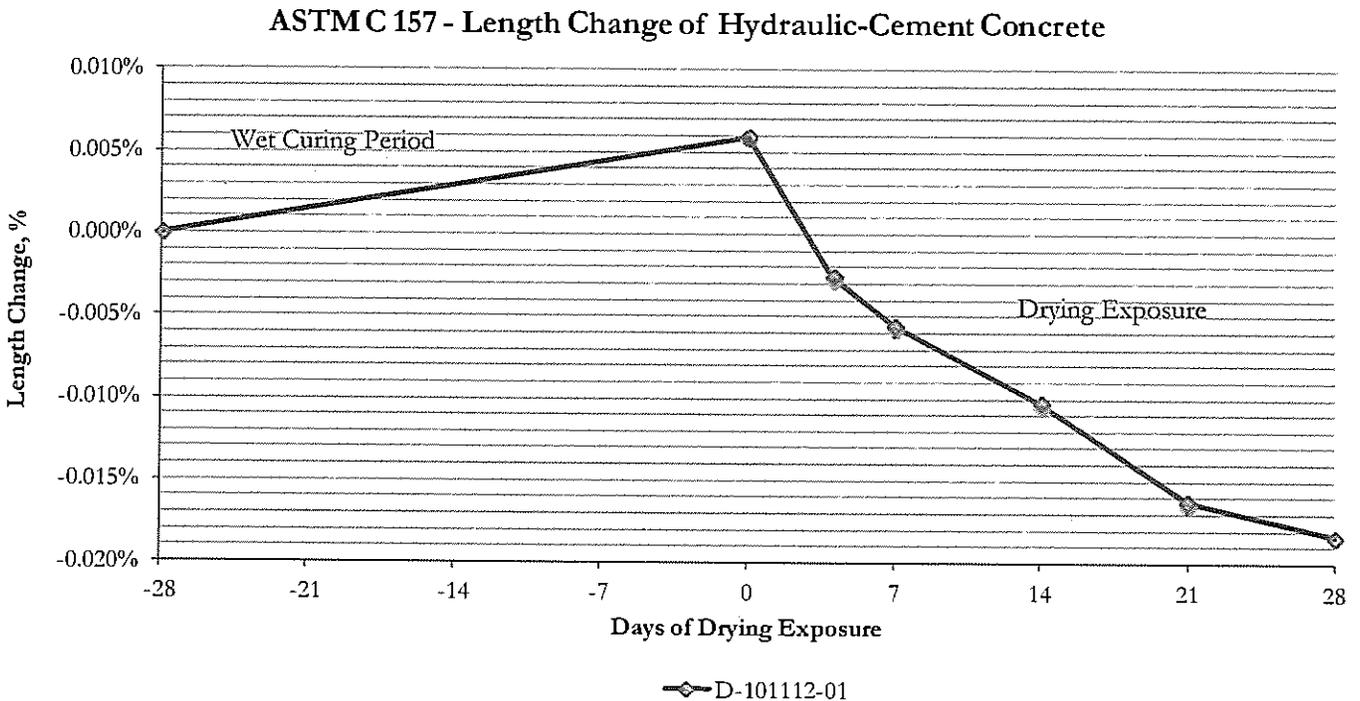
<u>Sample No.</u>	<u>Diameter, in.</u>	<u>Charge Passed, C</u>	<u>Corrected Charge, C</u>	<u>Qualitative Equivalent</u>	<u>Age, days</u>
D-101112-01	4.00	1,902	1,672	Low	28
	4.00	1,750	1,538	Low	56
	4.00	1,908	1,677	Low	56

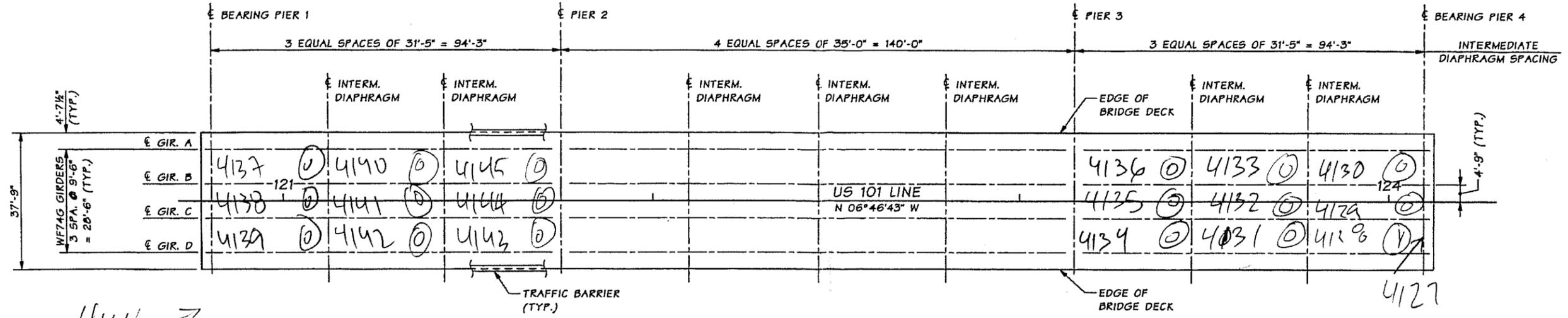
Specs 3.93 / mcs 28-29

ASTM C 157 Standard Test Method for Length Change of Hardened Hydraulic-Cement Mortar and Concrete

Material:	Concrete
Number of Specimens per Mixture:	4
Size of Specimens, in:	Length: 10.0
	Width: 4.0
	Height: 4.0
Method of Consolidation:	4
Period of Moist Curing:	28-days
Drying Exposure Conditions:	23°C, 50% RH

Length Change	<u>Reading</u>	<u>D-101112-01</u>
	Initial	0.000%
	0-days dry	0.006%
	4-days dry	-0.003%
	7-days dry	-0.006%
	14-days dry	-0.010%
	21-days dry	-0.016%
	28-days dry	-0.018%

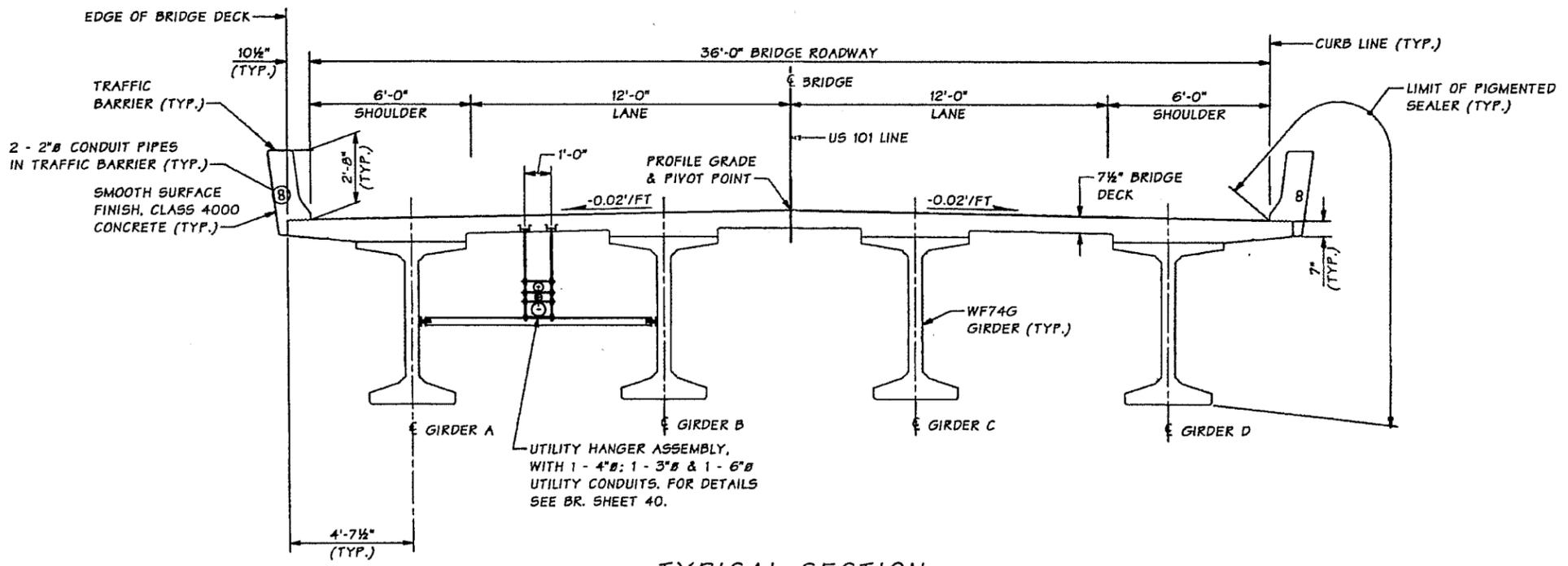




FRAMING PLAN

BEARINGS OF ALL PIERS ARE NORMAL TO US 101 LINE

4146 →
4147
4148



TYPICAL SECTION

SHOWN NEAR MID-SPAN

SR 101 FILE NO. 7021 SHEET BR31

Bridge Design Engr.	khaleghi, B	M:\Z-Team\US 101 Bone Rv. Bridge\window files\Framing Plan.WND	
Supervisor	Zeidenrust, RP	REGION NO.	STATE
Designed By	Zhang, H 05/11	30	WASH.
Checked By	Gallagher, P 09/11	JOB NUMBER 12X500	
Detailed By	Foote, N 05/11		
Bridge Projects Engr.			
Prefin. Plan By			
Architect/Specialist		DATE	REVISION
		BY	APP'D

BRIDGE AND STRUCTURES OFFICE
3/13/2012

Washington State Department of Transportation

US 101 BONE RIVER BRIDGE REPLACE BRIDGE BR. NO. 101/44		BRIDGE SHEET NO. BR31
FRAMING PLAN		SHEET 72 OF 94 SHEETS



Bridge #	101/44	Bridge Name	Bone River			Structure ID	0018292A	
Contract #	8292	Region	SW	Project Engineer	Lori Figone	Performance Deck Concrete?	YES	
Contractor	Cascade Bridge		Concrete Supplier	Bayview Redi Mix, Inc		Deck Placement	4/24/2013	
Bridge Description	3-Span (97' / 140' / 97'), 4-WF74G Girders (334" bridge length), 2-Lanes (36' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	0%
Min. =	0%
Max. =	5%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	31.42	9.50	0	16	0%
1	1	B	C	31.42	9.50	0	16	0%
1	1	C	D	31.42	9.50	0	16	0%
1	2	A	B	31.42	9.50	0	16	0%
1	2	B	C	31.42	9.50	0	16	0%
1	2	C	D	31.42	9.50	0	16	0%
1	3	A	B	31.42	9.50	0	16	0%
1	3	B	C	31.42	9.50	0	16	0%
1	3	C	D	31.42	9.50	0	16	0%
2	1	A	B	35.00	9.50	#N/A	18	#N/A
2	1	B	C	35.00	9.50	#N/A	18	#N/A
2	1	C	D	35.00	9.50	#N/A	18	#N/A
2	2	A	B	35.00	9.50	#N/A	18	#N/A
2	2	B	C	35.00	9.50	#N/A	18	#N/A
2	2	C	D	35.00	9.50	#N/A	18	#N/A
2	3	A	B	35.00	9.50	#N/A	18	#N/A
2	3	B	C	35.00	9.50	#N/A	18	#N/A
2	3	C	D	35.00	9.50	#N/A	18	#N/A
2	4	A	B	35.00	9.50	#N/A	18	#N/A
2	4	B	C	35.00	9.50	#N/A	18	#N/A
2	4	C	D	35.00	9.50	#N/A	18	#N/A
3	1	A	B	31.42	9.50	0	16	0%
3	1	B	C	31.42	9.50	0	16	0%
3	1	C	D	31.42	9.50	0	16	0%
3	2	A	B	31.42	9.50	0	16	0%
3	2	B	C	31.42	9.50	0	16	0%
3	2	C	D	31.42	9.50	0	16	0%
3	3	A	B	31.42	9.50	0	16	0%
3	3	B	C	31.42	9.50	0	16	0%
3	3	C	D	31.42	9.50	1	16	5%



	PIER 1			PIER 2				PIER 3			PIER 4
GIR. A											
GIR. B	0%	0%	0%	XXX	XXX	XXX	XXX	0%	0%	0%	
GIR. C	0%	0%	0%	XXX	XXX	XXX	XXX	0%	0%	0%	
GIR. D	0%	0%	0%	XXX	XXX	XXX	XXX	0%	0%	5%	

CRACKING INTENSITY ~ BRIDGE 101/44

100% = CRACK EVERY 2 FT.

X X X = CRACKS NOT COUNTED DUE TO LIMITED ACCESS

LESS CRACKING

MORE CRACKING

BRIDGE NUMBER	101/44
BRIDGE NAME	BONE RIVER
INSPECTION DATE	5/7/2015
DECK CONCRETE	PERFORMANCE BASED

APPENDIX D

MULTI-SPAN STEEL PLATE GIRDER BRIDGES

BRIDGE 5/434SCD (SBCD OVER SR 16)

BRIDGE 529/25 (EBEY SLOUGH)

BRIDGE 2/651W-S (W-S RAMP OVER US 2 / US 395)

BRIDGE 9/134 (PILCHUCK CREEK)

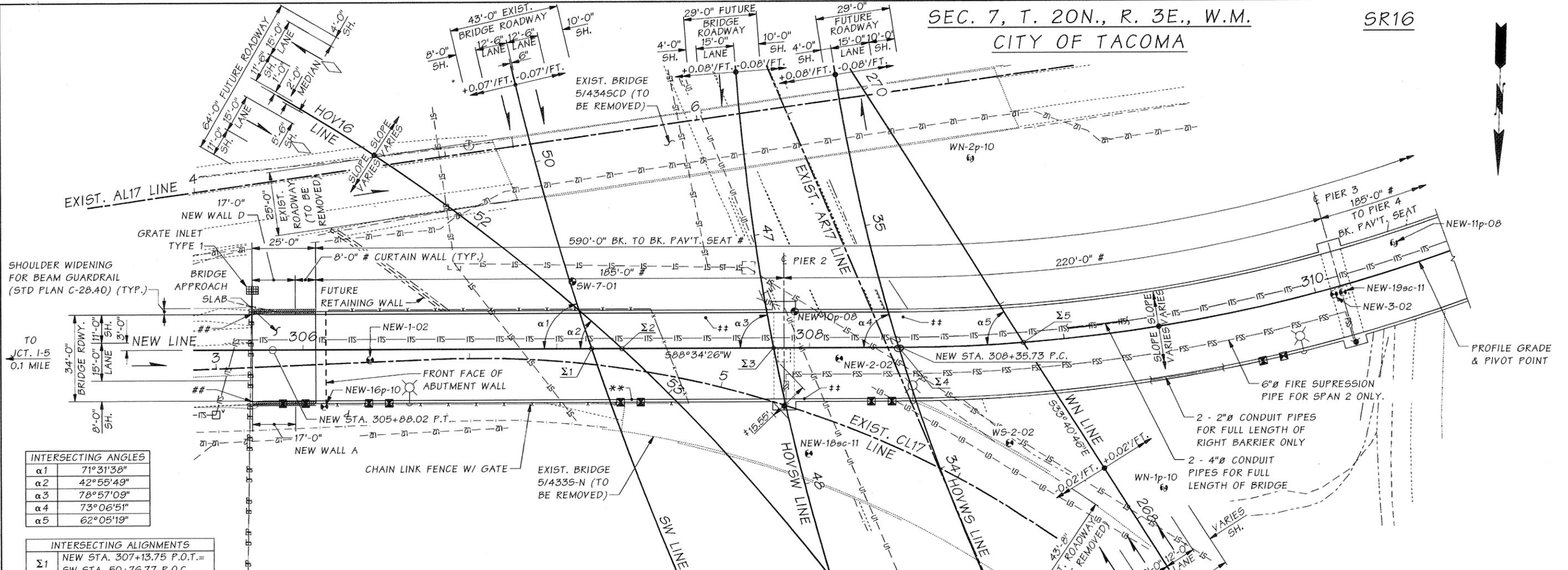
BRIDGE 5/434SCD (SBCD OVER SR 16)

Bridge #	5/434SCD	Bridge Name	SBCD Over SR 16 HOV & Ramps		Structure ID	0018189B	
Contract #	8189	Region	OR	Project Engineer	Neal Uhlmeyer	Performance Deck Concrete?	Yes
Contractor	Mowat Construction		Concrete Supplier	Holroyd Co.		Deck Placement	2/11/13, 2/19/13 & 2/26/13
Bridge Description	3-Span (185' / 220' / 185'), 3-Steel Plate Girders (590' bridge length), 1-Lane (34' wide roadway)						



CONTENTS

1. Layout Plan Sheet
2. Mix Design Summary
3. Concrete Mix Design Form
4. Concrete Test Results
5. Field Notes
6. Crack Summary
7. Crack Intensity Diagram

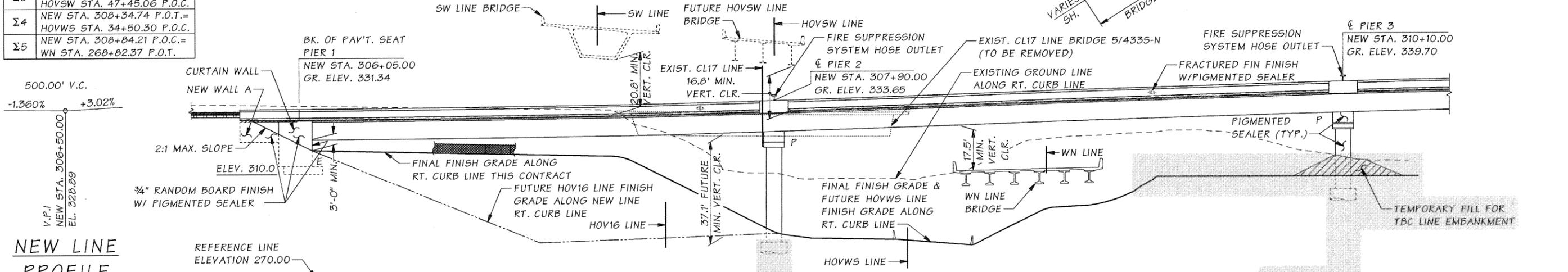


INTERSECTING ANGLES

α1	71°31'38"
α2	42°55'49"
α3	78°57'09"
α4	73°06'51"
α5	62°05'19"

INTERSECTING ALIGNMENTS

Σ1	NEW STA. 307+13.75 P.O.T.= SW STA. 50+76.77 P.O.C.
Σ2	NEW STA. 307+25.66 P.O.T.= HOV16 STA. 52+74.53 P.O.C.
Σ3	NEW STA. 307+85.89 P.O.T.= HOVSW STA. 47+45.06 P.O.C.
Σ4	NEW STA. 308+34.74 P.O.T.= HOVWS STA. 34+50.30 P.O.C.
Σ5	NEW STA. 308+84.21 P.O.C.= WN STA. 268+82.37 P.O.T.



DEVELOPED ELEVATION
GRADE ELEVATIONS SHOWN ARE FINISH GRADES AT TOP OF BRIDGE DECK ON NEW LINE AND ARE EQUAL TO PROFILE GRADE. SEE STD. PLAN A-50.20 FOR EMBANKMENT DETAILS AT BRIDGE ENDS.

COMPOSITE STEEL PLATE GIRDER
LOADING: HL-93

Bridge Design Engr.	Khaileghi, B	M:\Z-Team\SR16 EB NV\NEW Line>window files\Layout 1.Add1.WND
Supervisor	Zeldenrust, RP	
Designed By	Rosa, M	02/10
Checked By	Sweett, GD	04/11
Detailed By	Foote, N	03/10
Bridge Projects Engr.	Lewis, RA	7/14/11
Prelim. Plan By	CH2MHILL	
Architect/Specialist	PKD / NSB	

BRIDGE AND STRUCTURES OFFICE

7/7/11

Washington State Department of Transportation

I-5 / SR 16 EB NALLEY VALLEY - HOV		BRIDGE SHEET NO.
NEW LINE BRIDGE		BA2
LAYOUT 1		SHEET
		713
		OF
		1341
		SHEETS

SR 16 FILE NO. 2587 SHEET BA2

PROJ. NO. XL3477 ~ OLYMPIC REGION ~ I-5 & SR16 INTERCHANGE ~ EASTBOUND NALLEY VALLEY ~ NEW LINE BRIDGE

Concrete Mix Design

Contractor Mowat Construction Co		Submitted By Greg Smith	Date 12/15/2011
Concrete Supplier Holroyd Co., Inc.		Plant Location 3131 29th Ave Sw Tumwater, WA	
Contract Number 8189	Contract Name Nalley Valley Eastbound		

This mix is to be used in the following Bid Item No(s): 121, 122, 123, 124, 125, 126, 127

Concrete Class: (*check one only*)

- 3000
 4000
 4000^a
 4000P^a
 4000W
 Concrete Overlay
 Cement Concrete Pavement^d
 Other Shrinkage Reducer

Remarks: _____

Mix Design No. 6091FASD Plant No. Tacoma (3-4)

Cementitious Materials	Source	Type, Class or Grade	Sp. Gr.	Lbs/cy
Cement	Lehigh Cement Co	Type I-II	3.15	480
Fly Ash ^a	Lafarge	Type F	2.61	85
GGBFS (Slag)				
Latex				
Microsilica				

Concrete Admixtures	Manufacturer	Product	Type	Est. Range (oz/cy)
Air Entrainment	BASF Admixtures, Inc.	MB AE™ 90		1-6
Water Reducer				
High-Range Water Reducer	BASF Admixtures, Inc.	Glenium® 3030 NS	Type F	25-45
Set Retarder				
Other Shrinkage Reducer	BASF Admixtures, Inc.	MasterLIFE® SRA 20	Type S	30-45

Water (Maximum) 217 lbs/cy Is any of the water Recycled or Reclaimed? Yes^e No

Water Cementitious Ratio (Maximum) 0.38 Mix Design Density 146.8 lbs/cf^d

Design Performance	1	2	3	4	5	Average ^f
28 Day Compressive Strength (cylinders) psi	6,370	6,460	6,380	6,410	6,670	6,458
14 Day Flexural ^d Strength (beams) psi						

Agency Use Only (Check appropriate Box)

This Mix Design **MEETS CONTRACT SPECIFICATIONS** and may be used on the bid items noted above
 This Mix Design **DOES NOT MEET CONTRACT SPECIFICATIONS** and is being returned for corrections

Reviewed By: *[Signature]* 11 Apr 2013
 PE Signature Date

Aggregate Information

Concrete Aggregates	Component 1	Component 2	Component 3	Component 4	Component 5	Combined Gradation
WSDOT Pit No.	J-9	J-9	J-9			
WSDOT ASR 14-day Results (%) ^b	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No	
Grading ^c	Class 1	#67	#4			
Percent of Total Aggregate	39.6	45.1	15.3			100%
Specific Gravity	2.63	2.69	2.69			
Lbs/cy (ssd)	1265	1440	490			3195

Percent Passing

2 inch			100.0			100
1-1/2 inch			100.0			100
1 inch		100.0	52.0			93.4
3/4 inch		99.0	12.0			87.3
1/2 inch						66.9
3/8 inch	100.0	36.0	0			50.3
No. 4	97.0	3.0				39.4
No. 8	81.0	1.0				31.9
No. 16	62.0					23.2
No. 30	36.0					13.9
No. 50	13.0					5.2
No. 100	5.0					1.9
No. 200	2.5					1.0

Fineness Modulus: _____ (Required for Class 2 Sand)

ASR Mitigation Method Proposed^b: Pit No. J-9 has ASR of 0.43 and is mitigated by the use of low alkali cement.

Notes:

- a Required for Class 4000D and 4000P mixes.
- b Alkali Silica Reactivity Mitigation is required for sources with expansions over 0.20% - Incidate method for ASR mitigation. For expansion of 0.21% - 0.45%, acceptable mitigation can be the use of low alkali cement or 25% type F fly ash. Any other proposed mitigation method or for pits with greater than 0.45% expansion, proof of mitigating measure, either ASTM C1260 / AASHTO T303 test results must be attached. If ASTM C 1293 testing has been submitted indicating 1-year expansion of 0.04% or less, mitigation is not required.
- c AASHTO No. 467, 57, 67, 7, 8; WSDOT Class 1, Class 2; or combined gradation. See Standard Specification 9-03.1.
- d Required for Cement Concrete Pavements.
- e Attach test results indicating conformance to Standard Specification 9-25.1.
- f Actual Average Strength as determined from testing or estimated from ACI 211.



Lafarge North America Concrete Lab
5400 W Marginal Way SW
Seattle, WA. 98106

Report To: Holroyd
Attention: Quality Control Personnel

Date: September 30, 2011

Subject: Electrical Indication of Concrete's Ability to Resist Chloride Ion Penetration: ASTM C-1202

Tested Materials: Date Sampled: **August 2, 2011**
Mix Design: **Nalley Valley HPC**

Curing: ASTM C-1202 Standard Cure

Results:

Age
56 day

Coulombs
1463

*The ASTM C-1202 procedure was followed.

The test result is only valid if the aggregate(s) sample(s) is(are) representative of the current production and it is to be noted that Lafarge has no knowledge of the representatives of the sample received for testing. Also, material quality can vary with different locations in a quarry. It is recommended that testing be carried out on an annual basis or more frequently if a variation in stone quality is suspected.

Although the Lafarge North America Seattle Concrete Lab. applies state-of-the-art test methods, Lafarge North America. and its affiliates (Lafarge) can not guarantee the results shown above and shall assume no liability whatsoever for any errors in such results and for the consequence of such errors.

A handwritten signature in black ink that reads 'Robt S. Shogren'.

Rob Shogren, P.E.
Technical Service Engineer
Lafarge North America



Lafarge North America Concrete Lab
5400 W Marginal Way SW
Seattle, WA. 98106

Report To: Holroyd
Attention: Quality Control Personnel

Date: September 30, 2011

Subject: Length Change of Hardened Hydraulic-Cement Concrete Using Procedures of ASTM C-157

Tested Materials: Date Sampled: **August 2, 2011**
Source of Aggregates: Holroyd

Mix Design: WSDOT HPC

Results: Slump: 4.5"
Temp: 64^F Specimen Size: 4"x4"x10"
Consolidation: Rodding
Initial Cure: Lime water submersion (28 day initial cure)

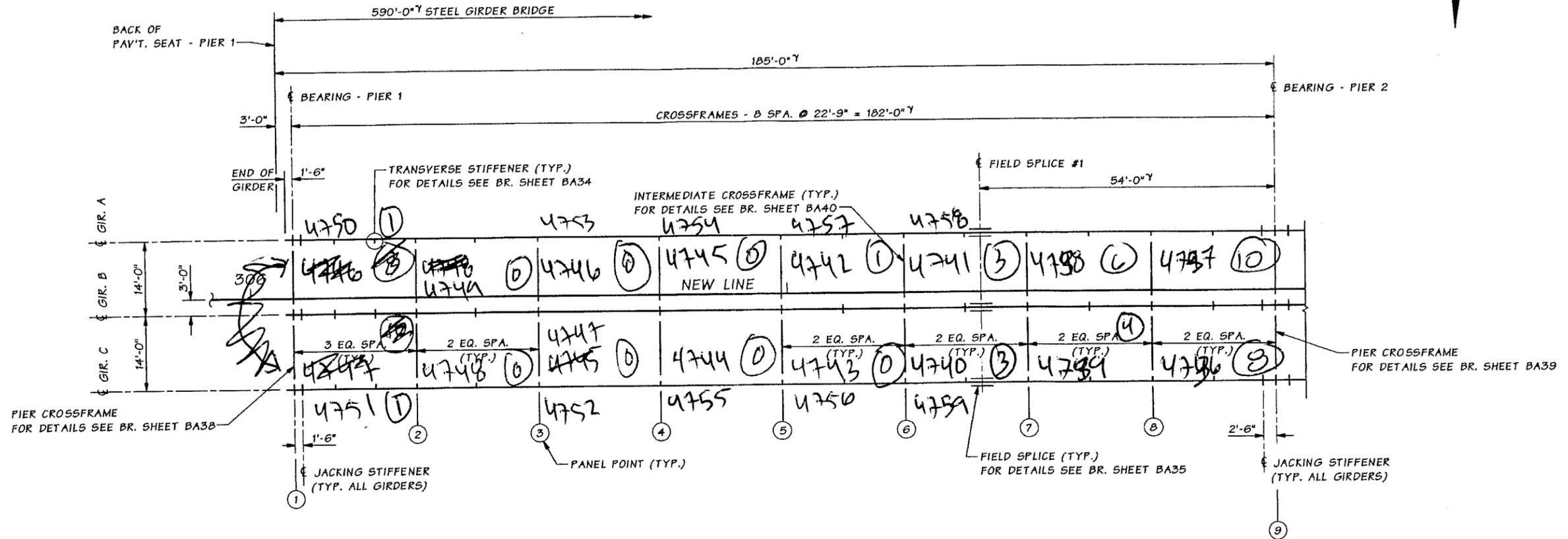
<u>Age (Days) After Initial Cure</u>	<u>Percent Length Change (Average of 3)</u>
7	0.010
14	0.018
21	0.026
28 (final)	0.028

*The ASTM C-157 procedure was followed.

The test result is only valid if the aggregate(s) sample(s) is(are) representative of the current production and it is to be noted that Lafarge has no knowledge of the representatives of the sample received for testing. Also, material quality can vary with different locations in a quarry. It is recommended that testing be carried out on an annual basis or more frequently if a variation in stone quality is suspected.

Although the Lafarge North America Seattle Concrete Lab. applies state-of-the-art test methods, Lafarge North America. and its affiliates (Lafarge) can not guarantee the results shown above and shall assume no liability whatsoever for any errors in such results and for the consequence of such errors.

Rob Shogren, P.E.
Technical Service Engineer
Lafarge North America



FRAMING PLAN - SPAN 1

ALL CROSSFRAMES ARE NORMAL TO NEW LINE
 Y MEASURED ALONG NEW LINE

SR 16 FILE NO. 2587 SHEET BA28

Bridge Design Engr.	Khaleghi, B	M:\Z-Team\SR16 EB NV\New Line>window files\Framing Plan I.WND		REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
Supervisor	Zeldenrust, RP			10	WASH.			
Designed By	ROSA, M	02/10		JOB NUMBER				
Checked By	Swett, GD	04/11		09C519				
Detailed By	Footo, N	08/10						
Bridge Projects Engr.								
Prelim. Plan By								
Architect/Specialist		DATE	REVISION	BY	APPD			



BRIDGE AND STRUCTURES OFFICE



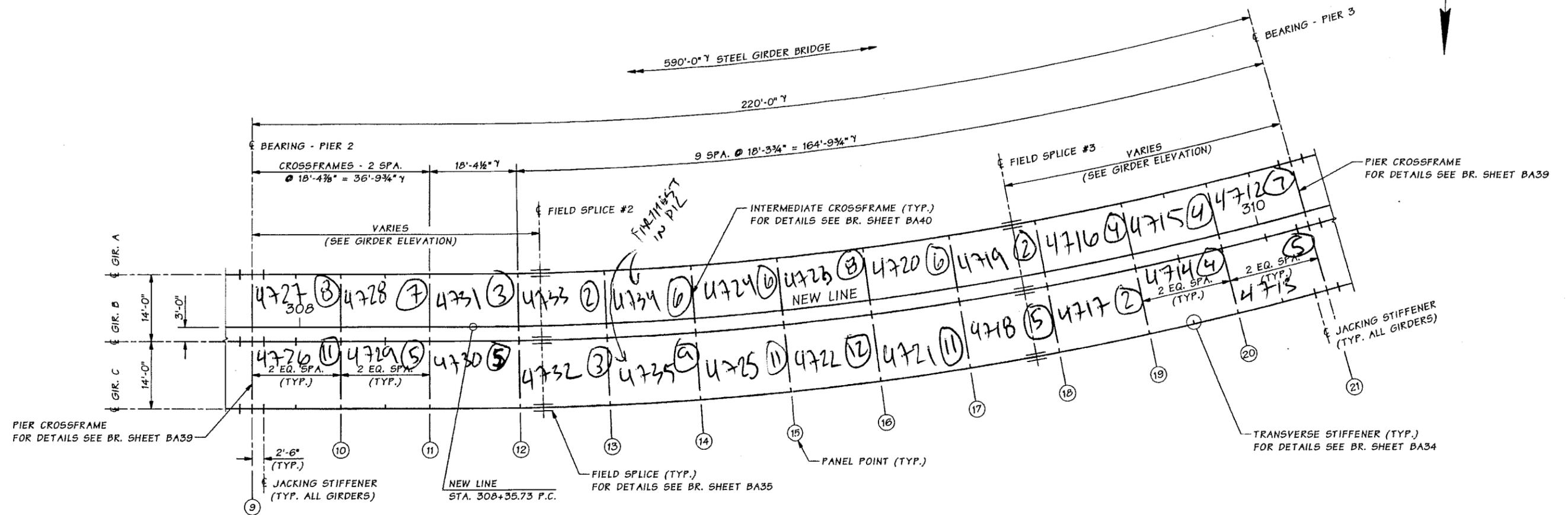
Washington State Department of Transportation

I-5 / SR 16
 EB NALLEY VALLEY - HOV
 NEW LINE BRIDGE
 FRAMING PLAN
 SHEET 1 OF 3

BRIDGE SHEET NO.
 BA28
 SHEET
 739
 OF
 1341
 SHEETS

5/434 SCD

GIRDER	RADIUS
A	628'-9 1/8"
B	642'-9 1/8"
C	656'-9 1/8"

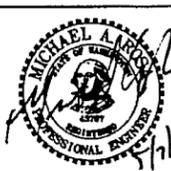


FRAMING PLAN - SPAN 2

ALL CROSSFRAMES ARE NORMAL OR RADIAL TO NEW LINE
 'Y' MEASURED ALONG NEW LINE

SHEET BA29

ENGR.	DATE	REVISION	BY	APPD.	REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
Engr. Khaleghi, B					10	WASH.			
Zeldenrust, RP									
Rosa, M	02/10								
Swett, GO	04/11								
Boote, N	08/10								



BRIDGE AND STRUCTURES OFFICE

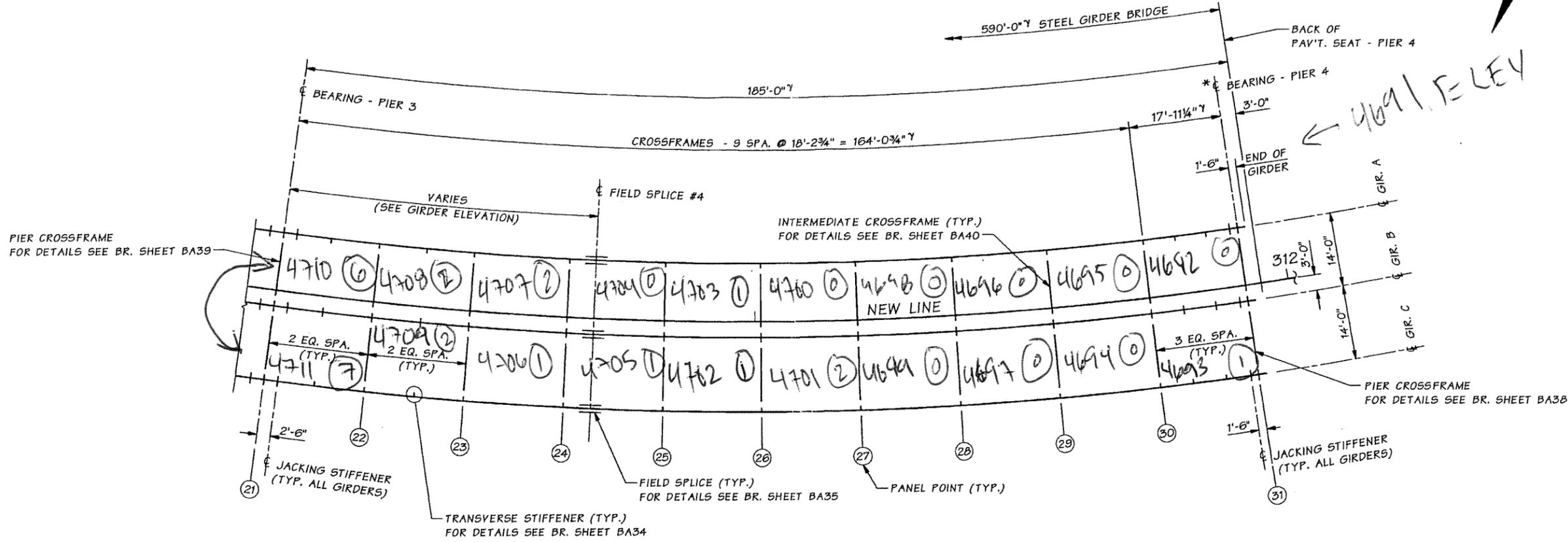


Washington State Department of Transportation

I-5 / SR 16 EB NALLEY VALLEY - HOV		BRIDGE SHEET NO. BA29
NEW LINE BRIDGE		SHEET 740
FRAMING PLAN SHEET 2 OF 3		OF 1341
		SHEETS

5/4345CD

GIRDER	RADIUS
A	628'-9 1/8"
B	642'-9 1/8"
C	656'-9 1/8"



FRAMING PLAN - SPAN 3

ALL CROSSFRAMES ARE NORMAL OR RADIAL TO NEW LINE
 γ MEASURED ALONG NEW LINE
 * PARALLEL TO BACK OF PAVEMENT SEAT

SR 16 FILE NO. 2587 SHEET BA30

Bridge Design Engr.	Khaleghi, B	M:\Z-Team\SR16 EB NV\NEW Line\window files\Framing Plan 3.WND
Supervisor	Zeldenrust, RP	
Designed By	Rosa, M	02/10
Checked By	Swett, GD	04/11
Detailed By	Foote, N	08/10
Bridge Projects Engr.		
Prelim. Plan By		
Architect/Specialist		
DATE	REVISION	BY APP'D

MICHAEL A. ROSA
 BRIDGE AND STRUCTURES OFFICE
 RICHARD P. ZELDENRUST
 WASHINGTON STATE DEPARTMENT OF TRANSPORTATION
 5/19/11

I-5 / SR 16 EB NALLEY VALLEY - HOV	BRIDGE SHEET NO. BA30
NEW LINE BRIDGE	SHEET 741 OF 1341 SHEETS
FRAMING PLAN SHEET 3 OF 3	

5/4345CD



Bridge #	5/434SCD	Bridge Name	SBCD Over SR 16 HOV & Ramps			Structure ID	0018189B	
Contract #	8189	Region	OR	Project Engineer	Neal Uhlmeier	Performance Deck Concrete?	Yes	
Contractor	Mowat Construction		Concrete Supplier	Holroyd Co.		Deck Placement	11/13, 2/19/13 & 2/26/	
Bridge Description	3-Span (185' / 220' / 185'), 3-Steel Plate Girders (590' bridge length), 1-Lane (34' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr} / N_{100} (rounded to the nearest 5%)

Avg. =	36%
Min. =	0%
Max. =	100%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	22.75	14.00	1	11	10%
1	1	B	C	22.75	14.00	1	11	10%
1	2	A	B	22.75	14.00	0	11	0%
1	2	B	C	22.75	14.00	0	11	0%
1	3	A	B	22.75	14.00	0	11	0%
1	3	B	C	22.75	14.00	0	11	0%
1	4	A	B	22.75	14.00	0	11	0%
1	4	B	C	22.75	14.00	0	11	0%
1	5	A	B	22.75	14.00	1	11	10%
1	5	B	C	22.75	14.00	0	11	0%
1	6	A	B	22.75	14.00	3	11	25%
1	6	B	C	22.75	14.00	3	11	25%
1	7	A	B	22.75	14.00	6	11	55%
1	7	B	C	22.75	14.00	4	11	35%
1	8	A	B	22.75	14.00	10	11	90%
1	8	B	C	22.75	14.00	8	11	75%
2	1	A	B	18.41	14.00	8	9	90%
2	1	B	C	18.41	14.00	11	9	100%
2	2	A	B	18.41	14.00	7	9	80%
2	2	B	C	18.41	14.00	5	9	55%
2	3	A	B	18.38	14.00	3	9	35%
2	3	B	C	18.38	14.00	5	9	55%
2	4	A	B	18.31	14.00	2	9	20%
2	4	B	C	18.31	14.00	3	9	35%
2	5	A	B	18.31	14.00	6	9	65%
2	5	B	C	18.31	14.00	9	9	100%
2	6	A	B	18.31	14.00	6	9	65%
2	6	B	C	18.31	14.00	11	9	100%
2	7	A	B	18.31	14.00	8	9	90%
2	7	B	C	18.31	14.00	12	9	100%
2	8	A	B	18.31	14.00	6	9	65%
2	8	B	C	18.31	14.00	11	9	100%
2	9	A	B	18.31	14.00	2	9	20%
2	9	B	C	18.31	14.00	5	9	55%
2	10	A	B	18.31	14.00	4	9	45%
2	10	B	C	18.31	14.00	2	9	20%
2	11	A	B	18.31	14.00	4	9	45%
2	11	B	C	18.31	14.00	4	9	45%
2	12	A	B	18.31	14.00	7	9	80%
2	12	B	C	18.31	14.00	5	9	55%
3	1	A	B	18.31	14.00	6	9	65%



Bridge #	5/434SCD	Bridge Name	SBCD Over SR 16 HOV & Ramps			Structure ID	0018189B	
Contract #	8189	Region	OR	Project Engineer	Neal Uhlmeier	Performance Deck Concrete?	Yes	
Contractor	Mowat Construction		Concrete Supplier	Holroyd Co.		Deck Placement	11/13, 2/19/13 & 2/26/	
Bridge Description	3-Span (185' / 220' / 185'), 3-Steel Plate Girders (590' bridge length), 1-Lane (34' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	36%
Min. =	0%
Max. =	100%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
3	1	B	C	18.31	14.00	7	9	80%
3	2	A	B	18.31	14.00	2	9	20%
3	2	B	C	18.31	14.00	2	9	20%
3	3	A	B	18.31	14.00	2	9	20%
3	3	B	C	18.31	14.00	1	9	10%
3	4	A	B	18.31	14.00	0	9	0%
3	4	B	C	18.31	14.00	1	9	10%
3	5	A	B	18.31	14.00	1	9	10%
3	5	B	C	18.31	14.00	1	9	10%
3	6	A	B	18.31	14.00	0	9	0%
3	6	B	C	18.31	14.00	2	9	20%
3	7	A	B	18.31	14.00	0	9	0%
3	7	B	C	18.31	14.00	0	9	0%
3	8	A	B	18.31	14.00	0	9	0%
3	8	B	C	18.31	14.00	0	9	0%
3	9	A	B	18.31	14.00	0	9	0%
3	9	B	C	18.31	14.00	0	9	0%
3	10	A	B	17.94	14.00	0	9	0%
3	10	B	C	17.94	14.00	1	9	10%

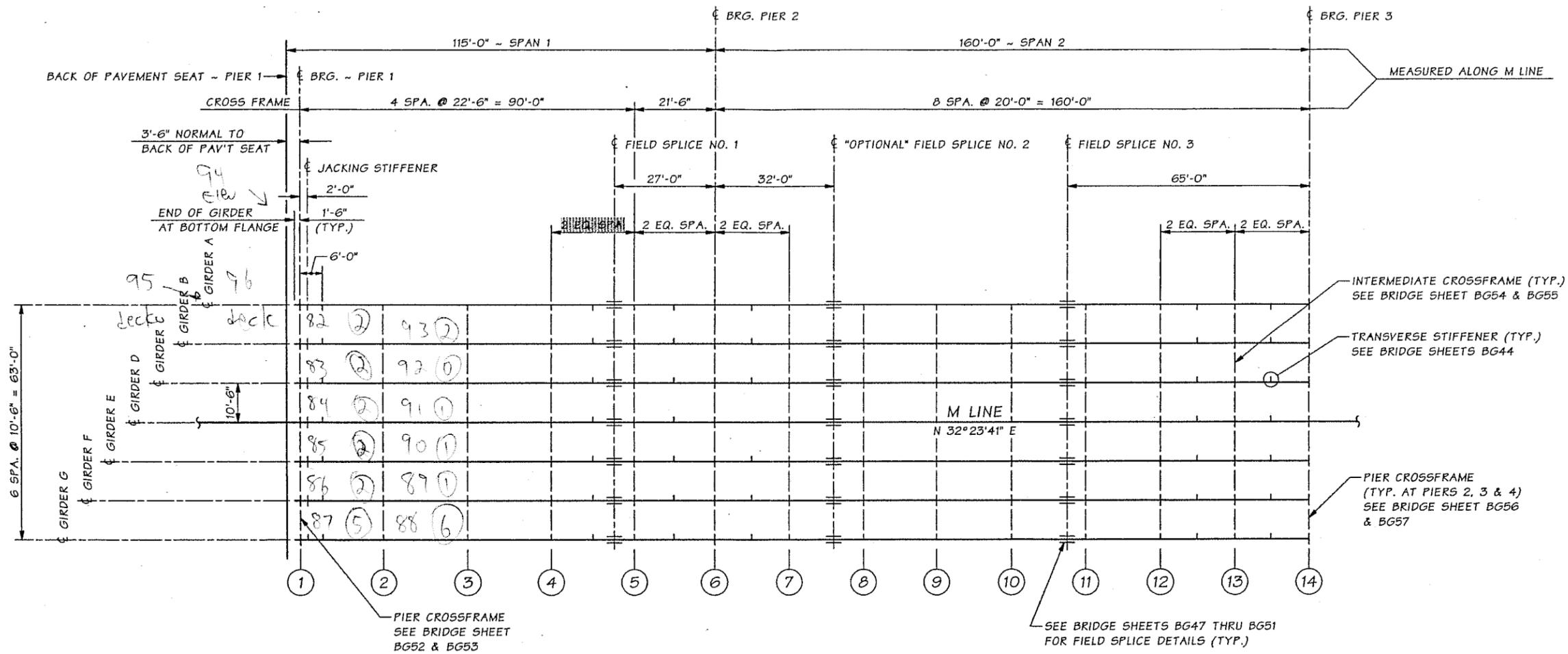
BRIDGE 529/25 (EBEY SLOUGH)

Bridge #	529/25	Bridge Name	Ebey Slough		Structure ID	0017948A	
Contract #	7948	Region	NW	Project Engineer	Mark Sawyer	Performance Deck Concrete?	No
Contractor	Granite Construction		Concrete Supplier		Deck Placement	≈ 2012	
Bridge Description	4-Span (115' / 160' / 160' / 170'), 7-Steel Plate Girders (680' bridge length), 4-Lanes (58' wide roadway)						



CONTENTS

1. Layout Plan Sheet
2. Field Notes
3. Crack Summary
4. Crack Intensity Diagram



GIRDER FRAMING PLAN ~ SPANS 1 & 2

ALL LENGTHS ARE MEASURED HORIZONTALLY AND ARE ALONG ϵ OF THE BRIDGE. CROSSFRAMES ARE PERPENDICULAR TO THE M LINE.

NOTE:

1 THRU 14 - \odot - INDICATES PANEL POINT.

SR 529 FILE NO. 7009 SHEET BG34

Bridge Design Engr.	KhaTeghi, B	M:\X-Team\EBEY SLOUGH BR 529-25 REPL\EBEY SLOUGH BR 529-25 REPL-C>window files\FRAMING PLAN 1.WND
Supervisor	Stoddard, RB	
Designed By	Bushnaq, AA 11/09	
Checked By	Tran, LH 04/10	
Detailed By	McCarthy, DJ 11/09	
Bridge Projects Engr.		
Prelim. Plan By	DA/10/10	ADDED TRANSVERSE STIFFENERS
Architect/Specialist	DATE	REVISION
	BY	APPD



BRIDGE AND STRUCTURES OFFICE

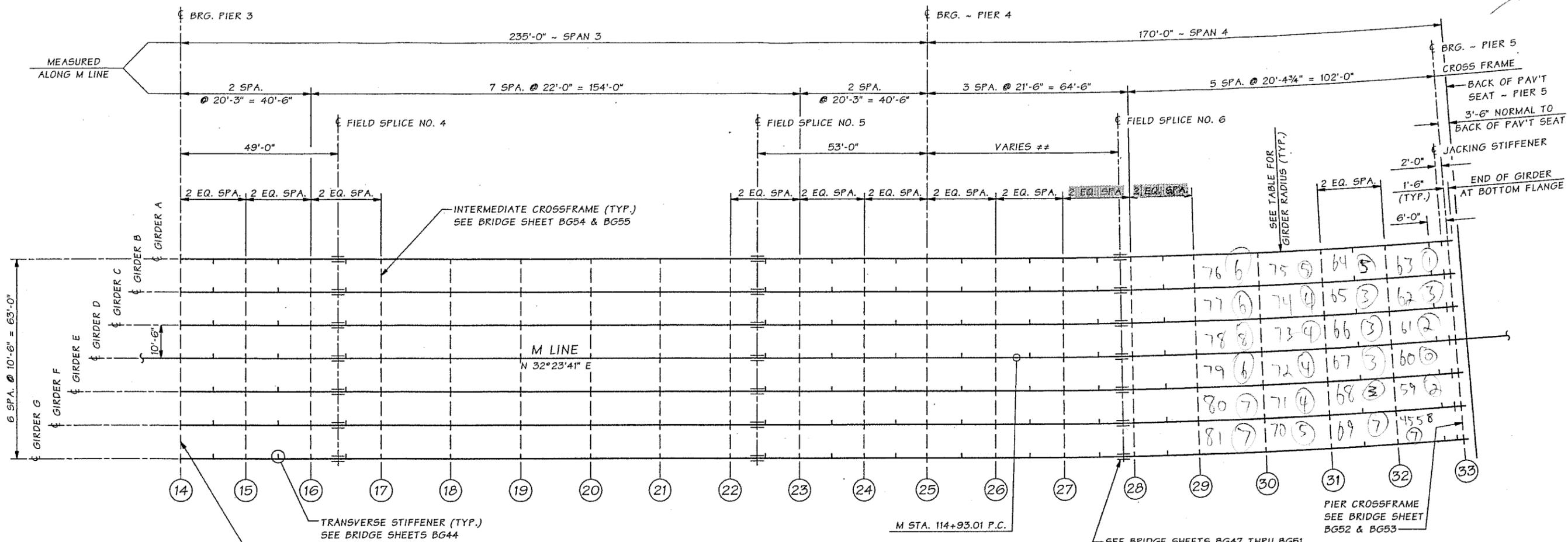


SR 529
EBEY SLOUGH BR. - REPLACE BRIDGE

EBEY SLOUGH BR. NO. 529/25 REPLACEMENT

FRAMING PLAN
DETAIL 1 OF 2

BRIDGE SHEET NO.	BG34
SHEET OF	193 OF 260
SHEETS	



GIRDER FRAMING PLAN ~ SPANS 3 & 4

ALL LENGTHS ARE MEASURED HORIZONTALLY AND ARE ALONG C OF THE BRIDGE. CROSSFRAMES 14 TO 26 ARE PERPENDICULAR TO THE M LINE AND 27 TO 33 ARE RADIAL TO THE M-LINE.

GIRDER	RADIUS
A	1718'-6"
B	1729'-0"
C	1739'-6"
D	1750'-0"
E	1760'-6"
F	1771'-0"
G	1781'-6"

NOTES:

14 THRU 33 - - INDICATES PANEL POINT.

SEE GIRDER ELEVATION SHEETS FOR DETAILS.

SR 529 FILE NO. 7009 SHEET BG35

Bridge Design Engr.	khalighi, B	M:\X-Team\EBEY SLOUGH BR 529-25 REPL\EBEY SLOUGH BR 529-25 REPL-C>window files\FRAMING PLAN 2.WND
Supervisor	Stoddard, RB	
Designed By	Bushnaq, AA	11/09
Checked By	Tran, LH	04/10
Detailed By	McCarthy, DJ	11/09
Bridge Projects Engr.		
Prelim. Plan By		
Architect/Specialist		
DATE	REVISION	BY APPD



BRIDGE AND STRUCTURES OFFICE



SR 529 EBEY SLOUGH BR. - REPLACE BRIDGE	BRIDGE SHEET NO. BG35
EBEY SLOUGH BR. NO. 529/25 REPLACEMENT	SHEET 194
FRAMING PLAN DETAIL 2 OF 2	OF 260
	SHEETS



Bridge #	529/25	Bridge Name	Ebey Slough			Structure ID	0017948A	
Contract #	7948	Region	NW	Project Engineer	Mark Sawyer	Performance Deck Concrete?	No	
Contractor	Granite Construction		Concrete Supplier			Deck Placement	≈ 2012	
Bridge Description	4-Span (115' / 160' / 160' / 170'), 7-Steel Plate Girders (680' bridge length), 4-Lanes (58' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	36%
Min. =	0%
Max. =	80%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	22.50	10.50	2	11	20%
1	1	B	C	22.50	10.50	2	11	20%
1	1	C	D	22.50	10.50	2	11	20%
1	1	D	E	22.50	10.50	2	11	20%
1	1	E	F	22.50	10.50	2	11	20%
1	1	F	G	22.50	10.50	5	11	45%
1	2	A	B	22.50	10.50	2	11	20%
1	2	B	C	22.50	10.50	0	11	0%
1	2	C	D	22.50	10.50	1	11	10%
1	2	D	E	22.50	10.50	1	11	10%
1	2	E	F	22.50	10.50	1	11	10%
1	2	F	G	22.50	10.50	6	11	55%
1	3	A	B	22.50	10.50	#N/A	11	#N/A
1	3	B	C	22.50	10.50	#N/A	11	#N/A
1	3	C	D	22.50	10.50	#N/A	11	#N/A
1	3	D	E	22.50	10.50	#N/A	11	#N/A
1	3	E	F	22.50	10.50	#N/A	11	#N/A
1	3	F	G	22.50	10.50	#N/A	11	#N/A
1	4	A	B	22.50	10.50	#N/A	11	#N/A
1	4	B	C	22.50	10.50	#N/A	11	#N/A
1	4	C	D	22.50	10.50	#N/A	11	#N/A
1	4	D	E	22.50	10.50	#N/A	11	#N/A
1	4	E	F	22.50	10.50	#N/A	11	#N/A
1	4	F	G	22.50	10.50	#N/A	11	#N/A
1	5	A	B	21.50	10.50	#N/A	11	#N/A
1	5	B	C	21.50	10.50	#N/A	11	#N/A
1	5	C	D	21.50	10.50	#N/A	11	#N/A
1	5	D	E	21.50	10.50	#N/A	11	#N/A
1	5	E	F	21.50	10.50	#N/A	11	#N/A
1	5	F	G	21.50	10.50	#N/A	11	#N/A
2	1	A	B	20.00	10.50	#N/A	10	#N/A
2	1	B	C	20.00	10.50	#N/A	10	#N/A
2	1	C	D	20.00	10.50	#N/A	10	#N/A
2	1	D	E	20.00	10.50	#N/A	10	#N/A
2	1	E	F	20.00	10.50	#N/A	10	#N/A
2	1	F	G	20.00	10.50	#N/A	10	#N/A
2	2	A	B	20.00	10.50	#N/A	10	#N/A
2	2	B	C	20.00	10.50	#N/A	10	#N/A
2	2	C	D	20.00	10.50	#N/A	10	#N/A
2	2	D	E	20.00	10.50	#N/A	10	#N/A
2	2	E	F	20.00	10.50	#N/A	10	#N/A



Bridge #	529/25	Bridge Name	Ebey Slough			Structure ID	0017948A	
Contract #	7948	Region	NW	Project Engineer	Mark Sawyer	Performance Deck Concrete?	No	
Contractor	Granite Construction		Concrete Supplier			Deck Placement	≈ 2012	
Bridge Description	4-Span (115' / 160' / 160' / 170'), 7-Steel Plate Girders (680' bridge length), 4-Lanes (58' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	36%
Min. =	0%
Max. =	80%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
2	2	F	G	20.00	10.50	#N/A	10	#N/A
2	3	A	B	20.00	10.50	#N/A	10	#N/A
2	3	B	C	20.00	10.50	#N/A	10	#N/A
2	3	C	D	20.00	10.50	#N/A	10	#N/A
2	3	D	E	20.00	10.50	#N/A	10	#N/A
2	3	E	F	20.00	10.50	#N/A	10	#N/A
2	3	F	G	20.00	10.50	#N/A	10	#N/A
2	4	A	B	20.00	10.50	#N/A	10	#N/A
2	4	B	C	20.00	10.50	#N/A	10	#N/A
2	4	C	D	20.00	10.50	#N/A	10	#N/A
2	4	D	E	20.00	10.50	#N/A	10	#N/A
2	4	E	F	20.00	10.50	#N/A	10	#N/A
2	4	F	G	20.00	10.50	#N/A	10	#N/A
2	5	A	B	20.00	10.50	#N/A	10	#N/A
2	5	B	C	20.00	10.50	#N/A	10	#N/A
2	5	C	D	20.00	10.50	#N/A	10	#N/A
2	5	D	E	20.00	10.50	#N/A	10	#N/A
2	5	E	F	20.00	10.50	#N/A	10	#N/A
2	5	F	G	20.00	10.50	#N/A	10	#N/A
2	6	A	B	20.00	10.50	#N/A	10	#N/A
2	6	B	C	20.00	10.50	#N/A	10	#N/A
2	6	C	D	20.00	10.50	#N/A	10	#N/A
2	6	D	E	20.00	10.50	#N/A	10	#N/A
2	6	E	F	20.00	10.50	#N/A	10	#N/A
2	6	F	G	20.00	10.50	#N/A	10	#N/A
2	7	A	B	20.00	10.50	#N/A	10	#N/A
2	7	B	C	20.00	10.50	#N/A	10	#N/A
2	7	C	D	20.00	10.50	#N/A	10	#N/A
2	7	D	E	20.00	10.50	#N/A	10	#N/A
2	7	E	F	20.00	10.50	#N/A	10	#N/A
2	7	F	G	20.00	10.50	#N/A	10	#N/A
2	8	A	B	20.00	10.50	#N/A	10	#N/A
2	8	B	C	20.00	10.50	#N/A	10	#N/A
2	8	C	D	20.00	10.50	#N/A	10	#N/A
2	8	D	E	20.00	10.50	#N/A	10	#N/A
2	8	E	F	20.00	10.50	#N/A	10	#N/A
2	8	F	G	20.00	10.50	#N/A	10	#N/A
3	1	A	B	20.25	10.50	#N/A	10	#N/A
3	1	B	C	20.25	10.50	#N/A	10	#N/A
3	1	C	D	20.25	10.50	#N/A	10	#N/A
3	1	D	E	20.25	10.50	#N/A	10	#N/A



Bridge #	529/25	Bridge Name	Ebey Slough			Structure ID	0017948A	
Contract #	7948	Region	NW	Project Engineer	Mark Sawyer	Performance Deck Concrete?	No	
Contractor	Granite Construction		Concrete Supplier				Deck Placement	≈ 2012
Bridge Description	4-Span (115' / 160' / 160' / 170'), 7-Steel Plate Girders (680' bridge length), 4-Lanes (58' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	36%
Min. =	0%
Max. =	80%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
3	1	E	F	20.25	10.50	#N/A	10	#N/A
3	1	F	G	20.25	10.50	#N/A	10	#N/A
3	2	A	B	20.25	10.50	#N/A	10	#N/A
3	2	B	C	20.25	10.50	#N/A	10	#N/A
3	2	C	D	20.25	10.50	#N/A	10	#N/A
3	2	D	E	20.25	10.50	#N/A	10	#N/A
3	2	E	F	20.25	10.50	#N/A	10	#N/A
3	2	F	G	20.25	10.50	#N/A	10	#N/A
3	3	A	B	22.00	10.50	#N/A	11	#N/A
3	3	B	C	22.00	10.50	#N/A	11	#N/A
3	3	C	D	22.00	10.50	#N/A	11	#N/A
3	3	D	E	22.00	10.50	#N/A	11	#N/A
3	3	E	F	22.00	10.50	#N/A	11	#N/A
3	3	F	G	22.00	10.50	#N/A	11	#N/A
3	4	A	B	22.00	10.50	#N/A	11	#N/A
3	4	B	C	22.00	10.50	#N/A	11	#N/A
3	4	C	D	22.00	10.50	#N/A	11	#N/A
3	4	D	E	22.00	10.50	#N/A	11	#N/A
3	4	E	F	22.00	10.50	#N/A	11	#N/A
3	4	F	G	22.00	10.50	#N/A	11	#N/A
3	5	A	B	22.00	10.50	#N/A	11	#N/A
3	5	B	C	22.00	10.50	#N/A	11	#N/A
3	5	C	D	22.00	10.50	#N/A	11	#N/A
3	5	D	E	22.00	10.50	#N/A	11	#N/A
3	5	E	F	22.00	10.50	#N/A	11	#N/A
3	5	F	G	22.00	10.50	#N/A	11	#N/A
3	6	A	B	22.00	10.50	#N/A	11	#N/A
3	6	B	C	22.00	10.50	#N/A	11	#N/A
3	6	C	D	22.00	10.50	#N/A	11	#N/A
3	6	D	E	22.00	10.50	#N/A	11	#N/A
3	6	E	F	22.00	10.50	#N/A	11	#N/A
3	6	F	G	22.00	10.50	#N/A	11	#N/A
3	7	A	B	22.00	10.50	#N/A	11	#N/A
3	7	B	C	22.00	10.50	#N/A	11	#N/A
3	7	C	D	22.00	10.50	#N/A	11	#N/A
3	7	D	E	22.00	10.50	#N/A	11	#N/A
3	7	E	F	22.00	10.50	#N/A	11	#N/A
3	7	F	G	22.00	10.50	#N/A	11	#N/A
3	8	A	B	22.00	10.50	#N/A	11	#N/A
3	8	B	C	22.00	10.50	#N/A	11	#N/A
3	8	C	D	22.00	10.50	#N/A	11	#N/A



Bridge #	529/25	Bridge Name	Ebey Slough			Structure ID	0017948A	
Contract #	7948	Region	NW	Project Engineer	Mark Sawyer	Performance Deck Concrete?	No	
Contractor	Granite Construction		Concrete Supplier			Deck Placement	≈ 2012	
Bridge Description	4-Span (115' / 160' / 160' / 170'), 7-Steel Plate Girders (680' bridge length), 4-Lanes (58' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	36%
Min. =	0%
Max. =	80%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
3	8	D	E	22.00	10.50	#N/A	11	#N/A
3	8	E	F	22.00	10.50	#N/A	11	#N/A
3	8	F	G	22.00	10.50	#N/A	11	#N/A
3	9	A	B	22.00	10.50	#N/A	11	#N/A
3	9	B	C	22.00	10.50	#N/A	11	#N/A
3	9	C	D	22.00	10.50	#N/A	11	#N/A
3	9	D	E	22.00	10.50	#N/A	11	#N/A
3	9	E	F	22.00	10.50	#N/A	11	#N/A
3	9	F	G	22.00	10.50	#N/A	11	#N/A
3	10	A	B	20.25	10.50	#N/A	10	#N/A
3	10	B	C	20.25	10.50	#N/A	10	#N/A
3	10	C	D	20.25	10.50	#N/A	10	#N/A
3	10	D	E	20.25	10.50	#N/A	10	#N/A
3	10	E	F	20.25	10.50	#N/A	10	#N/A
3	10	F	G	20.25	10.50	#N/A	10	#N/A
3	11	A	B	20.25	10.50	#N/A	10	#N/A
3	11	B	C	20.25	10.50	#N/A	10	#N/A
3	11	C	D	20.25	10.50	#N/A	10	#N/A
3	11	D	E	20.25	10.50	#N/A	10	#N/A
3	11	E	F	20.25	10.50	#N/A	10	#N/A
3	11	F	G	20.25	10.50	#N/A	10	#N/A
4	1	A	B	21.50	10.50	#N/A	11	#N/A
4	1	B	C	21.50	10.50	#N/A	11	#N/A
4	1	C	D	21.50	10.50	#N/A	11	#N/A
4	1	D	E	21.50	10.50	#N/A	11	#N/A
4	1	E	F	21.50	10.50	#N/A	11	#N/A
4	1	F	G	21.50	10.50	#N/A	11	#N/A
4	2	A	B	21.50	10.50	#N/A	11	#N/A
4	2	B	C	21.50	10.50	#N/A	11	#N/A
4	2	C	D	21.50	10.50	#N/A	11	#N/A
4	2	D	E	21.50	10.50	#N/A	11	#N/A
4	2	E	F	21.50	10.50	#N/A	11	#N/A
4	2	F	G	21.50	10.50	#N/A	11	#N/A
4	3	A	B	21.50	10.50	#N/A	11	#N/A
4	3	B	C	21.50	10.50	#N/A	11	#N/A
4	3	C	D	21.50	10.50	#N/A	11	#N/A
4	3	D	E	21.50	10.50	#N/A	11	#N/A
4	3	E	F	21.50	10.50	#N/A	11	#N/A
4	3	F	G	21.50	10.50	#N/A	11	#N/A
4	4	A	B	20.40	10.50	#N/A	10	#N/A
4	4	B	C	20.40	10.50	#N/A	10	#N/A



Bridge #	529/25	Bridge Name	Ebey Slough			Structure ID	0017948A	
Contract #	7948	Region	NW	Project Engineer	Mark Sawyer	Performance Deck Concrete?	No	
Contractor	Granite Construction		Concrete Supplier			Deck Placement	≈ 2012	
Bridge Description	4-Span (115' / 160' / 160' / 170'), 7-Steel Plate Girders (680' bridge length), 4-Lanes (58' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

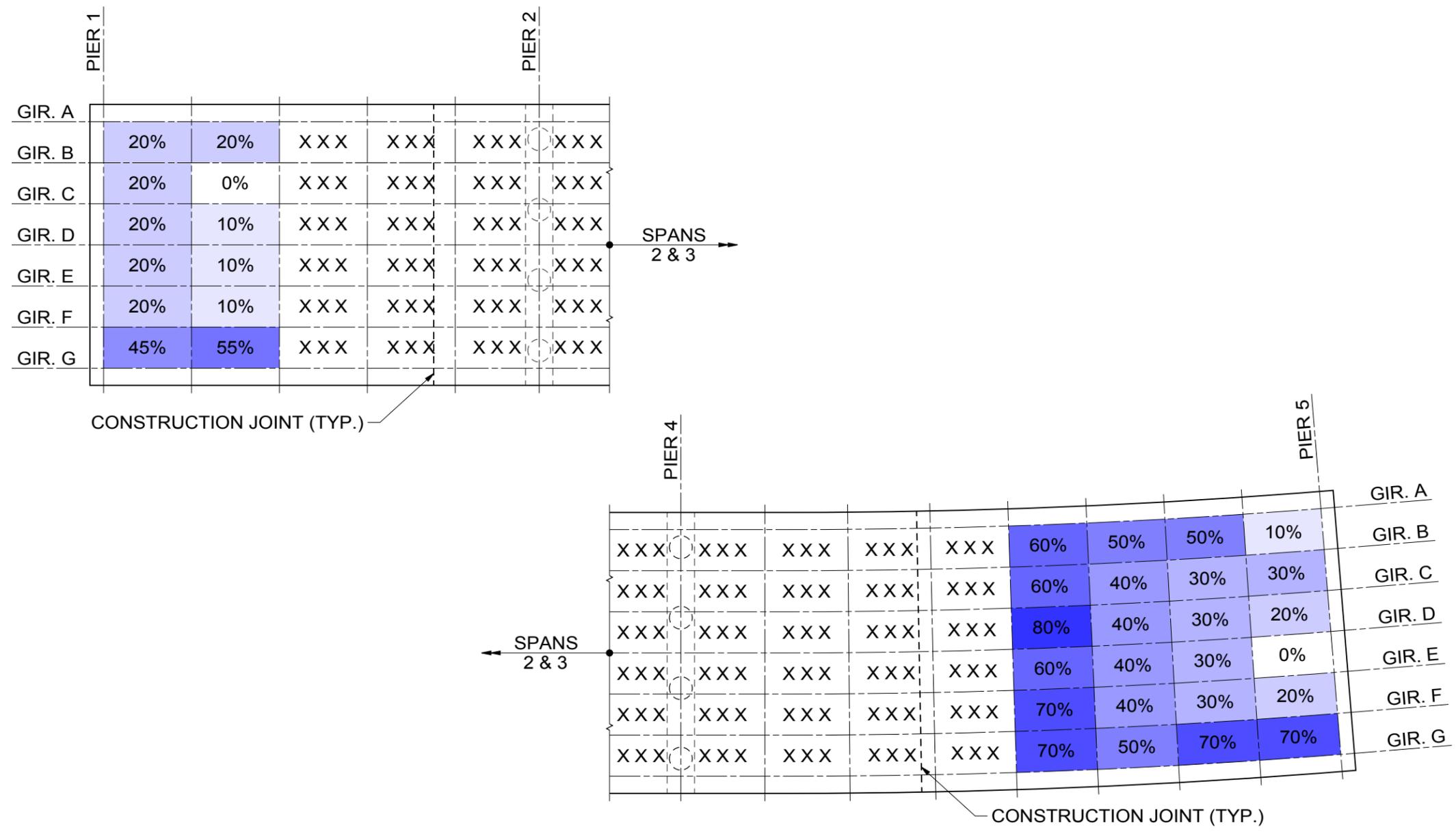
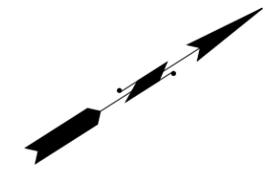
N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	36%
Min. =	0%
Max. =	80%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
4	4	C	D	20.40	10.50	#N/A	10	#N/A
4	4	D	E	20.40	10.50	#N/A	10	#N/A
4	4	E	F	20.40	10.50	#N/A	10	#N/A
4	4	F	G	20.40	10.50	#N/A	10	#N/A
4	5	A	B	20.40	10.50	6	10	60%
4	5	B	C	20.40	10.50	6	10	60%
4	5	C	D	20.40	10.50	8	10	80%
4	5	D	E	20.40	10.50	6	10	60%
4	5	E	F	20.40	10.50	7	10	70%
4	5	F	G	20.40	10.50	7	10	70%
4	6	A	B	20.40	10.50	5	10	50%
4	6	B	C	20.40	10.50	4	10	40%
4	6	C	D	20.40	10.50	4	10	40%
4	6	D	E	20.40	10.50	4	10	40%
4	6	E	F	20.40	10.50	4	10	40%
4	6	F	G	20.40	10.50	5	10	50%
4	7	A	B	20.40	10.50	5	10	50%
4	7	B	C	20.40	10.50	3	10	30%
4	7	C	D	20.40	10.50	3	10	30%
4	7	D	E	20.40	10.50	3	10	30%
4	7	E	F	20.40	10.50	3	10	30%
4	7	F	G	20.40	10.50	7	10	70%
4	8	A	B	20.40	10.50	1	10	10%
4	8	B	C	20.40	10.50	3	10	30%
4	8	C	D	20.40	10.50	2	10	20%
4	8	D	E	20.40	10.50	0	10	0%
4	8	E	F	20.40	10.50	2	10	20%
4	8	F	G	20.40	10.50	7	10	70%



CRACKING INTENSITY ~ BRIDGE 529/25

100% = CRACK EVERY 2 FT.

XXX = CRACKS NOT COUNTED DUE TO LIMITED ACCESS

SPANS 2 AND 3 NOT SHOWN FOR CLARITY



BRIDGE NUMBER	529/25
BRIDGE NAME	EBEY SLOUGH
INSPECTION DATE	5/22/2015
DECK CONCRETE	TRADITIONAL

BRIDGE 2/651W-S (W-S RAMP OVER US 2 / US 395)

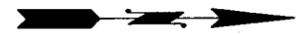
Bridge #	2/651W-S	Bridge Name	W-S Ramp over US 2/ US 395		Structure ID	0017610D	
Contract #	7610	Region	ER	Project Engineer	Bob Hilmes	Performance Deck Concrete?	No
Contractor	Graham Construction		Concrete Supplier		Deck Placement		≈ 2011
Bridge Description	6-Span (130' / 180' / 180' / 180' / 180' / 130'), 3-Steel Plate Girders (980' bridge length), 2-Lanes (38' wide roadway)						



CONTENTS

1. Layout Plan Sheet
2. Field Notes
3. Crack Summary
4. Crack Intensity Diagram

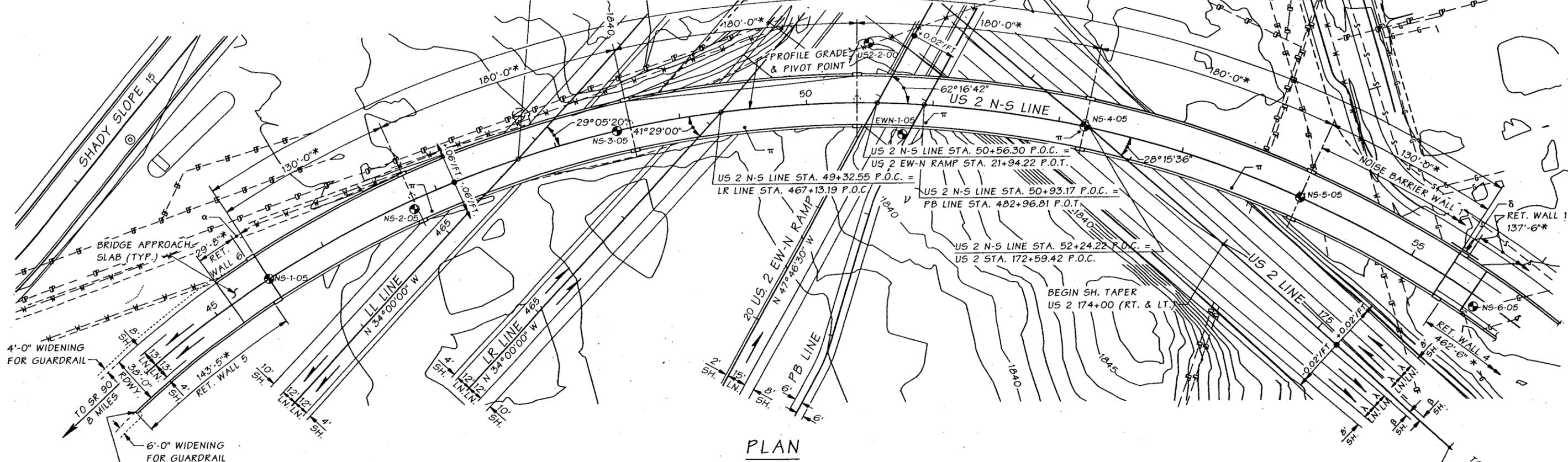
SEC. 4, T.26N., R.43E., W.M.
SPOKANE COUNTY



US 395

US 2 N-S LINE STA. 47+68.28 P.O.C. =
LL LINE STA. 465+79.47 P.O.T.

980'-0" BK. TO BK. OF PAV'T. SEATS *



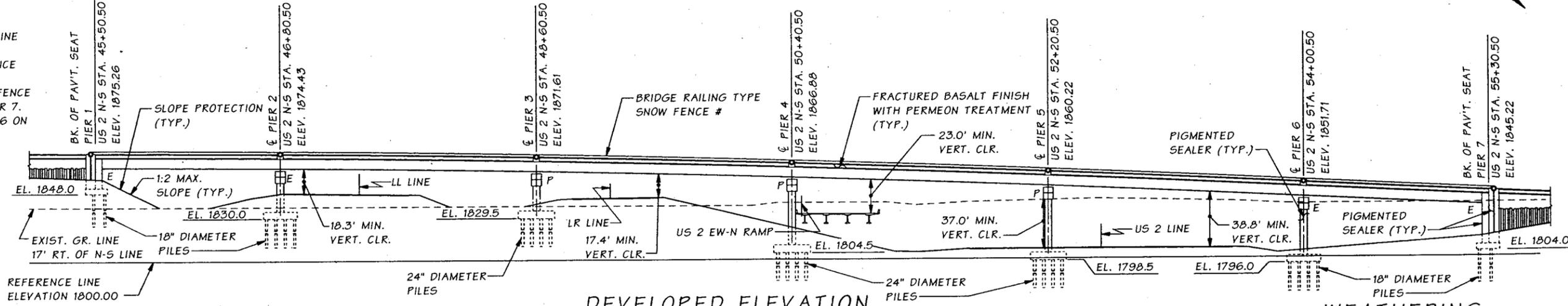
PLAN

BEARING OF ALL PIERS RADIAL TO N-S LINE.

LEGEND

- ⊙ = TEST HOLE
- * = MEASURED ALONG US 2 N-S LINE
- π = POINT OF MIN. VERT. CLEARANCE
- # = BRIDGE RAILING TYPE SNOW FENCE EXTENDS FROM PIER 1 TO PIER 7. ON RT. BARRIER & PIER 1 TO 6 ON LT. BARRIER.
- α = 7'-0" CURTAIN WALL (TYP. 4 CORNERS)
- β = 4'-0" SHOULDER
- λ = 11'-6" LANE
- δ = +20' TALL SHORING WALL

THREE BEAM GUARDRAIL CONNECTION TYPE "D". SEE STD. PLAN (TYP. 2 LOCATIONS)



DEVELOPED ELEVATION

GRADE ELEVATIONS SHOWN ARE FINISH GRADES AT TOP OF ROADWAY SLAB ON US 2 N-S LINE AND ARE EQUAL TO PROFILE GRADE. SEE BRIDGE SHEET NS3 FOR EMBANKMENT DETAILS AT BRIDGE ENDS.

WEATHERING
STEEL PLATE GIRDER
LOADING HL - 93

NOTE: CURVE DATA, PROFILES, AND SUPERELEVATION DIAGRAMS ARE ON SHEET NS2.

DATUM
N.A.V.D. OF 1988/1991

SR 2 FILE NO. 7235 SHEET NS1

Bridge Design Engr. Kha'teghi, B	M:\Z-Team\NSC - SR 395\PS&E\N-S RAMP STEEL\window files\LAYOUI.WND	REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
Supervisor Zeldenrust, RP		10	WASH.			
Designed By Rochon, MJ	09/07	JOB NUMBER 082011				
Checked By Bennion, S	07/08					
Detailed By Stitham, A	10/07					
Bridge Projects Engr. Lewis, RA	09/07					
Prefim. Plan By Rochon, MJ	10/07					
Architect/Specialist Kinderman, P	DATE	REVISION	BY	APPD		

BRIDGE AND STRUCTURES OFFICE

8/7/08

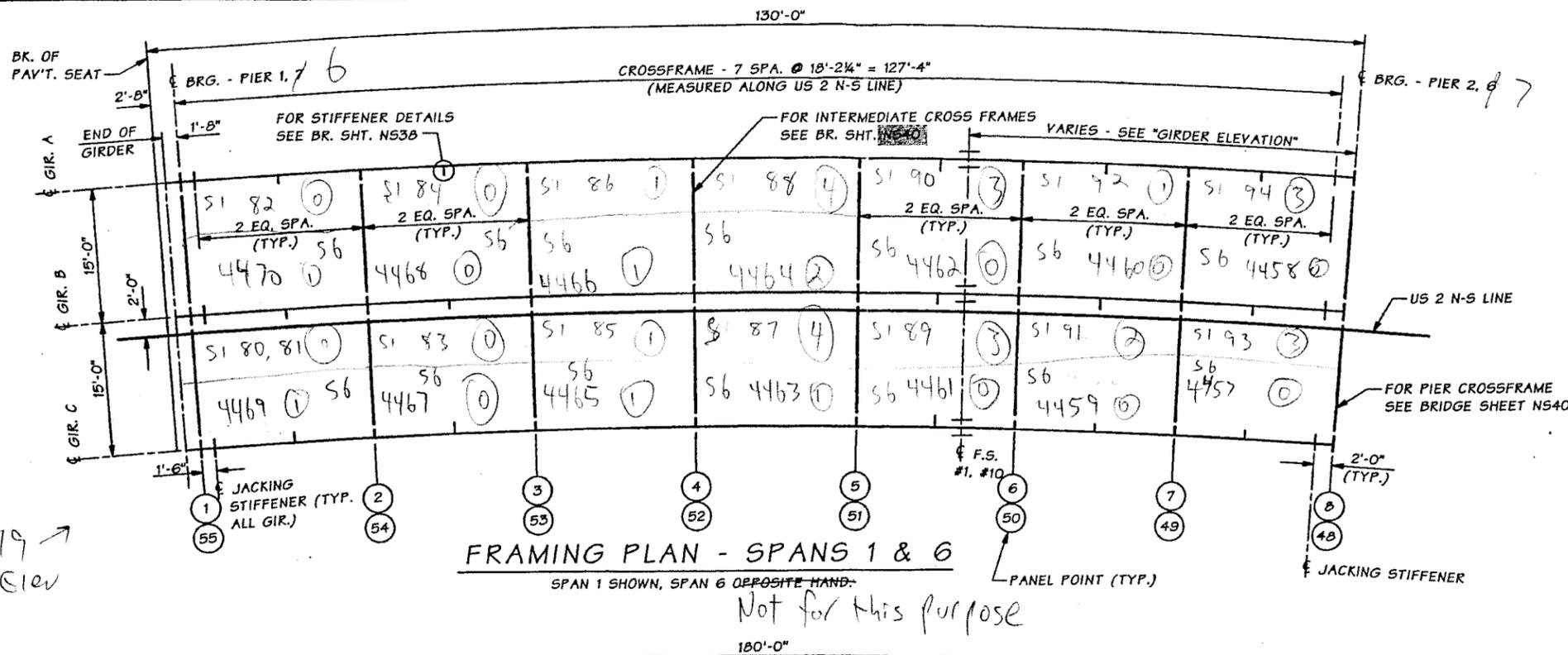
Washington State Department of Transportation

US 395
NSC - US 2 LOWERING
N-S RAMP OVER US 2 AND US 395 BRIDGE
LAYOUT

BRIDGE SHEET NO. NS1
SHEET 364 OF 548 SHEETS

C.S. 3208 ~ PROJ. NO. XL2231 ~ EASTERN REGION ~ M.P. 295.90 TO M.P. 296.01 ~ SR 2 ~ N-S RAMP BRIDGE.

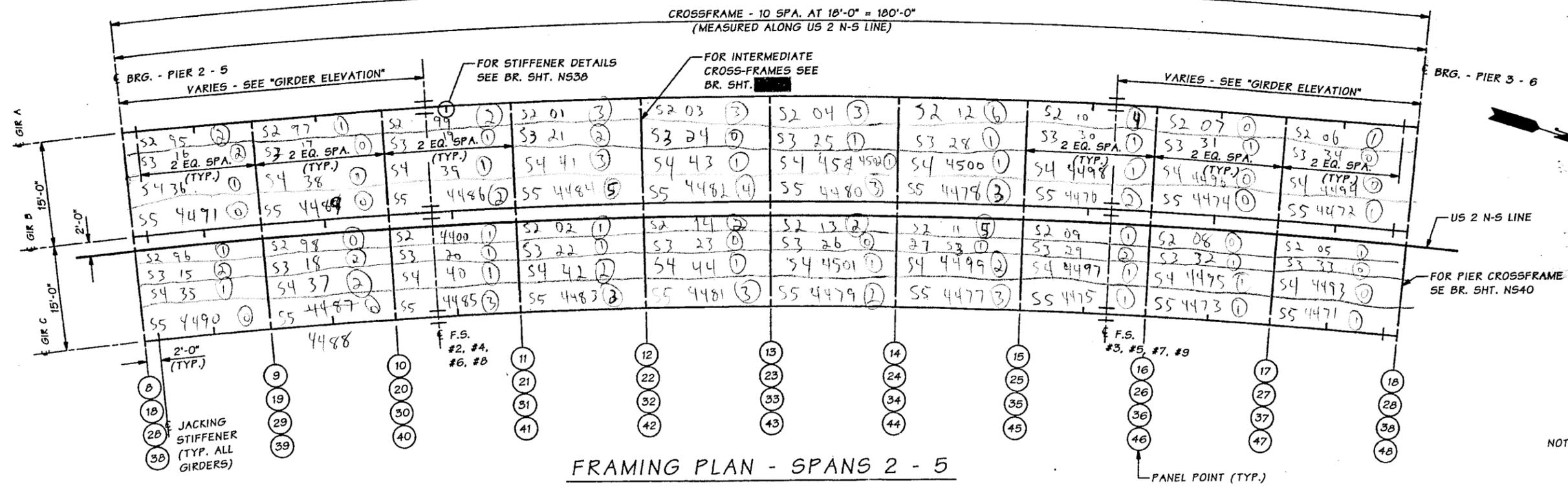
GIRDER	RADIUS
A	867'-0"
B	852'-0"
C	837'-0"



19 ->
elev

FRAMING PLAN - SPANS 1 & 6

180'-0"



FRAMING PLAN - SPANS 2 - 5

NOTE: F.S. = FIELD SPLICE

SR 2 FILE NO. 7235 SHEET NS36

Bridge Design Engr.	Khalighi, B	M:\z-Team\NSC - SR 395\PS&E\N-S RAMP STEEL>window files\FRAMING PLAN 1.WND
Supervisor	Zelidrust, RP	
Designed By	Rochon, MJ	09/07
Checked By	Brown, NS	07/08
Detailed By	Andreotti, L	09/07
Bridge Projects Engr.		
Prelim. Plan By		9/08
Architect/Specialist		

REVISION	DATE	BY	APPD
1	9/08		
2			
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BRIDGE AND STRUCTURES OFFICE

9/4/08

Washington State Department of Transportation

US 395
NSC - US 2 LOWERING

N-S RAMP OVER US 2 AND US 395 BRIDGE

FRAMING PLAN

BRIDGE SHEET NO. NS36

SHEET 399 OF 548 SHEETS

2/651-W-5



Bridge #	2/651W-S	Bridge Name	W-S Ramp over US 2/ US 395			Structure ID	0017610D	
Contract #	7610	Region	ER	Project Engineer	Bob Hilmes	Performance Deck Concrete?	No	
Contractor	Graham Construction		Concrete Supplier			Deck Placement	≈ 2011	
Bridge Description	6-Span (130' / 180' / 180' / 180' / 180' / 130'), 3-Steel Plate Girders (980' bridge length), 2-Lanes (38' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	13%
Min. =	0%
Max. =	65%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
1	1	A	B	18.19	15.00	0	9	0%
1	1	B	C	18.19	15.00	0	9	0%
1	2	A	B	18.19	15.00	0	9	0%
1	2	B	C	18.19	15.00	0	9	0%
1	3	A	B	18.19	15.00	1	9	10%
1	3	B	C	18.19	15.00	1	9	10%
1	4	A	B	18.19	15.00	4	9	45%
1	4	B	C	18.19	15.00	4	9	45%
1	5	A	B	18.19	15.00	2	9	20%
1	5	B	C	18.19	15.00	2	9	20%
1	6	A	B	18.19	15.00	1	9	10%
1	6	B	C	18.19	15.00	2	9	20%
1	7	A	B	18.19	15.00	3	9	35%
1	7	B	C	18.19	15.00	3	9	35%
2	1	A	B	18.00	15.00	2	9	20%
2	1	B	C	18.00	15.00	1	9	10%
2	2	A	B	18.00	15.00	1	9	10%
2	2	B	C	18.00	15.00	0	9	0%
2	3	A	B	18.00	15.00	2	9	20%
2	3	B	C	18.00	15.00	1	9	10%
2	4	A	B	18.00	15.00	2	9	20%
2	4	B	C	18.00	15.00	0	9	0%
2	5	A	B	18.00	15.00	3	9	35%
2	5	B	C	18.00	15.00	2	9	20%
2	6	A	B	18.00	15.00	3	9	35%
2	6	B	C	18.00	15.00	2	9	20%
2	7	A	B	18.00	15.00	6	9	65%
2	7	B	C	18.00	15.00	5	9	55%
2	8	A	B	18.00	15.00	3	9	35%
2	8	B	C	18.00	15.00	0	9	0%
2	9	A	B	18.00	15.00	0	9	0%
2	9	B	C	18.00	15.00	0	9	0%
2	10	A	B	18.00	15.00	1	9	10%
2	10	B	C	18.00	15.00	1	9	10%
3	1	A	B	18.00	15.00	2	9	20%
3	1	B	C	18.00	15.00	2	9	20%
3	2	A	B	18.00	15.00	0	9	0%
3	2	B	C	18.00	15.00	2	9	20%
3	3	A	B	18.00	15.00	0	9	0%
3	3	B	C	18.00	15.00	0	9	0%

← construction joint counte



Bridge #	2/651W-S	Bridge Name	W-S Ramp over US 2/ US 395			Structure ID	0017610D	
Contract #	7610	Region	ER	Project Engineer	Bob Hilmes	Performance Deck Concrete?	No	
Contractor	Graham Construction		Concrete Supplier			Deck Placement	≈ 2011	
Bridge Description	6-Span (130' / 180' / 180' / 180' / 180' / 130'), 3-Steel Plate Girders (980' bridge length), 2-Lanes (38' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	13%
Min. =	0%
Max. =	65%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
3	4	A	B	18.00	15.00	2	9	20%
3	4	B	C	18.00	15.00	1	9	10%
3	5	A	B	18.00	15.00	0	9	0%
3	5	B	C	18.00	15.00	0	9	0%
3	6	A	B	18.00	15.00	1	9	10%
3	6	B	C	18.00	15.00	0	9	0%
3	7	A	B	18.00	15.00	1	9	10%
3	7	B	C	18.00	15.00	1	9	10%
3	8	A	B	18.00	15.00	0	9	0%
3	8	B	C	18.00	15.00	1	9	10%
3	9	A	B	18.00	15.00	1	9	10%
3	9	B	C	18.00	15.00	1	9	10%
3	10	A	B	18.00	15.00	0	9	0%
3	10	B	C	18.00	15.00	0	9	0%
4	1	A	B	18.00	15.00	1	9	10%
4	1	B	C	18.00	15.00	1	9	10%
4	2	A	B	18.00	15.00	1	9	10%
4	2	B	C	18.00	15.00	2	9	20%
4	3	A	B	18.00	15.00	0	9	0%
4	3	B	C	18.00	15.00	0	9	0%
4	4	A	B	18.00	15.00	3	9	35%
4	4	B	C	18.00	15.00	2	9	20%
4	5	A	B	18.00	15.00	1	9	10%
4	5	B	C	18.00	15.00	1	9	10%
4	6	A	B	18.00	15.00	1	9	10%
4	6	B	C	18.00	15.00	1	9	10%
4	7	A	B	18.00	15.00	1	9	10%
4	7	B	C	18.00	15.00	2	9	20%
4	8	A	B	18.00	15.00	0	9	0%
4	8	B	C	18.00	15.00	0	9	0%
4	9	A	B	18.00	15.00	0	9	0%
4	9	B	C	18.00	15.00	1	9	10%
4	10	A	B	18.00	15.00	0	9	0%
4	10	B	C	18.00	15.00	0	9	0%
5	1	A	B	18.00	15.00	0	9	0%
5	1	B	C	18.00	15.00	0	9	0%
5	2	A	B	18.00	15.00	0	9	0%
5	2	B	C	18.00	15.00	0	9	0%
5	3	A	B	18.00	15.00	1	9	10%
5	3	B	C	18.00	15.00	2	9	20%
5	4	A	B	18.00	15.00	5	9	55%

← construction joint counte



Bridge #	2/651W-S	Bridge Name	W-S Ramp over US 2/ US 395			Structure ID	0017610D	
Contract #	7610	Region	ER	Project Engineer	Bob Hilmes	Performance Deck Concrete?	No	
Contractor	Graham Construction		Concrete Supplier				Deck Placement	≈ 2011
Bridge Description	6-Span (130' / 180' / 180' / 180' / 180' / 130'), 3-Steel Plate Girders (980' bridge length), 2-Lanes (38' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	13%
Min. =	0%
Max. =	65%

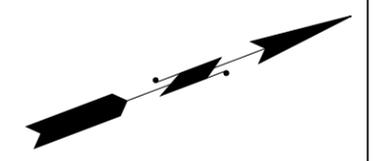
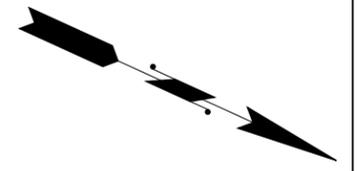
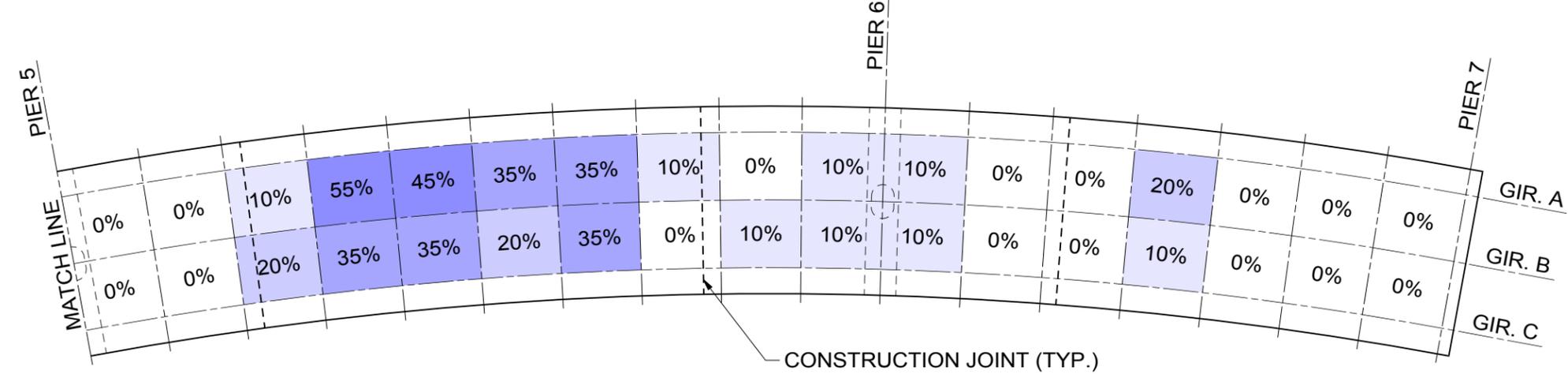
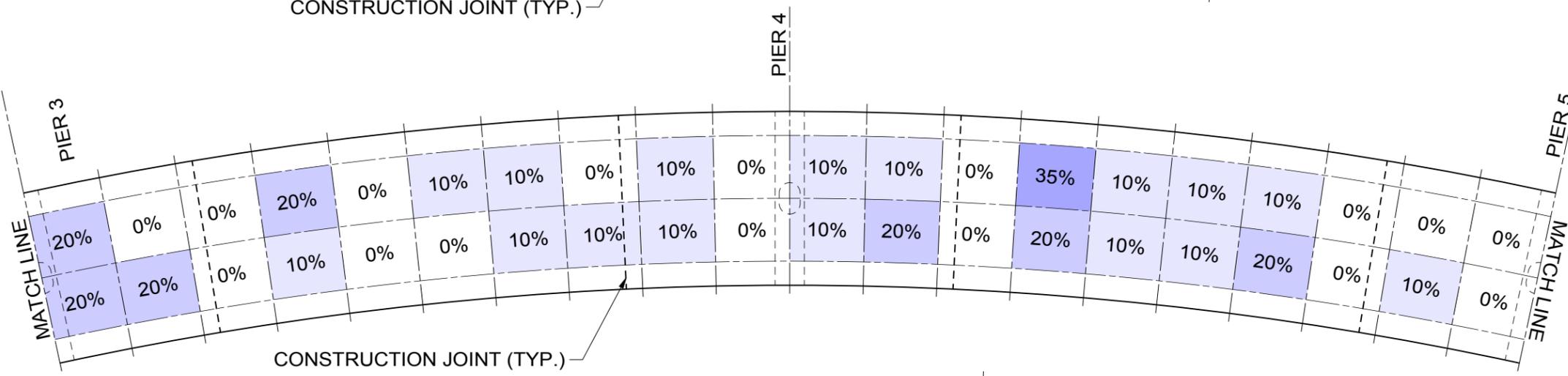
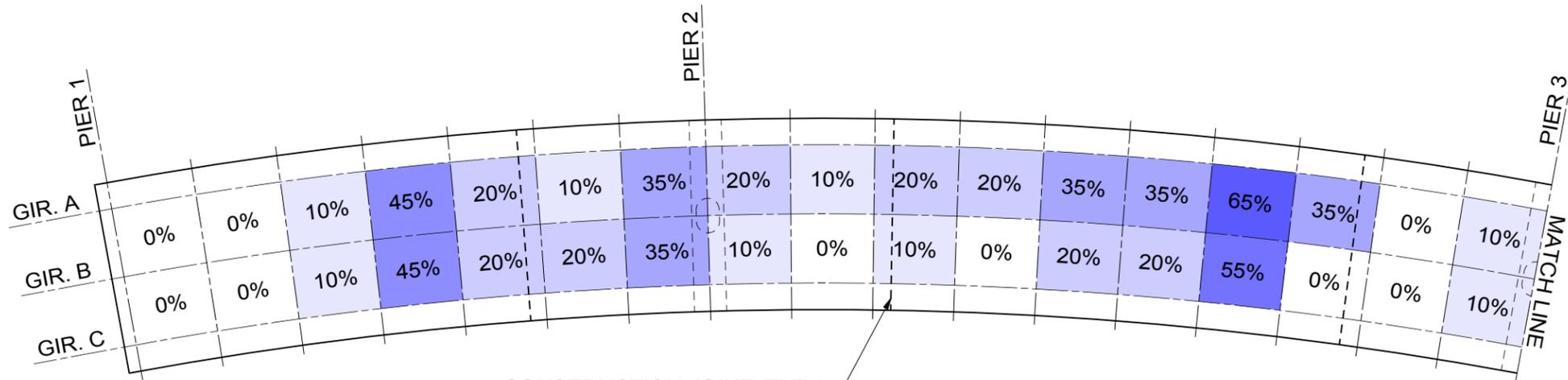
Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
5	4	B	C	18.00	15.00	3	9	35%
5	5	A	B	18.00	15.00	4	9	45%
5	5	B	C	18.00	15.00	3	9	35%
5	6	A	B	18.00	15.00	3	9	35%
5	6	B	C	18.00	15.00	2	9	20%
5	7	A	B	18.00	15.00	3	9	35%
5	7	B	C	18.00	15.00	3	9	35%
5	8	A	B	18.00	15.00	1	9	10%
5	8	B	C	18.00	15.00	0	9	0%
5	9	A	B	18.00	15.00	0	9	0%
5	9	B	C	18.00	15.00	1	9	10%
5	10	A	B	18.00	15.00	1	9	10%
5	10	B	C	18.00	15.00	1	9	10%
6	1	A	B	18.00	15.00	1	9	10%
6	1	B	C	18.00	15.00	1	9	10%
6	2	A	B	18.00	15.00	0	9	0%
6	2	B	C	18.00	15.00	0	9	0%
6	3	A	B	18.00	15.00	0	9	0%
6	3	B	C	18.00	15.00	0	9	0%
6	4	A	B	18.00	15.00	2	9	20%
6	4	B	C	18.00	15.00	1	9	10%
6	5	A	B	18.00	15.00	0	9	0%
6	5	B	C	18.00	15.00	0	9	0%
6	6	A	B	18.00	15.00	0	9	0%
6	6	B	C	18.00	15.00	0	9	0%
6	7	A	B	18.00	15.00	0	9	0%
6	7	B	C	18.00	15.00	0	9	0%

← construction joint count

← construction joint count

← construction joint count

← construction joint count



CRACKING INTENSITY ~ BRIDGE 2/651W-S

100% = CRACK EVERY 2 FT.

LESS CRACKING

MORE CRACKING



BRIDGE NUMBER	2/651W-S
BRIDGE NAME	W-S RAMP OVER US 2/US 395
INSPECTION DATE	5/21/2015
DECK CONCRETE	TRADITIONAL

BRIDGE 9/134 (PILCHUCK CREEK)

Bridge #	9/134	Bridge Name	Pilchuck Creek		Structure ID	0018363A	
Contract #	8383	Region	NW	Project Engineer	Dave Crisman	Performance Deck Concrete?	Yes
Contractor	Granite Construction		Concrete Supplier	Stanwood Redi-Mix		Deck Placement	11/27/13, 12/11/13 & 1/14/14
Bridge Description	3-Span (170' / 220' / 170'), 3-Steel Plate Girders (560' bridge length), 2-Lanes (36' wide roadway)						



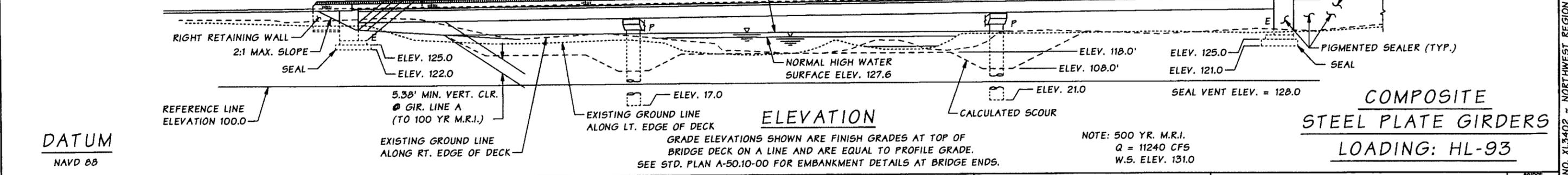
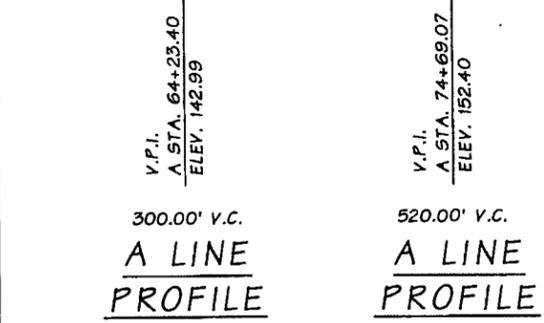
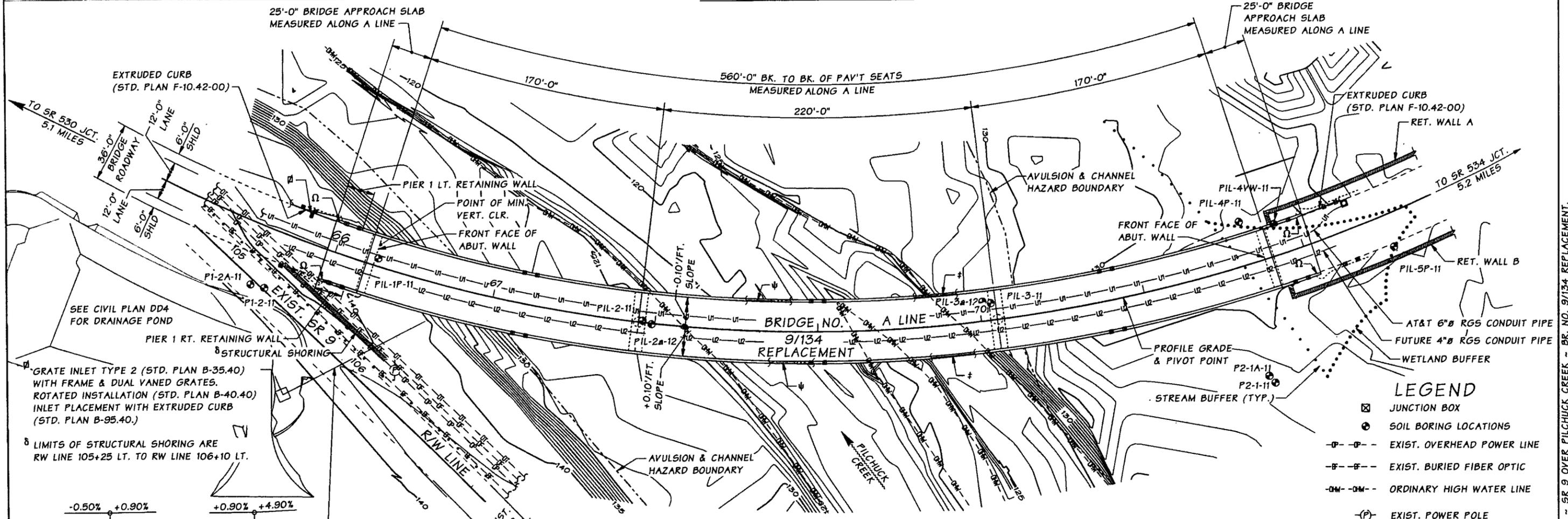
CONTENTS

1. Layout Plan Sheet
2. Mix Design Summary
3. Concrete Mix Design Form
4. Concrete Test Results
5. Field Notes
6. Crack Summary
7. Crack Intensity Diagram

CURVE DATA					
P.I. STATION	Δ	RADIUS	TANGENT	LENGTH	BK. TANGENT BRG.
A STA. 70+05.93	67°15'41" LT.	880.00'	585.35'	1033.06'	N 20°52'11" E

SEC. 16, T.32N., R.5E., W.M.
SNOHOMISH COUNTY

SR 9



- LEGEND**
- ☒ JUNCTION BOX
 - ⊙ SOIL BORING LOCATIONS
 - P-P- EXIST. OVERHEAD POWER LINE
 - F-F- EXIST. BURIED FIBER OPTIC
 - OM-OM- ORDINARY HIGH WATER LINE
 - (P) EXIST. POWER POLE
 - ↓ 2 - 2" CONDUIT PIPES IN TRAFFIC BARRIER FOR FULL LENGTH OF BARRIER (TYP.)
 - ± BRIDGE RAILING TYPE BP (TYP. BOTH SIDES)
 - Ω THRIE BEAM GUARDRAIL CONNECTION TYPE D (STD. PLAN C-5)
 - PROPOSED CONCRETE MANHOLE

SR 9 FILE NO. 7350 SHEET 1

Bridge Design Engr. Khaleghi, B	02/11	W:\X-Team\SR9 PILCHUCK CREEK>window files\LAYOUT.wnd
Supervisor Stoddard, RB		
Designed By EJF/MT/NTR	12/11	
Checked By NTR/ MT/EJF	05/12	
Detailed By Puryear, D	12/11	
Bridge Projects Engr. Lewis, R	02/11	
Prelim. Plan By Wei, J	12/10	
Architect/Specialist NSB/PDK/GAW	02/11	DATE REVISION BY APPD

BRIDGE AND STRUCTURES OFFICE

7/17/12

Washington State Department of Transportation

**SR9
PILCHUCK CREEK
REPLACE BRIDGE**

LAYOUT

BRIDGE SHEET NO. 1

SHEET 100 OF 155 SHEETS

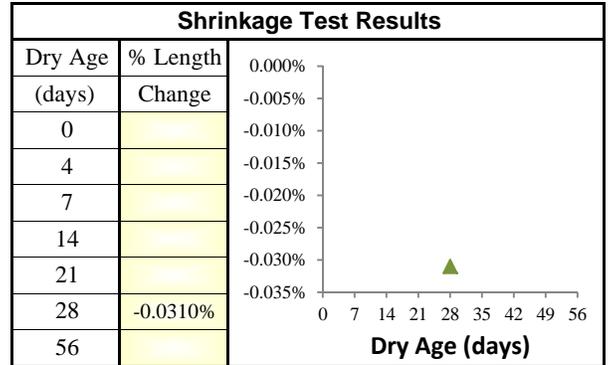
C.S. 3132 - PROJ. NO. XL3402 - NORTHWEST REGION - SR 9 - MP 34.80 TO MP 35.00 - SR 9 OVER PILCHUCK CREEK - BR. NO. 9/134 REPLACEMENT.



Bridge #	9/134	Bridge Name	Pilchuck Creek		Structure ID	0018363A	
Contract #	8383	Region	NW	Project Engineer	Dave Crisman	Performance Deck Concrete?	Yes
Contractor	Granite Construction		Concrete Supplier	Stanwood Redi-Mix		Deck Placement	11/27/13, 12/11/13 & 1/14/14
Bridge Description	3-Span (170' / 220' / 170'), 3-Steel Plate Girders (560' bridge length), 2-Lanes (36' wide roadway)						

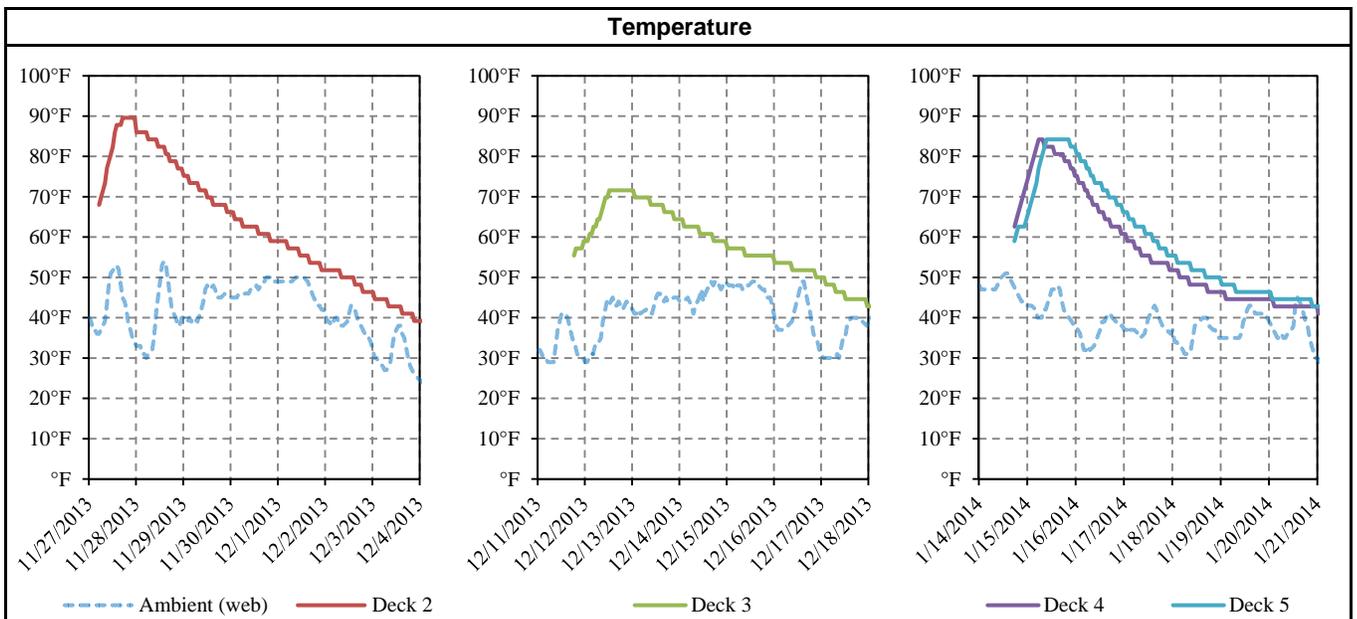
Mix Design (WSDOT Form 350-040)			
Water (max) =		252 lbs/cy	w/c = 0.41 max
Cementitious Materials	Lbs/cy	Source	Type, Class or Grade
cement	458	Lafarge	Type I-II
fly ash	153	Lafarge	Type F/GGBFS 50/50
slag			
latex			
microsilica			
Concrete Admixtures	oz/cy	Manufacturer	Product
air entrainment	1-75	WR Grace	Dravair 1000
water reducer	1-50	WR Grace	Zyla 610
HR water reduce	1-75	WR Grace	Adva 140M
set retarder			
shrink. reducer	1-150	WR Grace	Eclipse 4500

Concrete Test Results		
compressive strength @ 28 days	5,770	psi
modulus of elasticity	4,785,321	psi
permeability @ 56 days	1,705	coulombs
mix design density	148.0	lb/cf



Aggregate					
	Comp. 1	Comp. 2	Comp. 3	Comp. 4	Comp. 5
WSDOT Pit #	D-342	D-342	D-342	D-342	
Grading	#57	#8	Class 2	#4	
% Total	48.0%	5.0%	39.0%	8.0%	
Lbs/cy	1476	170	1202	247	
ASR Mitigation	None Required				

Notes
Although mix design indicates a range for the SRA, testing was done using a 1/4 gallon SRA
Only one number listed for "shrinkage" per AASHTO T-160, assumed to be at 28 days of drying
Deck consisted of 5 placements, only recieved info for 4.





Contractor Granite Construction Inc		Submitted By Stanwood Redi-Mix	Date 6/17/2013
Concrete Supplier Stanwood Redi- Mix		Plant Location Silvana Wa	
Contract Number	Contract Name Pilchuck Creek Bridge		

This mix is to be used in the following Bid Item No(s): BI-045.04.01 SUB-022.00

Concrete Class: (check one only)

- 3000
 4000
 4000^a
 4000^aP
 4000W
 Concrete Overlay
 Cement Concrete Pavement^d
 Other _____

Remarks: _____

Mix Design No. 78424I Plant No. Silvana

Cementitious Materials	Source	Type, Class or Grade	Sp. Gr.	Lbs/cy
Cement	Lafarge/Richmond, BC	Type I-II	3.10	458
Fly Ash ^a	Lafarge/Seattle	Type F Flyash/GGBFS 50/50	2.67	153
GGBFS (Slag)				
Latex				
Microsilica				

Concrete Admixtures	Manufacturer	Product	Type	Est. Range (oz/cy)
Air Entrainment	WR Grace	Daravair 1000		1-75
Water Reducer	WR Grace	Zyla 610	Type A	1-50
High-Range Water Reducer	WR Grace	Adva 140M	Type A-F	1-75
Set Retarder				
Other SRA	WR Grace	Eclipse 4500		1-150

Water (Maximum) 252 lbs/cy Is any of the water Recycled or Reclaimed? Yes^e No

Water Cementitious Ratio (Maximum) 0.41 Mix Design Density 148 lbs/cf^d

Design Performance	1	2	3	4	5	Average ^f
28 Day Compressive Strength (cylinders) psi	5,780	5,700	5,830			5,770
14 Day Flexural ^d Strength (beams) psi						

Agency Use Only (Check appropriate Box)

- This Mix Design **MEETS CONTRACT SPECIFICATIONS** and may be used on the bid items noted above
 This Mix Design **DOES NOT MEET CONTRACT SPECIFICATIONS** and is being returned for corrections

Reviewed By: _____
PE Signature

7/29/13
Date

Mix Design No. 78424I

Plant No. Silvana

Aggregate Information

Concrete Aggregates	Component 1	Component 2	Component 3	Component 4	Component 5	Combined Gradation
WSDOT Pit No.	D-342	D-342	D-342	D-342		
WSDOT ASR 14-day Results (%) ^b	<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	<input type="checkbox"/> Yes <input type="checkbox"/> No				
Grading ^c	No. 57	No. 8	Class 2	No.4		
Percent of Total Aggregate	48	5	39	8		100%
Specific Gravity	2.69	2.69	2.64	2.69		
Lbs/cy (ssd)	1476	170	1202	247		

Percent Passing

	Component 1	Component 2	Component 3	Component 4	Component 5	Combined
2 inch	100	100	100	100		
1-1/2 inch	100	100	100	100		
1 inch	100	100	100	17.2		
3/4 inch	88.06	100	100	2.6		
1/2 inch	36.15	100	100			
3/8 inch	11.07	85.79	100	.9		
No. 4	0.67	12.41	100			
No. 8	0	0.62	90.17			
No. 16	0	0.25	66.03			
No. 30	0	0	39.48			
No. 50	0	0	19.31			
No. 100	0	0	7.76			
No. 200	0	0	1.72	.1		

Fineness Modulus: 2.70 (Required for Class 2 Sand)

ASR Mitigation Method Proposed^b: None Required

Notes:

- a Required for Class 4000D and 4000P mixes.
- b Alkali Silica Reactivity Mitigation is required for sources with expansions over 0.20% - Incidate method for ASR mitigation. For expansion of 0.21% - 0.45%, acceptable mitigation can be the use of low alkali cement or 25% type F fly ash. Any other proposed mitigation method or for pits with greater than 0.45% expansion, proof of mitigating measure, either ASTM C1260 / AASHTO T303 test results must be attached. If ASTM C 1293 testing has been submitted indicating 1-year expansion of 0.04% or less, mitigation is not required.
- c AASHTO No. 467, 57, 67, 7, 8; WSDOT Class 1, Class 2; or combined gradation. See Standard Specification 9-03.1.
- d Required for Cement Concrete Pavements.
- e Attach test results indicating conformance to Standard Specification 9-25.1.
- f Actual Average Strength as determined from testing or estimated from ACI 211.



Modulus of Elasticity c-469

4,785,321 psi

ASTM C-672 Scaling Resistance of Concrete Surfaces Exposed to Deicing Chemicals

Result:	Cycles	Rating
	5	0
	10	0
	15	1
	25	1
	30	1
	50	1



AASHTO T-160 Drying Shrinkage

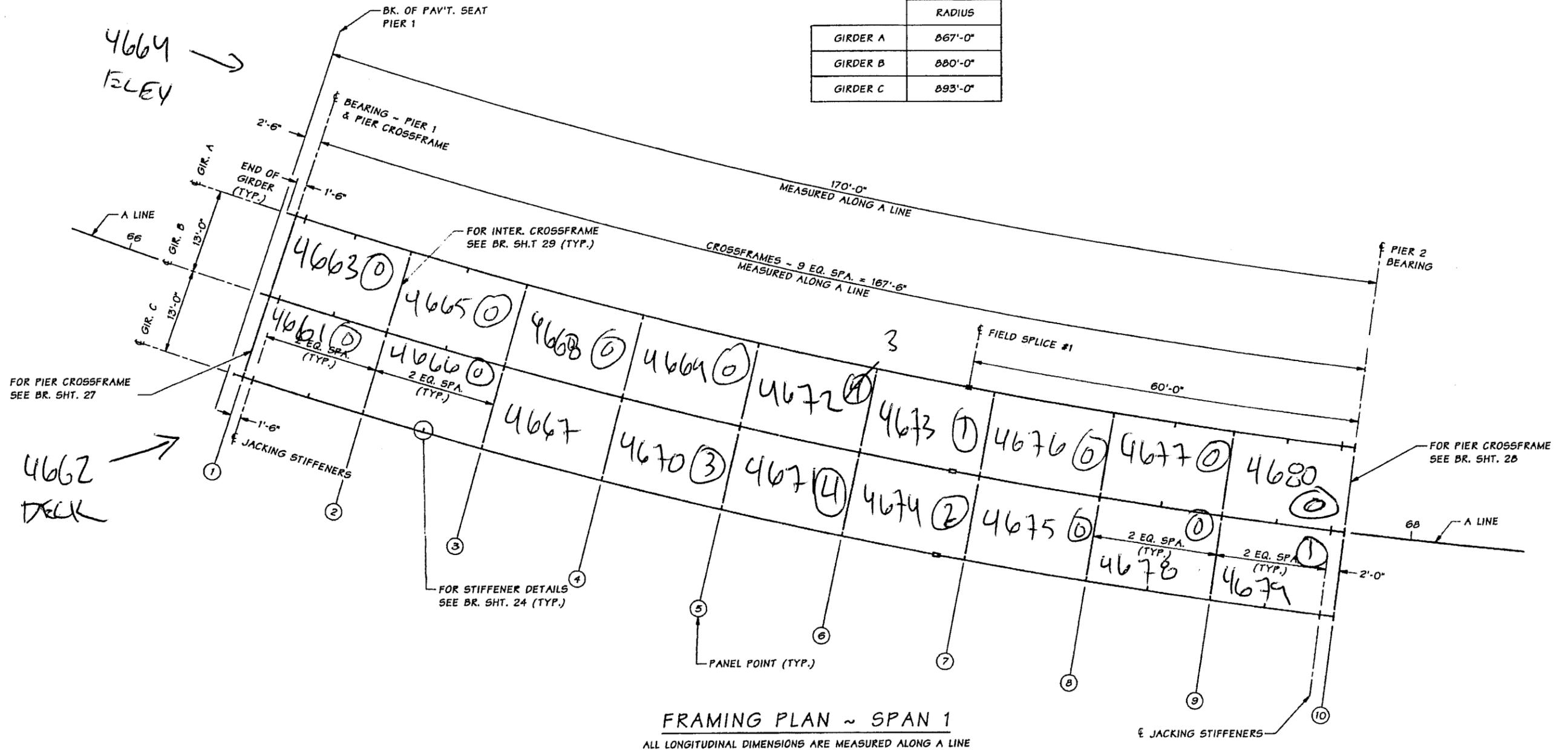
Micro Strain: 310
WSDOT Requirements : Less than 320

AASHTO T-227 Rapid Chloride Ion Permeability

Result:	Days	Coulombs	WSDOT Requirements
	56	1705	Less than 2000

Rob Shogren, P.E, Ph.D.
Technical Service Engineer
Lafarge North America

	RADIUS
GIRDER A	867'-0"
GIRDER B	880'-0"
GIRDER C	893'-0"



SR 9 FILE NO. 7350 SHEET 19

Bridge Design Engr.	Khalteghi, S	N:\X-Team\SR9 PILCHUCK CREEK\window files\FRAMING PLAN 1.wpd		REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
Supervisor	Stoddard, RB			30	WASH.			
Designed By	Talukdar, M	05/12						
Checked By	Rodda, NT	05/12						
Detailed By	Puryear, D	05/12						
Bridge Projects Engr.				JOB NUMBER 11A020				
Prelim. Plan By								
Architect/Specalist		DATE	REVISION	BY	APPD			



BRIDGE AND STRUCTURES OFFICE

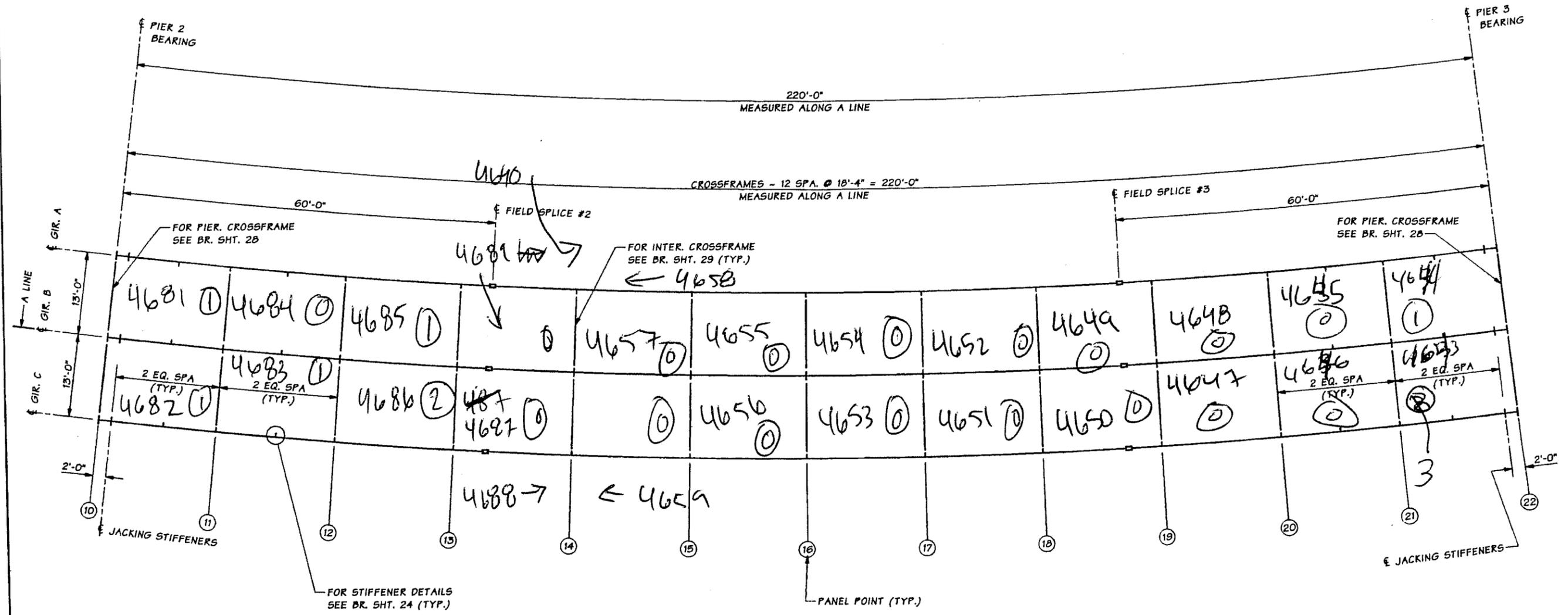


Washington State Department of Transportation

SR9
PILCHUCK CREEK
REPLACE BRIDGE

FRAMING PLAN
1 OF 3

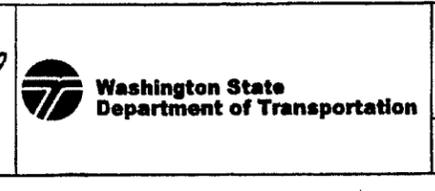
BRIDGE SHEET NO. 19
SHEET 118 OF 155 SHEETS



SR 9 FILE NO. 7350 SHEET 20

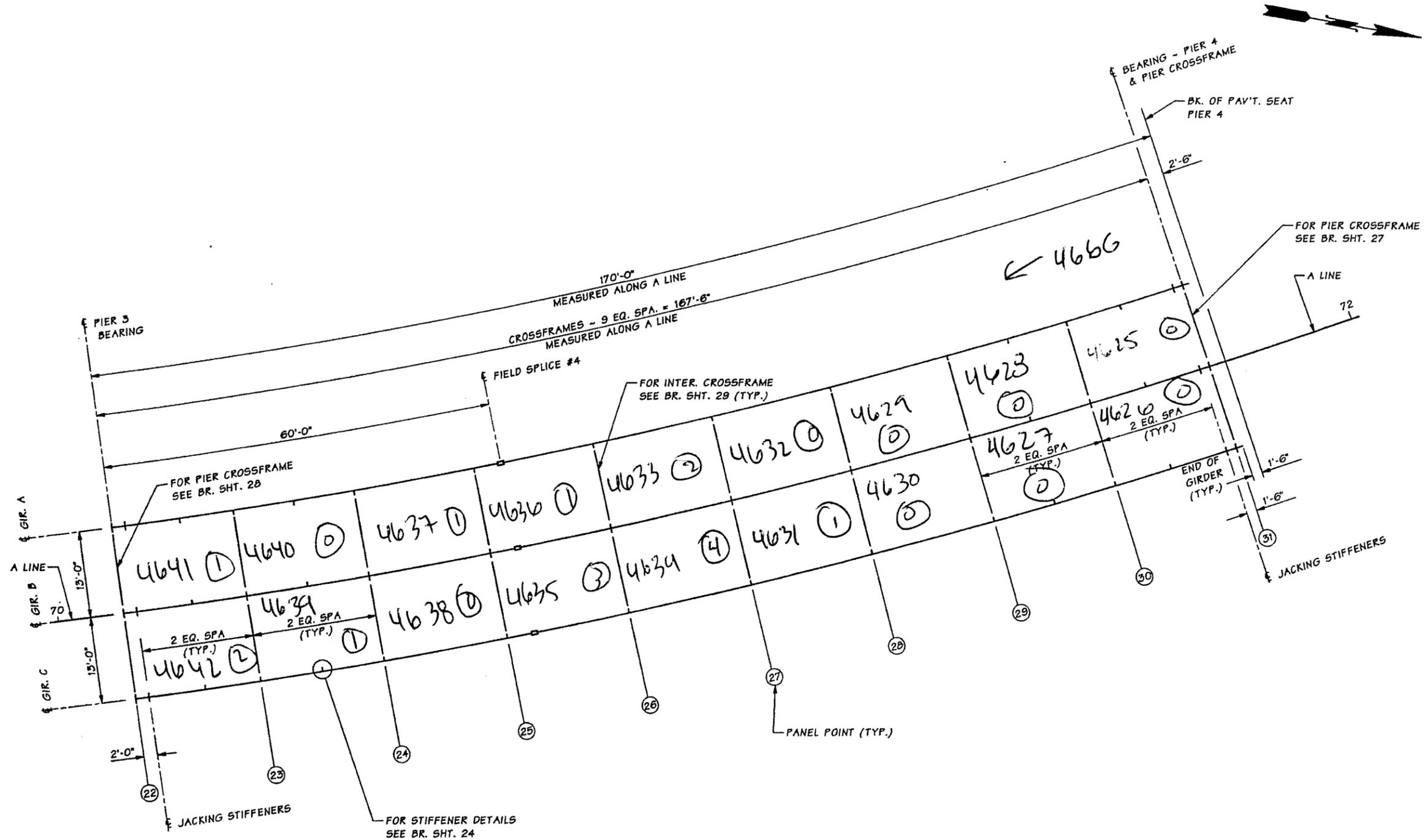
Bridge Design Engr.	Khaleghi, S	M:\X-Team\SR9 PILCHUCK CREEK\window files\FRAMING PLAN 2.wnd	
Supervisor	Stoddard, RB	MISSION NO.	STATE
Designed By	Talukdar, M 05/12	10	WASH.
Checked By	Rodda, NT 05/12	JOB NUMBER 11A020	
Detailed By	Puryear, D 05/12		
Bridge Projects Engr.			
Prelim. Plan By			
Architect/Specialist		DATE	REVISION
		BY	APPD

BRIDGE AND STRUCTURES OFFICE
 7/16/12



SR9 PILCHUCK CREEK REPLACE BRIDGE	BRIDGE SHEET NO. 20 SHEET 119 OF 155 SHEETS
FRAMING PLAN 2 OF 3	

Mon Jul 16 16:14:54 2012



FRAMING PLAN ~ SPAN 3
ALL LONGITUDINAL DIMENSIONS ARE MEASURED ALONG A LINE

SR 9 FILE NO. 7350 SHEET 21

Bridge Design Engr.	Khaleghi, B	M:\X-Team\SR9 PILCHUCK CREEK\window files\FRAMING PLAN 3.wid		REGION NO.	STATE	FED. AID PROJ. NO.	SHEET NO.	TOTAL SHEETS
Supervisor	Stoddard, RB			10	WASH.			
Designed By	Talukdar, M	05/12						
Checked By	Rodda, NT	05/12						
Detailed By	Puryear, D	05/12						
Bridge Projects Engr.								
Prelim. Plan By								
Architect/Specialist		DATE	REVISION	BY	APPD			

BRIDGE AND STRUCTURES OFFICE

7/16/12

7/16/12

Washington State Department of Transportation

SR9 PILCHUCK CREEK REPLACE BRIDGE

FRAMING PLAN 3 OF 3

21
120
155



Bridge #	9/134	Bridge Name	Pilchuck Creek			Structure ID	0018363A		
Contract #	8383	Region	NW	Project Engineer	Dave Crisman		Performance Deck Concrete?	Yes	
Contractor	Granite Construction		Concrete Supplier	Stanwood Redi-Mix		Deck Placement	11/27/13, 12/11/13 & 1/14/14		
Bridge Description	3-Span (170' / 220' / 170'), 3-Steel Plate Girders (560' bridge length), 2-Lanes (36' wide roadway)								

L = length between diaphragms (or length of "bay")

S = girder spacing

N₁₀₀ = number of cracks equal to get 100% cracking severity = L / 2 ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

% = cracking severity percentage = N_{cr}/N₁₀₀ (rounded to the nearest 5%)

Avg. =	7%
Min. =	0%
Max. =	45%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N _{cr}	N ₁₀₀	%
1	1	A	B	18.61	13.00	0	9	0%
1	1	B	C	18.61	13.00	0	9	0%
1	2	A	B	18.61	13.00	0	9	0%
1	2	B	C	18.61	13.00	0	9	0%
1	3	A	B	18.61	13.00	0	9	0%
1	3	B	C	18.61	13.00	0	9	0%
1	4	A	B	18.61	13.00	0	9	0%
1	4	B	C	18.61	13.00	3	9	35%
1	5	A	B	18.61	13.00	3	9	35%
1	5	B	C	18.61	13.00	4	9	45%
1	6	A	B	18.61	13.00	1	9	10%
1	6	B	C	18.61	13.00	2	9	20%
1	7	A	B	18.61	13.00	0	9	0%
1	7	B	C	18.61	13.00	0	9	0%
1	8	A	B	18.61	13.00	0	9	0%
1	8	B	C	18.61	13.00	0	9	0%
1	9	A	B	18.61	13.00	0	9	0%
1	9	B	C	18.61	13.00	1	9	10%
2	1	A	B	18.33	13.00	1	9	10%
2	1	B	C	18.33	13.00	1	9	10%
2	2	A	B	18.33	13.00	0	9	0%
2	2	B	C	18.33	13.00	1	9	10%
2	3	A	B	18.33	13.00	1	9	10%
2	3	B	C	18.33	13.00	2	9	20%
2	4	A	B	18.33	13.00	0	9	0%
2	4	B	C	18.33	13.00	0	9	0%
2	5	A	B	18.33	13.00	0	9	0%
2	5	B	C	18.33	13.00	0	9	0%
2	6	A	B	18.33	13.00	0	9	0%
2	6	B	C	18.33	13.00	0	9	0%
2	7	A	B	18.33	13.00	0	9	0%
2	7	B	C	18.33	13.00	0	9	0%
2	8	A	B	18.33	13.00	0	9	0%
2	8	B	C	18.33	13.00	0	9	0%
2	9	A	B	18.33	13.00	0	9	0%
2	9	B	C	18.33	13.00	0	9	0%
2	10	A	B	18.33	13.00	0	9	0%
2	10	B	C	18.33	13.00	0	9	0%
2	11	A	B	18.33	13.00	0	9	0%
2	11	B	C	18.33	13.00	0	9	0%
2	12	A	B	18.33	13.00	1	9	10%



Bridge #	9/134	Bridge Name	Pilchuck Creek			Structure ID	0018363A	
Contract #	8383	Region	NW	Project Engineer	Dave Crisman	Performance Deck Concrete?	Yes	
Contractor	Granite Construction		Concrete Supplier	Stanwood Redi-Mix		Deck Placement	11/27/13, 12/11/13 & 1/14/14	
Bridge Description	3-Span (170' / 220' / 170'), 3-Steel Plate Girders (560' bridge length), 2-Lanes (36' wide roadway)							

L = length between diaphragms (or length of "bay")

S = girder spacing

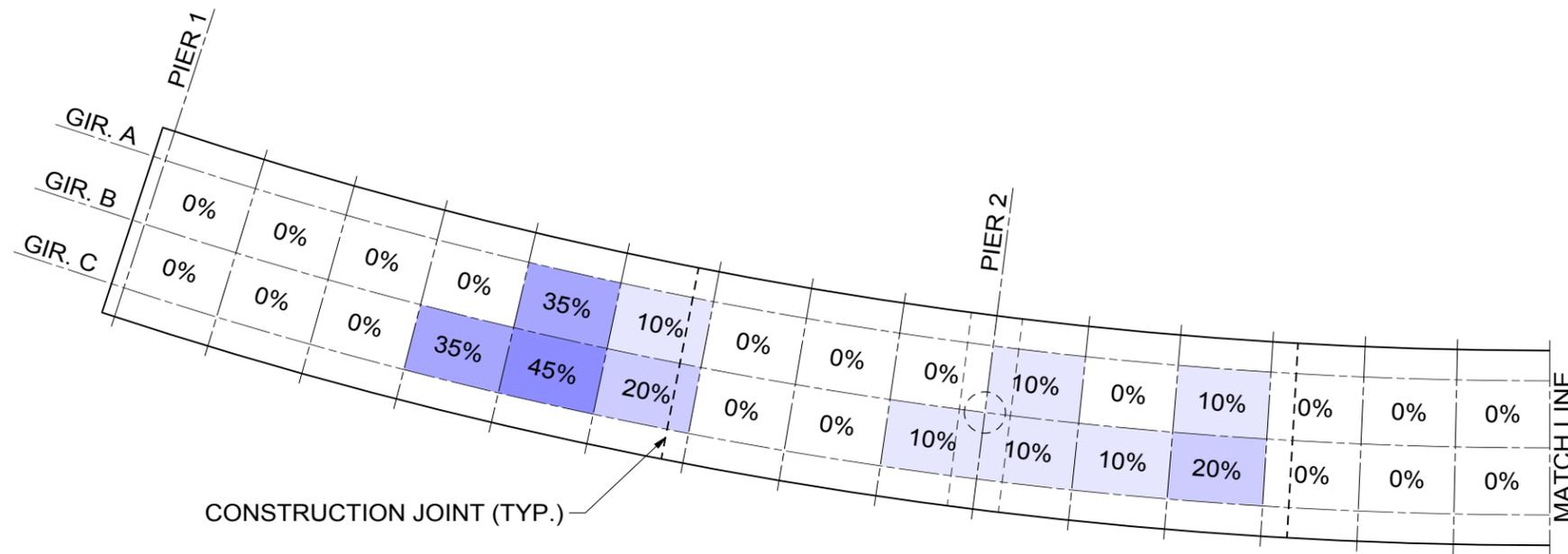
N_{100} = number of cracks equal to get 100% cracking severity = $L / 2$ ft (transverse crack spaced at 2 ft on center)

N_{cr} = number of leaching cracks counted during visual inspection

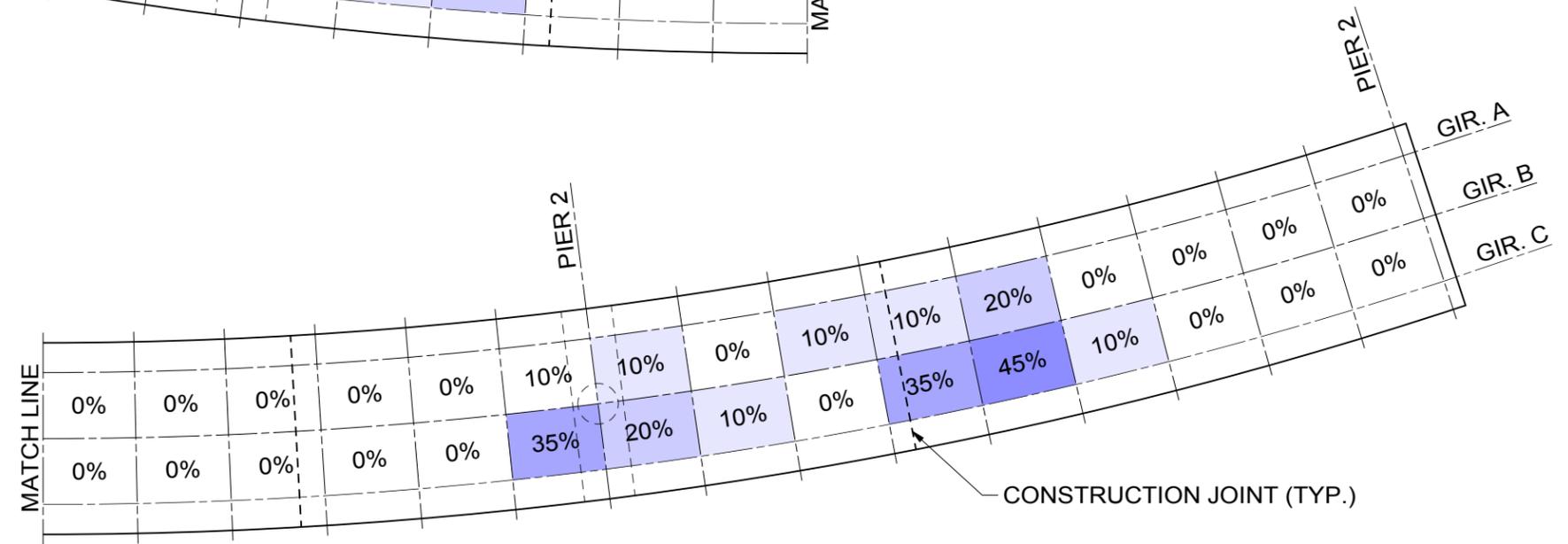
% = cracking severity percentage = N_{cr}/N_{100} (rounded to the nearest 5%)

Avg. =	7%
Min. =	0%
Max. =	45%

Span	Bay	Gir. Lt.	Gir Rt.	L (ft)	S (ft)	N_{cr}	N_{100}	%
2	12	B	C	18.33	13.00	3	9	35%
3	1	A	B	18.61	13.00	1	9	10%
3	1	B	C	18.61	13.00	2	9	20%
3	2	A	B	18.61	13.00	0	9	0%
3	2	B	C	18.61	13.00	1	9	10%
3	3	A	B	18.61	13.00	1	9	10%
3	3	B	C	18.61	13.00	0	9	0%
3	4	A	B	18.61	13.00	1	9	10%
3	4	B	C	18.61	13.00	3	9	35%
3	5	A	B	18.61	13.00	2	9	20%
3	5	B	C	18.61	13.00	4	9	45%
3	6	A	B	18.61	13.00	0	9	0%
3	6	B	C	18.61	13.00	1	9	10%
3	7	A	B	18.61	13.00	0	9	0%
3	7	B	C	18.61	13.00	0	9	0%
3	8	A	B	18.61	13.00	0	9	0%
3	8	B	C	18.61	13.00	0	9	0%
3	9	A	B	18.61	13.00	0	9	0%
3	9	B	C	18.61	13.00	0	9	0%



CONSTRUCTION JOINT (TYP.)



CONSTRUCTION JOINT (TYP.)

CRACKING INTENSITY ~ BRIDGE 9/134

100% = CRACK EVERY 2 FT.



BRIDGE NUMBER	9/134
BRIDGE NAME	PILCHUCK CREEK
INSPECTION DATE	5/22/2015
DECK CONCRETE	PERFORMANCE BASED